

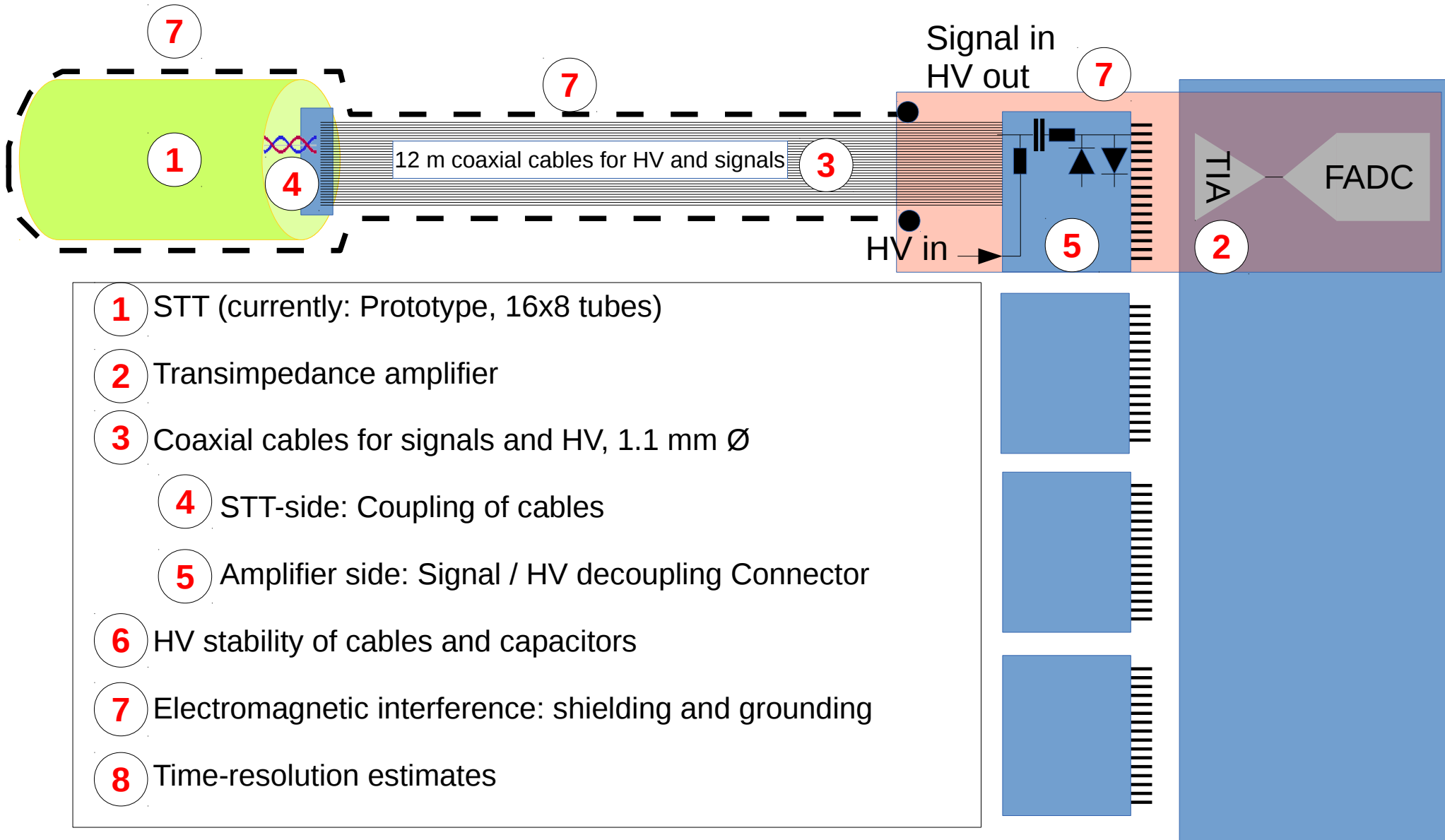
Remote Electronics and HV for the PANDA STT Component- and Prototype Studies

PANDA CM, December 9, 2014

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Advantages expected:

