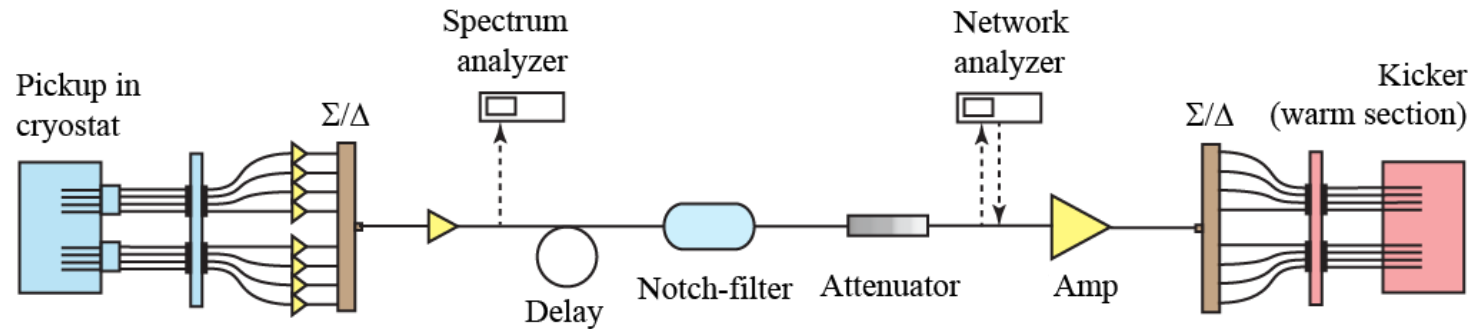


# Algorithmic control of stochastic cooling systems

21 January 2019 | Nikolay Shurkhno, FZ Jülich

# Stochastic cooling system as an object



## Approaches to cooling system control:

1. Individual control of each device

### Devices:

- Amplifiers
- Switches
- Delays
- Attenuators
- Power supplies
- Meas. devices
- ...

### Interfaces:

- USB
- RS232
- Ethernet
- I2C
- Custom API
- ...

2. Control independent of specific hardware

### Cooling system

- Gain
- Delay
- Mode
- HTF
- Adjust to energy
- ...

# Class hierarchy

## Base instr.

- self-test
- address
- name
- ..



## Generic instr.

- Switch
- VNA
- Power supply
- ..

## Interface

USB/RS232/TCPIP

- read
- write
- connect
- ..



## Instrument

VNA, SA, Switch

- read
- write
- connect
- ..

The only system-dependent part

## Complex instrument

- Any device-specific methods
- delay
- adjust\_gain
- ..

Notch-filters

Complex delays with adjustable attenuation

Complex gains/attenuations

Thin clients

Measurement subsystems

...

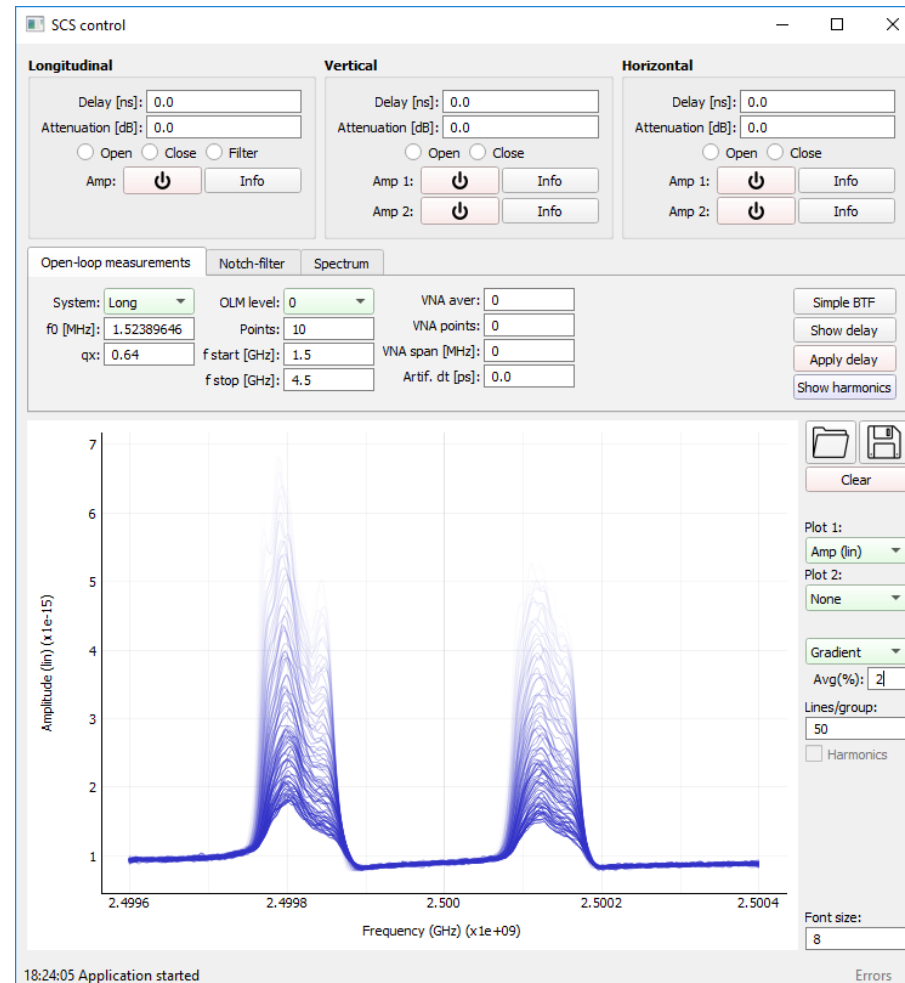
## Stochastic cooling system

- gain
- delay
- mode
- complex gain
- ...

# Issues

1. Multi-threading – “per query”
2. Built-in simulation
3. Embedding into accelerator control system (EPICS, FESA, TANGO, etc.) – reimplement classes for specific instruments

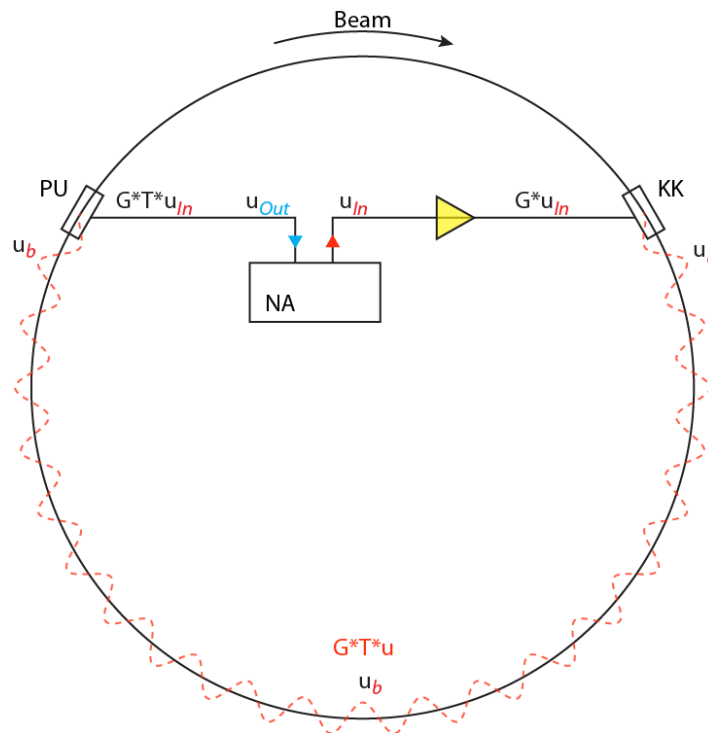
# Control software basic draft



# Algorithms

1. Vector network analyzer
  1. Single open-loop measurements
  2. Multiple open-loop measurements
2. Notch-filter
  1. Frequency
  2. Depth
3. Spectrum analyzer
  1. Distribution evolution ( $\Psi(t)$ )
  2. PU amplitude measurements
  3. Open/closed loop measurements

