

# THMP and Temperature Sensor Production

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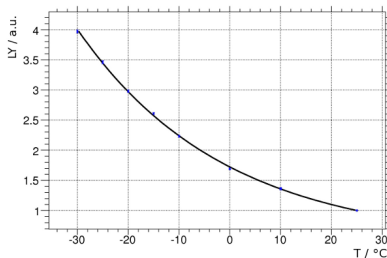
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# Why and How Do We Measure Temperatures?

PWO-II:  $LY$  depends on  $T$  with  $\frac{d(LY)}{dT} = 3\%/^{\circ}\text{C}$  at  $-25^{\circ}\text{C}$



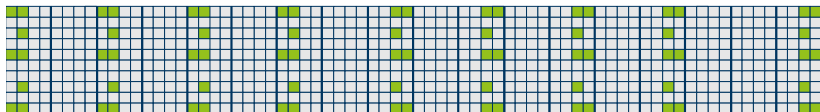
- Goal for  $\overline{\text{PANDA}}$ :  $\Delta T < 0.1^{\circ}\text{C} \rightarrow$  sensors with  $\sigma_T < 0.02^{\circ}\text{C}$
- $R$  vs  $T$  relation of platinum quite linear

$$R(T) \approx R(0^{\circ}\text{C})(1 + \alpha_{\text{Pt}} \cdot T), \quad \alpha_{\text{Pt}} = 3.89 \cdot 10^{-3} \text{K}^{-1}$$

- Accuracy for temperature sensors translates to accuracy for the THMP:  $\sigma_R \approx \frac{\partial R(T)}{\partial T} \cdot \sigma_T \approx 7.8 \text{ m}\Omega$

# Status of Temperature Sensor Production

- Need:
  - 482 temperature sensors designated for forward endcap
  - 1152 temperature sensors designated for barrel (72/slice)  
(Mainz is taking care of backward endcap)



positioning by Markus Moritz

# Status of Temperature Sensor Production

- Need:
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  - 1152 temperature sensors designated for barrel (72/slice)  
(Mainz is taking care of backward endcap)
- Status:
  - 613 temperature sensors produced
  - 545 temperature sensors calibrated (uptodate setup!)  
(64 shortcut / bad connection)
  - 83 high quality sensors provided for test slice (11 spare)
  - Adapter boards for test slice designed and printed,  
currently equipping with connectors

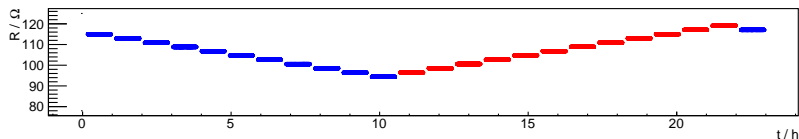


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- Keep running:
  - Sufficient amount of platinum wire bought and delivered
  - Boards (plugs) ordered
  - Inviting offers for copper coated polyamid foil (ultrathin wires)

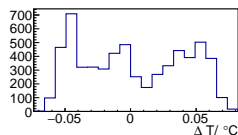
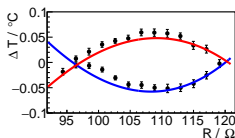
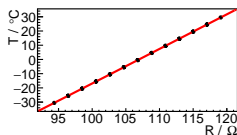
# Quality Assurance

- Data selection: Consider all data except first 10 minutes after change of temperature set value
- Split the data into two sets to respect hysteresis



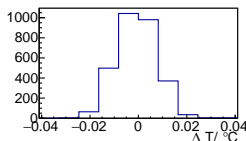
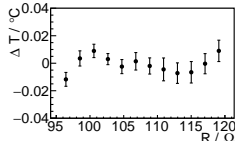
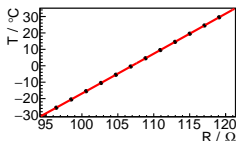
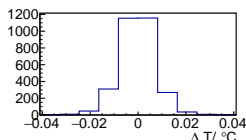
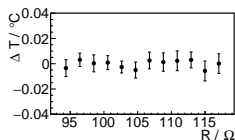
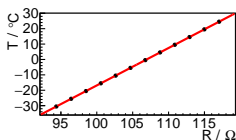
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# Quality Assurance