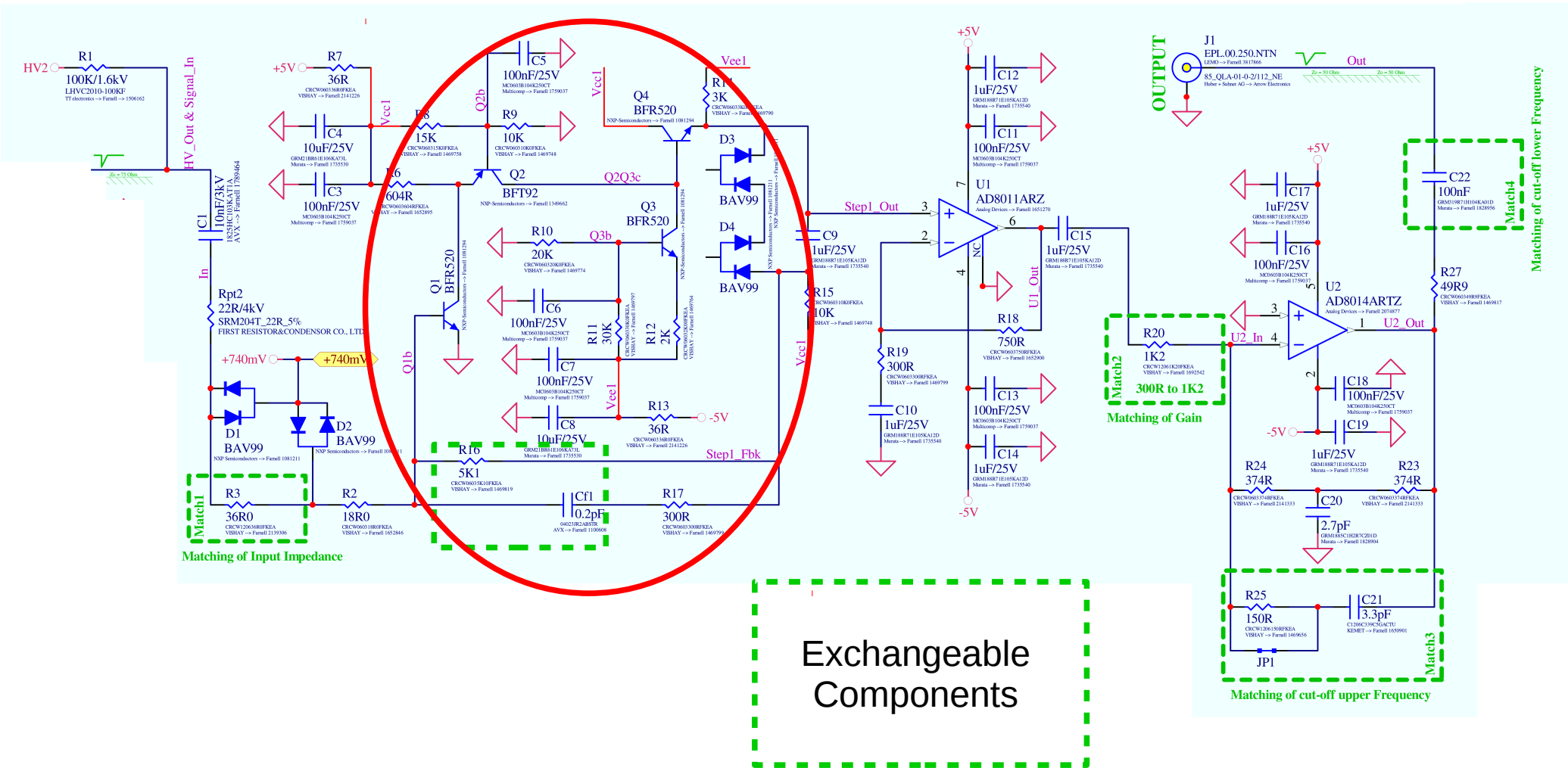
- No space problem
- No heat release
- No additional cables for HV and LV needed
- No radiation damage
- All components possibly subject to failure are accessible outside the detector
- Broken tubes in the STT can be decoupled individually from HV