# Open-loop measurements



$$S_{21} = \frac{u_{out}}{u_{in}} = \textcolor{red}{HTF} \cdot BTF$$

(HTF = hardware transfer function  
BTF = beam transfer function)

Transverse and longitudinal BTF:

$$\tilde{T}_n^\perp = \frac{1}{2\omega_\beta} \int \frac{\Psi(E)}{\omega_{\textcolor{red}{n}}(E) - \omega} dE$$

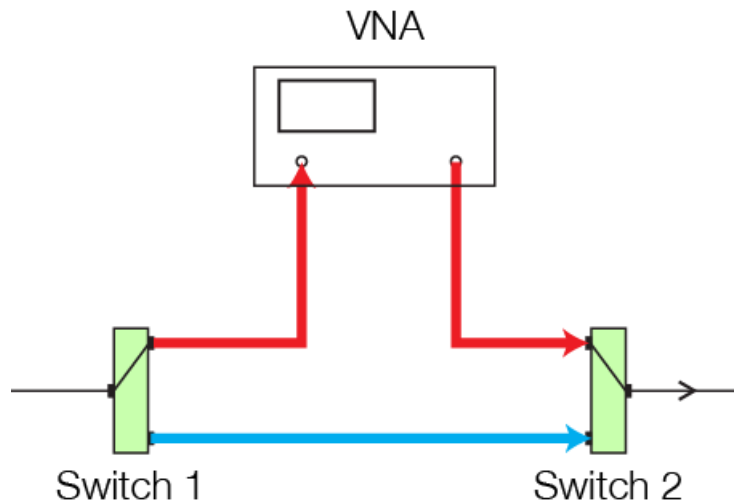
$$\tilde{T}_n^\Sigma = i \frac{e^2 f_0^2}{\textcolor{red}{n}k} \int \frac{\partial \Psi / \partial E}{E - \textcolor{red}{E}} dE$$

BTF theoretically could be de-embedded with PDF measurements, but in any case relative HTF is enough:

$$S_{21} \rightarrow S_{21} * n = HTF * const$$

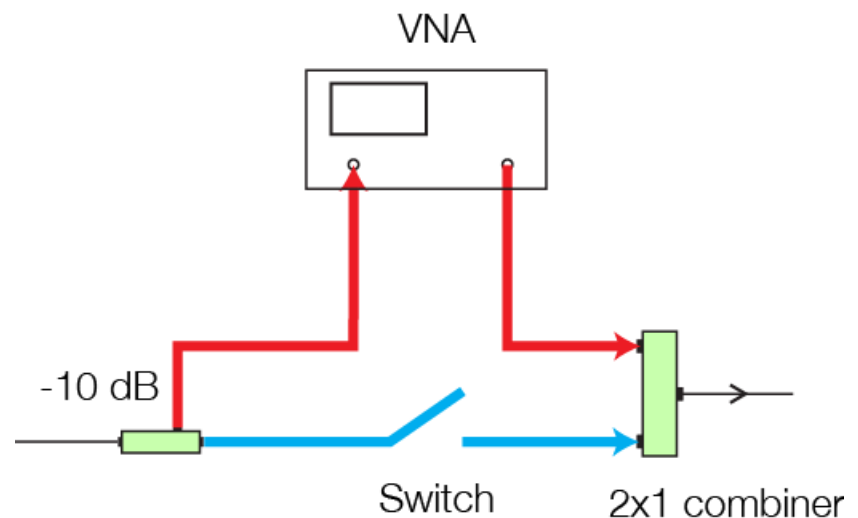
# Setup for open-loop measurements

Traditional scheme



Maintenance stops for adjustment

New scheme



Parallel adjustment

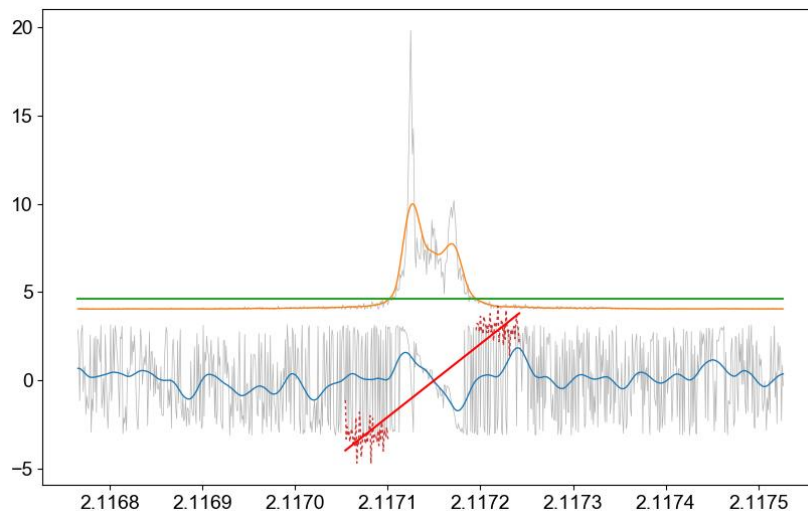
VNA calibration is done manually and data is saved to a PC, so the VNA could be changed if needed



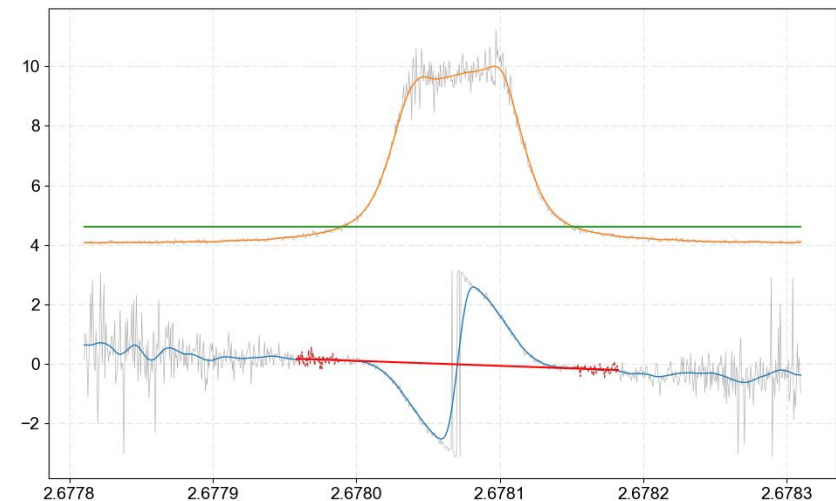
# Open-loop measurements techniques

- Single sweep
  - Set VNA  $f_{start}, f_{stop}$  to the  $n_1, n_2$  of the passband, set VNA points to  $n_2 - n_1 - 1$
  - Very fast ( $\sim$ s), especially for small number of points
- Multiple sweep
  - Measure harmonics individually and calculate
  - Time-consuming (seconds to minutes, depends on number of points), but clear and precise and doesn't require manual setting for points of NA (not every device has this option)