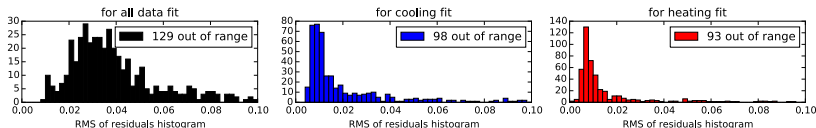
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- Consider the distance of each datapoint to the fitted function





# Quality Assurance

- Data selection: Consider all data except first 10 minutes after change of temperature set value
- Split the data into two sets to respect hysteresis
- Consider the distance of each datapoint to the fitted function
- Determine the RMS of the distribution



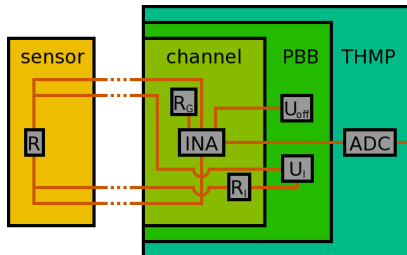
- 305 of 545 sensors (55%):  $\text{RMS} < 0.02$  for both subsamples

# Status of THMP Production

- Need:
  - 10 THMPs designated for forward endcap  
(74  $T$ -PBBs, 6  $p$ -PBBs)
  - 2 THMPs designated for barrel test slice  
(12  $T$ -PBBs, 4  $p$ -PBBs)
- Status:
  - 15 fully equipped and tested THMP-mainboards  
12 of which in cases
  - 92 fully equipped and tested  $T$ -PBBs
  - 25 fully equipped and tested  $p$ -PBBs
- Next steps:
  - Calibrate the THMPs (temperature dependent)  
→ 8 cot 24 h measurements per THMP

# THMP Concept

- 4-wire measurement
- constant current  $I = \frac{U_I}{R_I}$
- gain  $G = 5 + \frac{200 \text{ k}\Omega}{R_G}$
- offset voltage  $U_{\text{off}}$
- ADC conversion factor  $C$



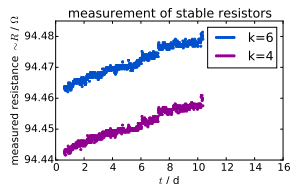
$$(R \cdot I \cdot G + U_{\text{off}}) \cdot C = R \cdot \underbrace{I \cdot G \cdot C}_m + \underbrace{U_{\text{off}} \cdot C}_n = N$$

→  $\sigma_R$  corresponds to 3.5 ADC channels for optimized values of  $U_I$ ,  $R_I$ ,  $R_G$  and  $U_{\text{off}}$

# Drift

! There was an additional PBB-wide drift of unknown origin ( $t$ )!

- constant current  $I_k(T, t) = \frac{U_I(T, t)}{R_{I, k}(T)}$
- gain  $G_k(T) = 5 + \frac{200 \text{ k}\Omega}{R_{G, k}(T)}$
- offset voltage  $U_{\text{off}}(T, t)$
- ADC conversion factor  $C$



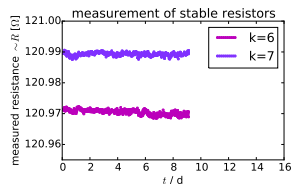
$$R_k \cdot \underbrace{I_k(T, t) \cdot G_k(T) \cdot C}_{m_k(T, t)} + \underbrace{U_{\text{off}}(T, t) \cdot C}_{n(T, t)} = N_k(T, t)$$

# Drift

! There was an additional PBB-wide drift of unknown origin ( $t$ )!

✓ With the new configuration there is no drift anymore!

- constant current  $I_k(T, t) = \frac{U_I(T, t)}{R_{I, k}(\bar{T})}$
- gain  $G_k(T) = 5 + \frac{200 \text{ k}\Omega}{R_{G, k}(\bar{T})}$
- offset voltage  $U_{\text{off}}(T, t)$
- ADC conversion factor  $C$



$$R_k \cdot \underbrace{I_k(T, t) \cdot G_k(T) \cdot C}_{m_k(T, t)} + \underbrace{U_{\text{off}}(T, t) \cdot C}_{n(T, t)} = N_k(T, t)$$

→ No reference resistors needed!

# Summary and Outlook

- ✓ Almost all produced temperature sensors calibrated
- ✓ 305 approved temperature sensors ( $\approx 50\%$ )
  - ! Improving the fitting to temperature sensor data will most probably increase approved share
  - ! Study hysteresis effect
- ✓ THMP hardware is ready!
- ✓ No drift visible anymore!
  - ! Next: Temperature dependent calibration of all THMPs

Questions? Comments?