To be demonstrated:

- HV Stability
- Protection against induced parasitic signals ("EMI")
- Still good time resolution
- Technical solutions exist

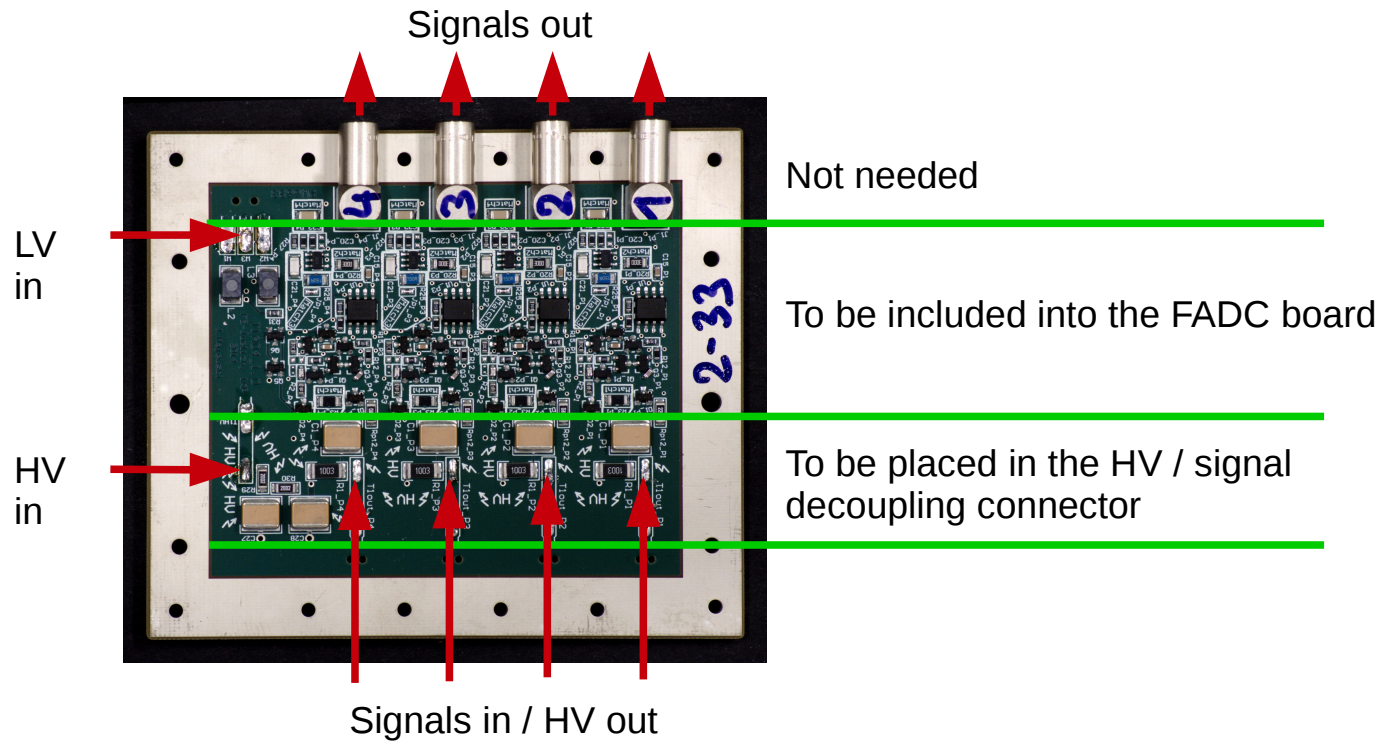
Low-Noise Transimpedance Amplifier

- To be included into the FADC board
- New design needed
- Low-noise input stage with discrete components
- Components controlling input impedance, gain and shaping easily exchangeable