# Trick for automatic multiple sweep



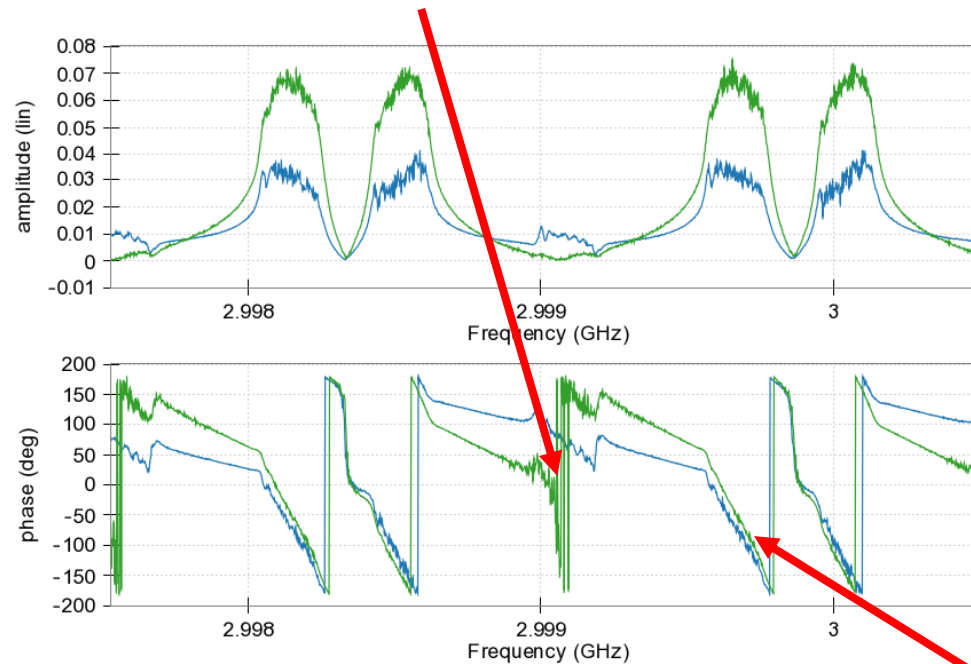
Measured phase near -180deg



Corrected phase  
 $dt_{opt} = \min(\arg(S_{21}(dt)))$   
 dt – artificial delay

# Transverse harmonic sweep

It's easy to measure center frequency for longitudinal cooling



But for transverse cooling one need to know exact fractional tune, which could be unknown

# System adjustment after open-loop measurements

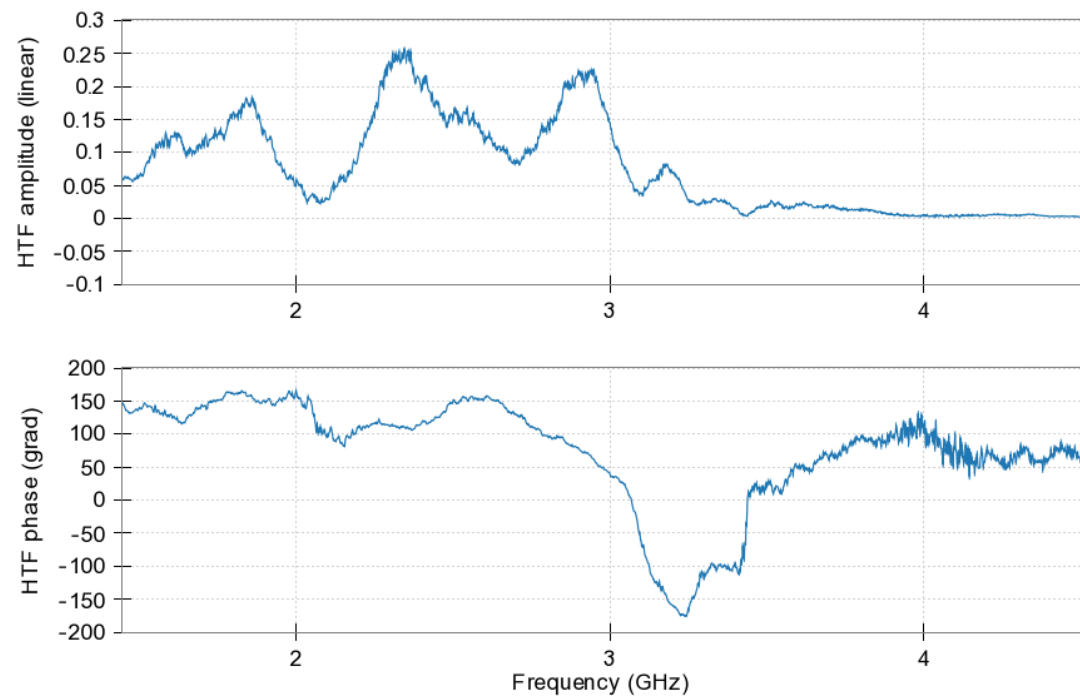
The real HTF is fundamentally non-linear, so things like “lets make the phase flat” don’t fully solve the problem

The adjustment must be done with respect to the task:

$$\tau_0 \text{ VS. } \sigma_\infty / A_\infty^\beta$$

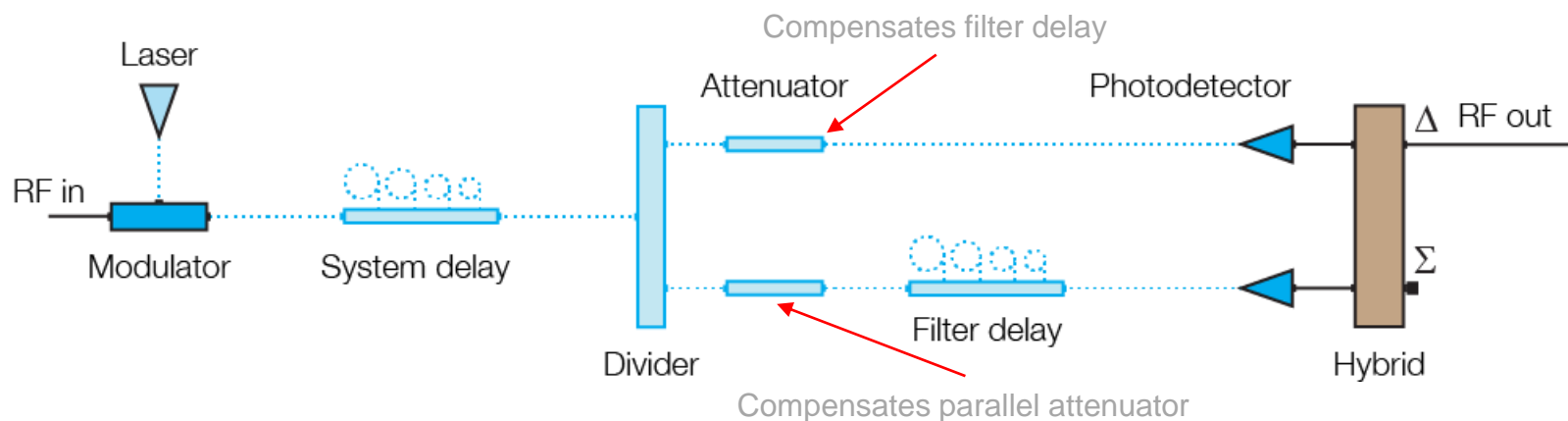
So one can do a lot of measurements studying the behavior of the system wrt to gain and delay or immediately simulate the process

HTF of system with turned-around kicker:

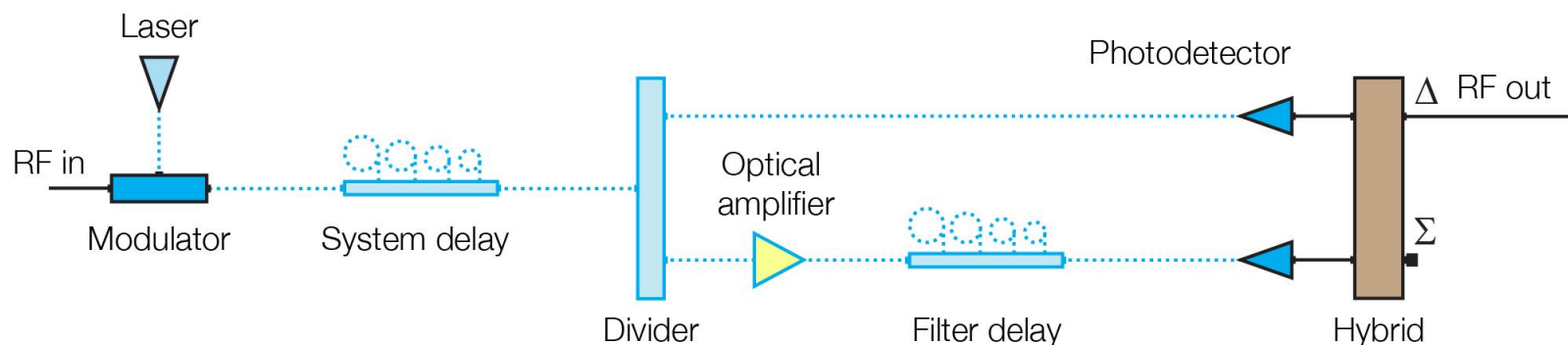


# Optical notch-filter

## “Traditional” scheme:

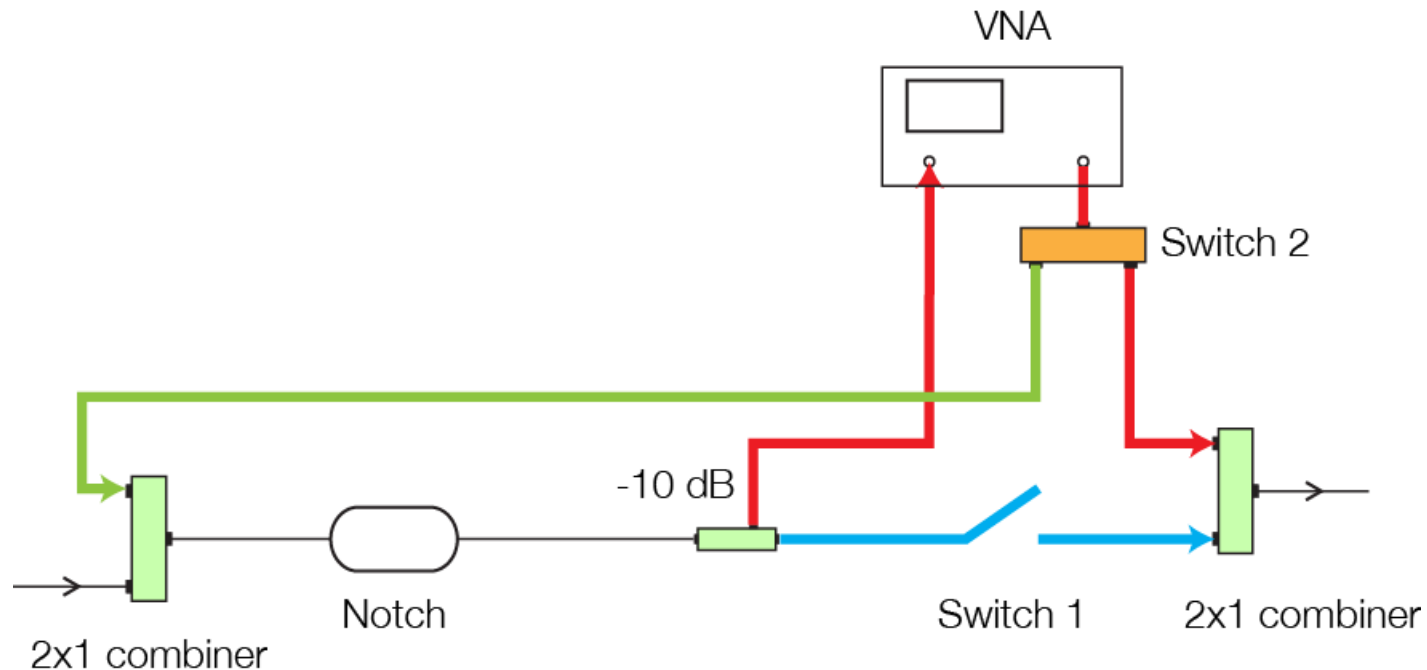


## New scheme:



The intrinsic delay of notch-filter was significantly enhanced

# Open-loop measurements with notch-filter



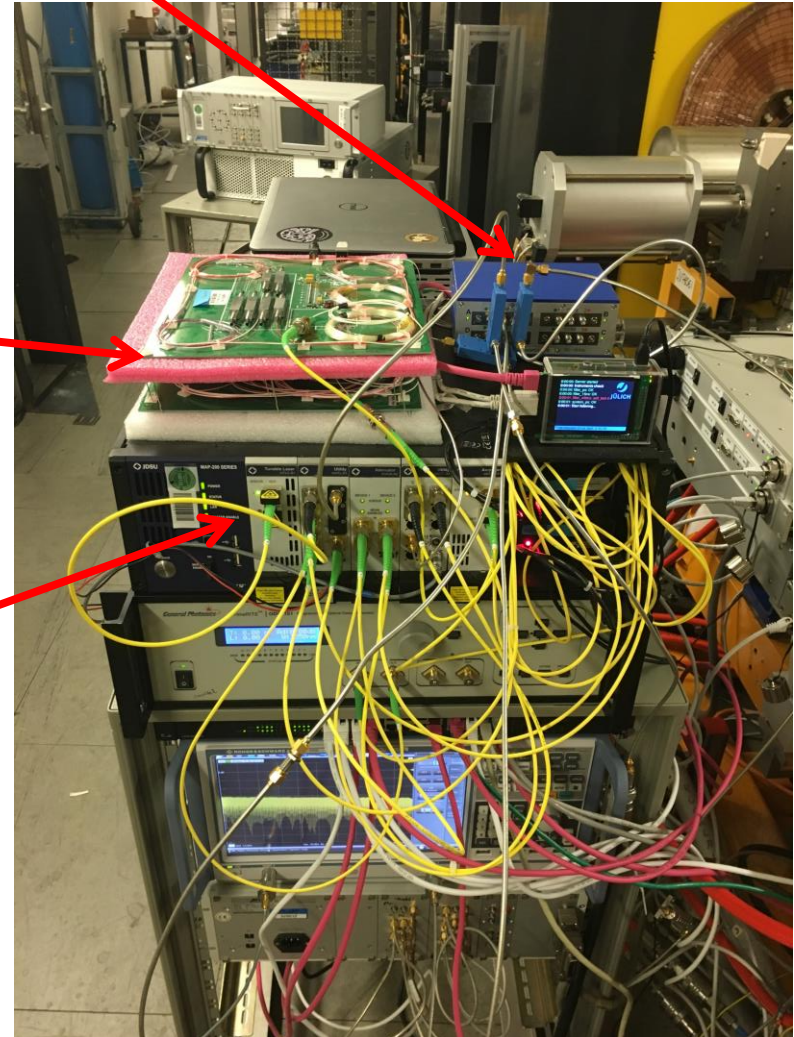
Notch-filter and open-loop measurements  
can be done independently of system operation

## Switch for OLM/filter measurements

## Notch-filter

Two step delays  
0-15.5ns /  $dt=0.5\text{ns}$   
0-496ns /  $dt=16\text{ns}$

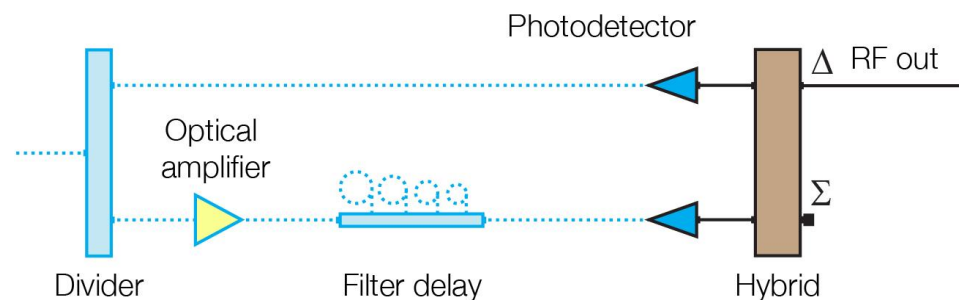
JDSU platform  
Laser, modulator,  
attenuators, amplifier  
precise delay, etc.



# Notch-filter adjustment

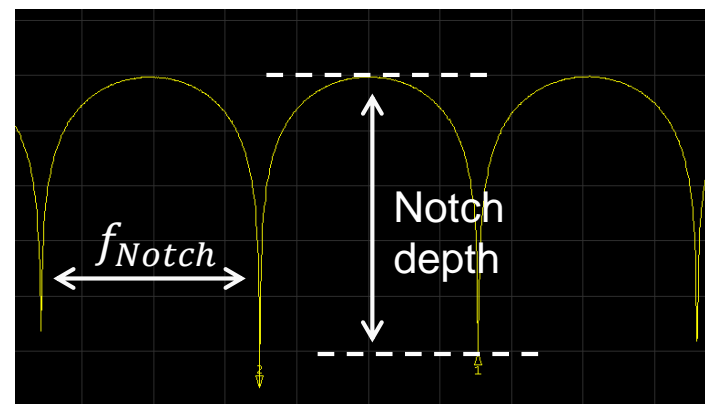
Parameters of interest:

- **Notch frequency** ( $\sim \Delta \text{delay}$ )
- **Notches' depths** ( $\sim \Delta \text{attenuation}$ )



The intuitive measurements of *power* and *delay differences* for both legs are fast, but not accurate (and breaks the loop), so

- **Frequency** is adjusted by measuring the average frequency (3 meas. for extending spans) and correction
- **Depths** are adjusted by binary search for the optimum gain value

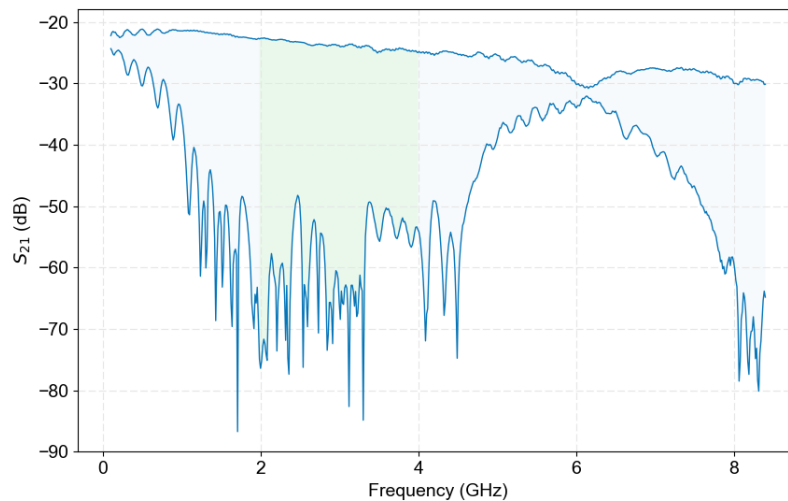


The complete adjustment takes  $<1$  min, but we always missed several ps!

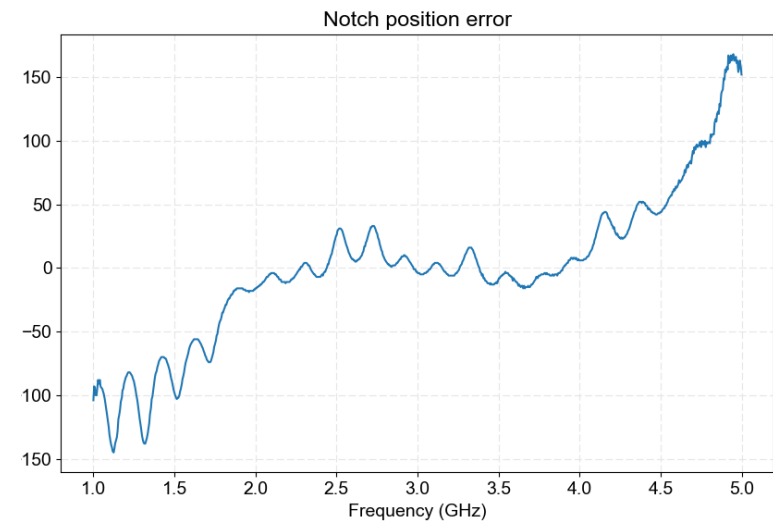


# Notch-filter dispersion

Notch frequency and depths fluctuate in passband



Notch-filter amplitude response

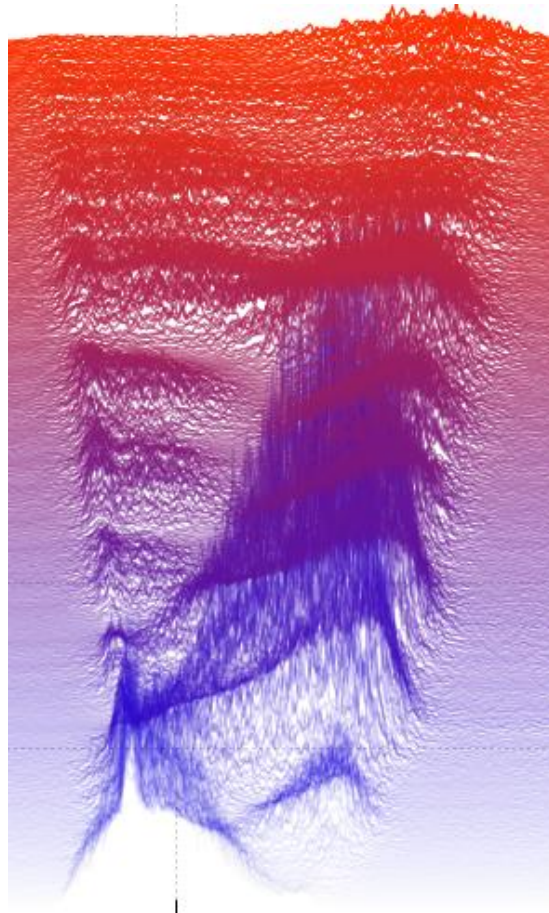


Measured notches' position errors (difference between expected and measured notch)

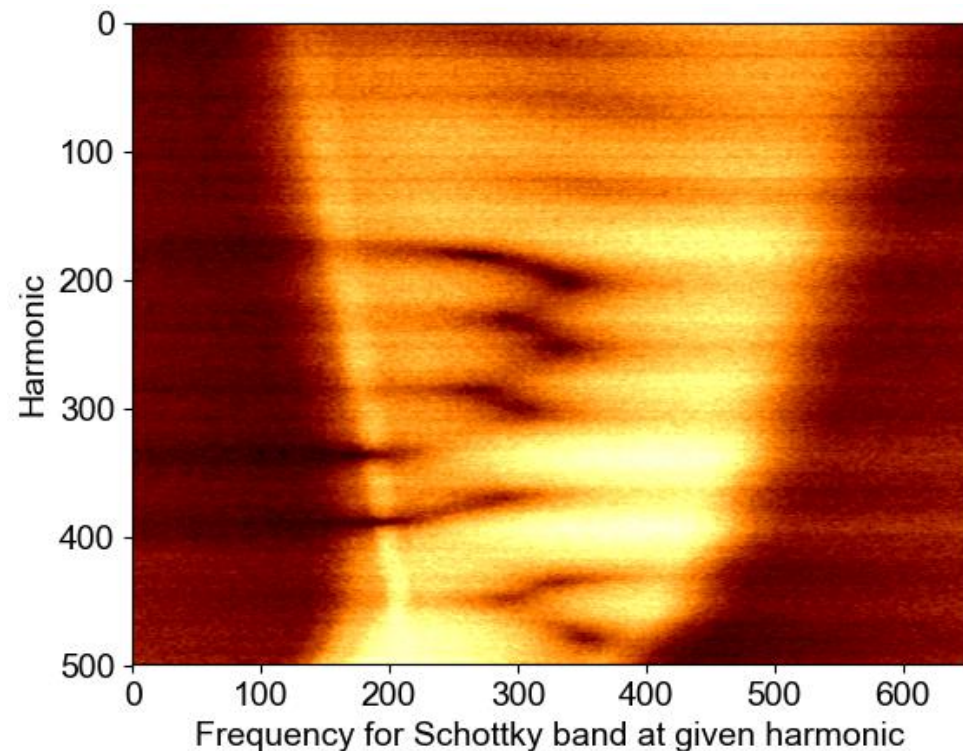
To make proper adjustment we can use simulation of PDF's center of mass evolution and compensate for lost ps

# Spectrum Analyzer

## Notch-filter dispersion and the beam



Waterfall plot of filtered longitudinal Schottky noise



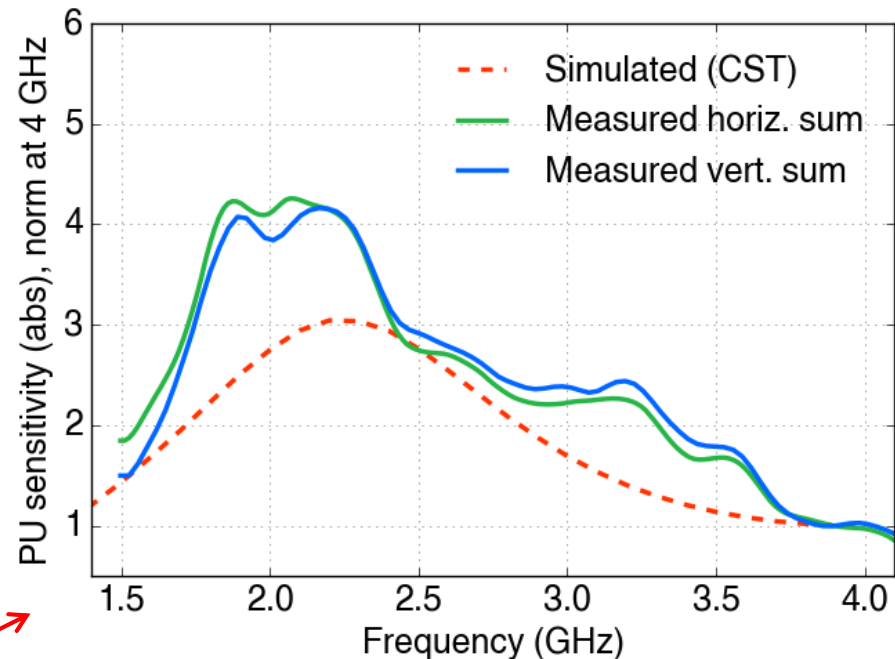
# Pick-up amplitude behavior (and sometimes kicker)

Signal from the spectrum analyzer:

$$S(f) \sim \frac{\Psi}{n}$$

So

$$|S_{PU}| \sim S(f) \cdot n$$

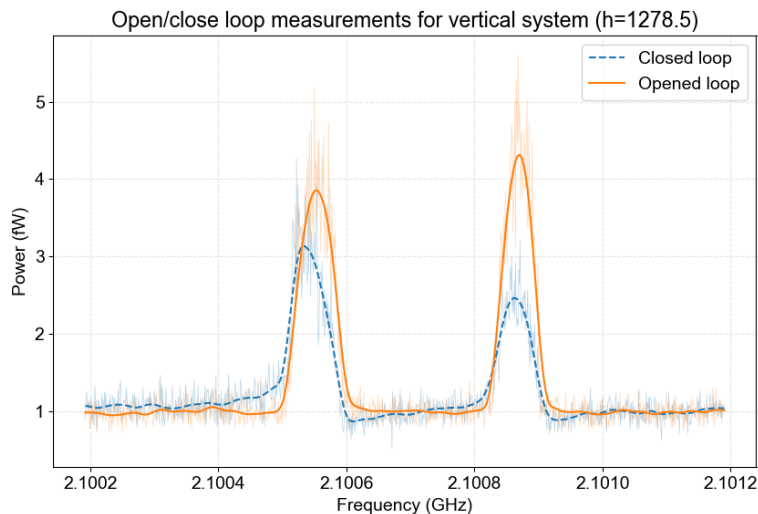


Comparison of measured pick-up amplitude with the results of spectrum measurements, cables and preamplifiers were de-embedded

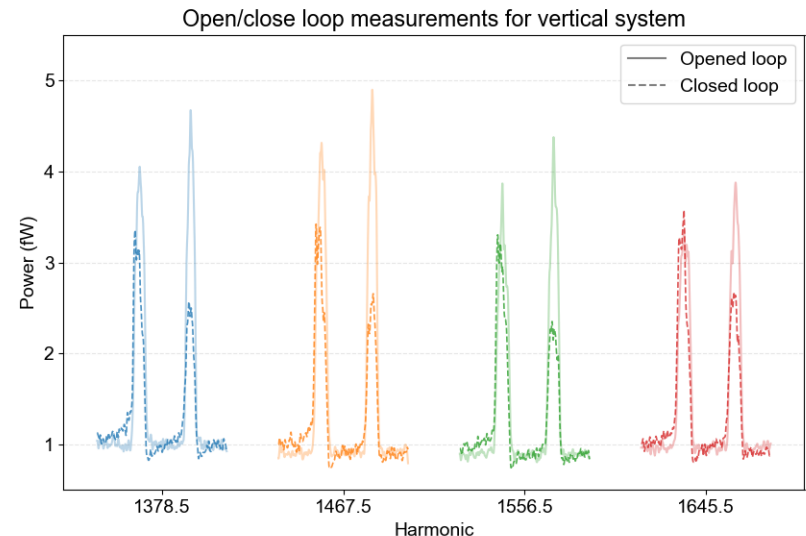
# Opened/closed loop measurements

With opened/closed loop measurements system also can be fully adjusted.

Method is straightforward, at all desired harmonics:  
open loop, measure, close loop, measure. It is also advantageous to make normal open-loop measurements with VNA for further simulation



OCLM for single harmonic

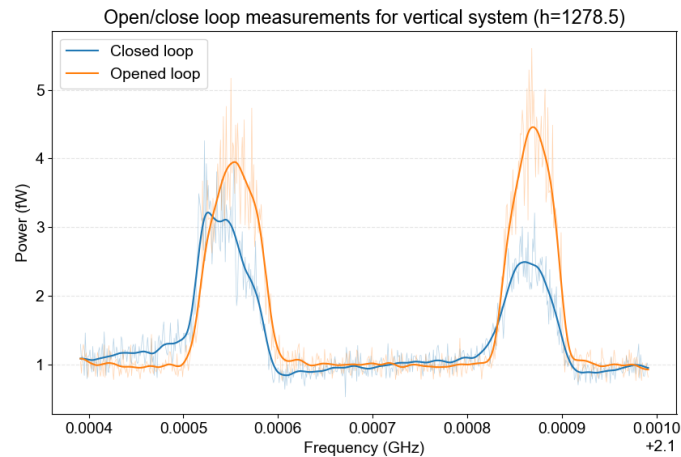


OCLM for several harmonics

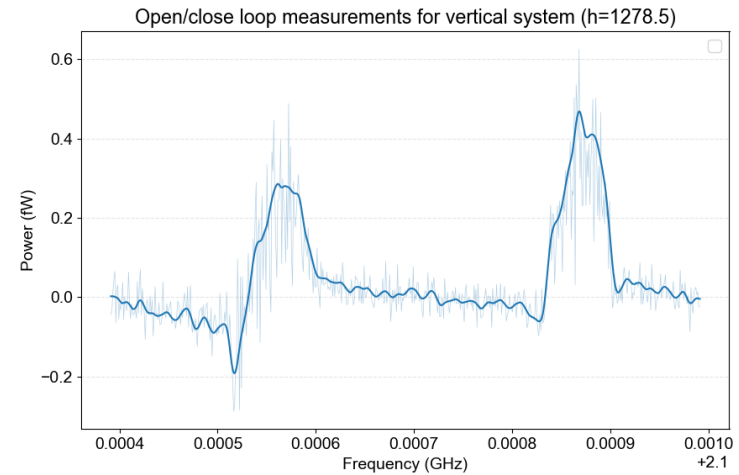
Clean measurements with SA are time-consuming, so every closed loop measurement influence the beam, thus measurements in the beginning and in the end could be inconsistent

# Transverse opened/closed loop measurements

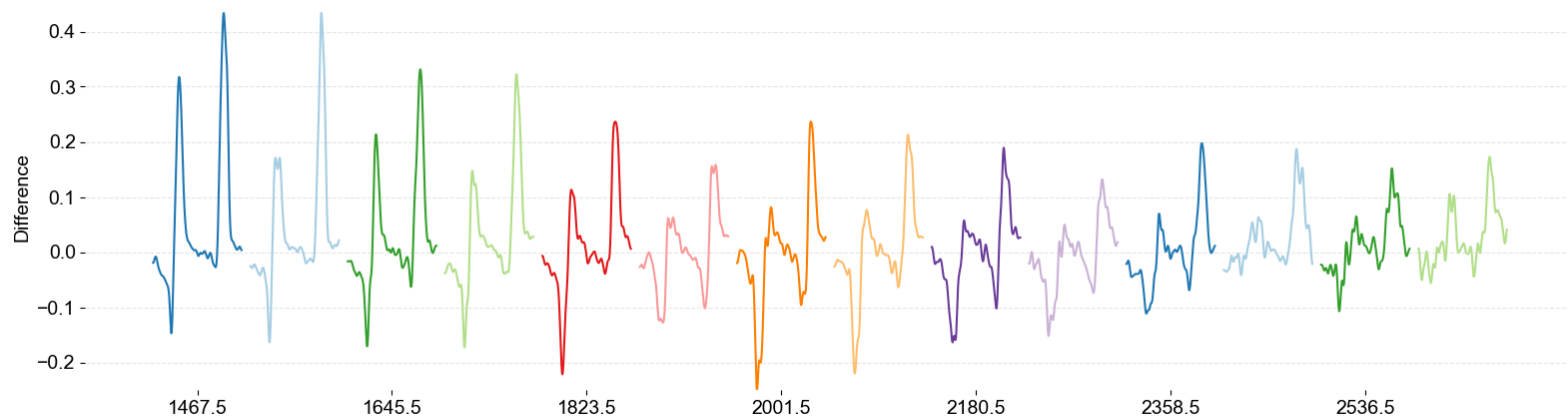
Raw measurements:



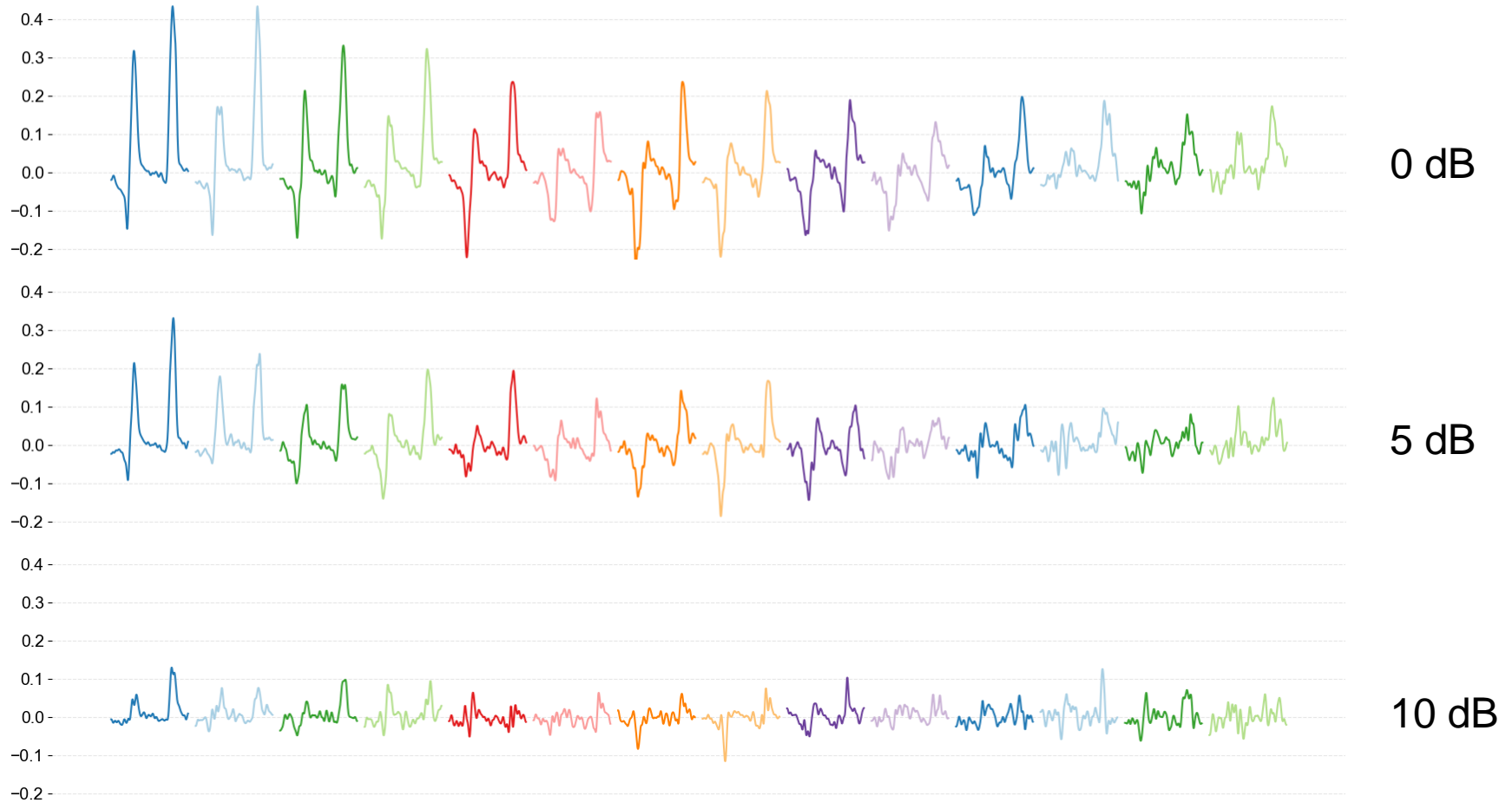
$$(S_{Open} - S_{Closed}) / \max(S_{Open})$$



Differences within passband:

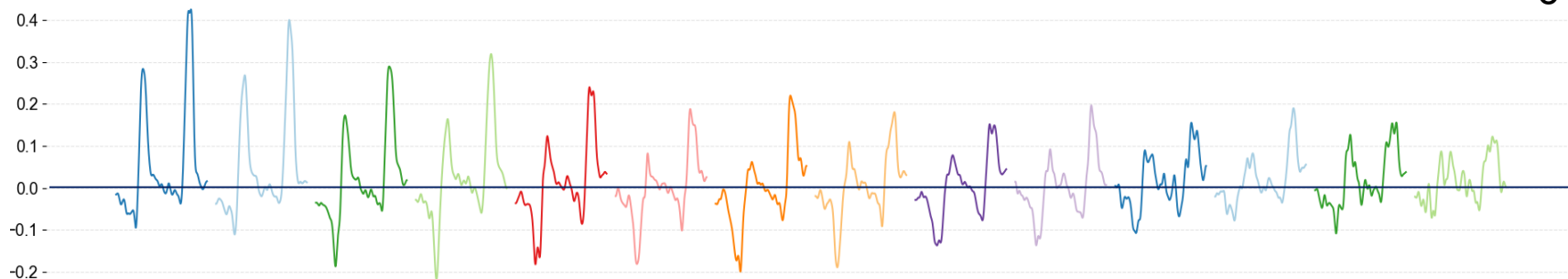


# Different attenuations

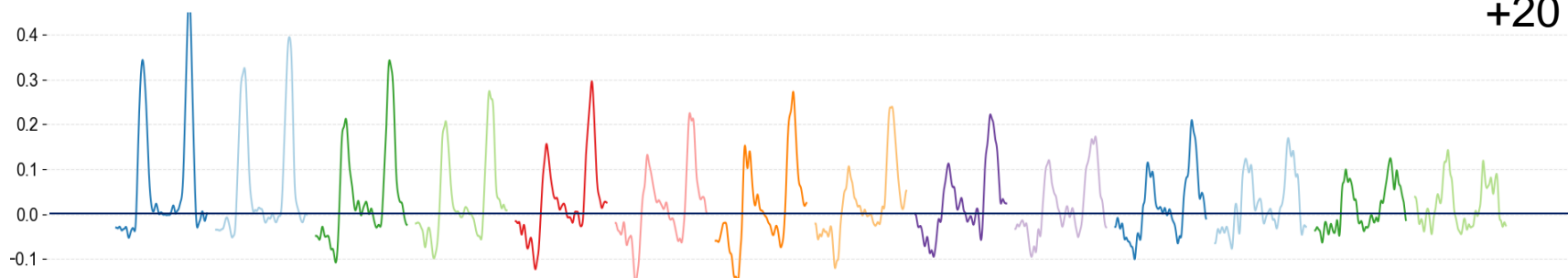


# Different system delays

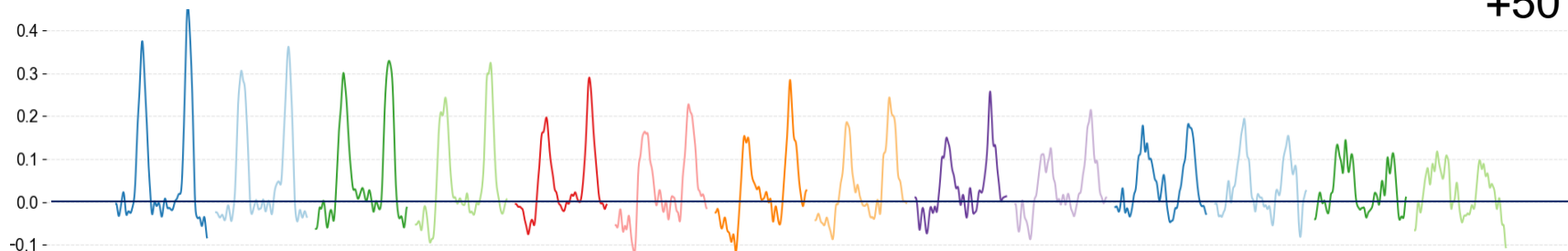
0 ps



+20 ps



+50 ps



**Thank you for your attention!**