Low-Noise Transimpedance Amplifier

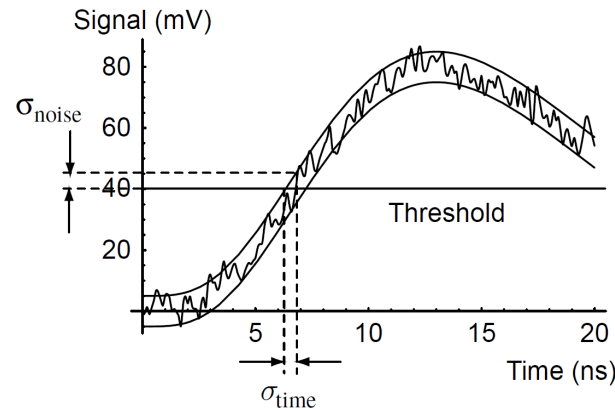
- Successfully used for STT read-out in recent beamtimes



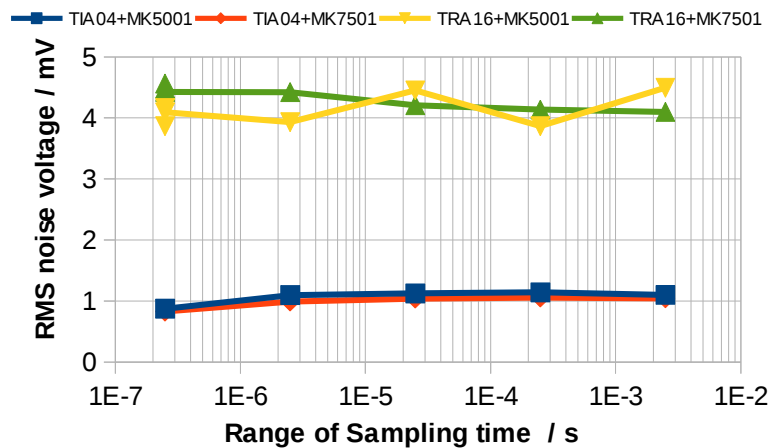
Performance of Transimpedance Amplifiers

Improvement of the time resolution with a low-noise amplifier

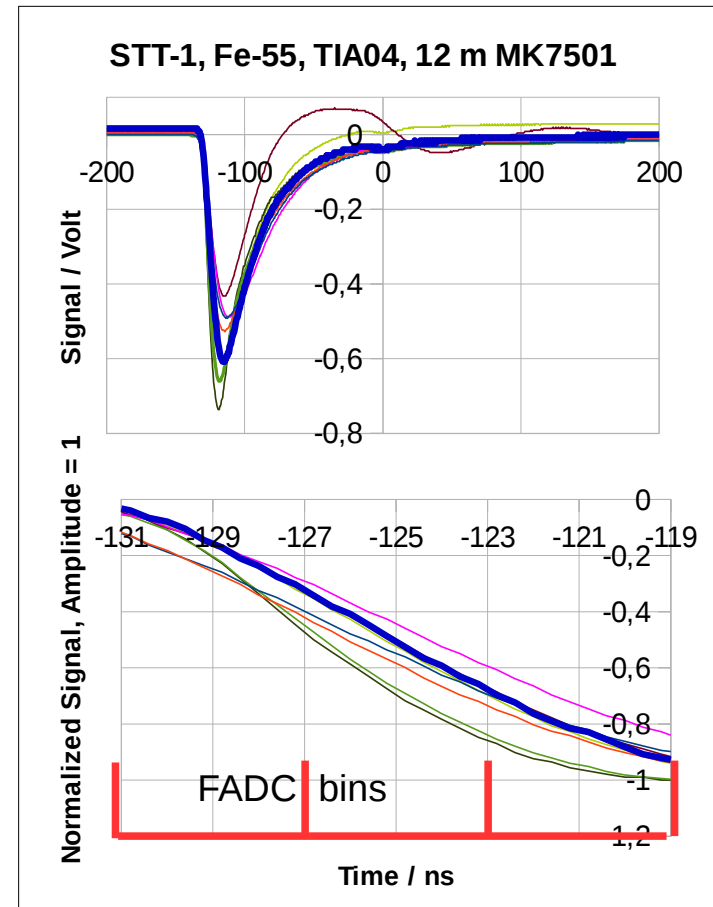
$$\sigma_{\text{time}} = \sigma_{\text{noise}} / dV/dt$$



Noise of TIA04 and TRA16 with 12 m long input cables



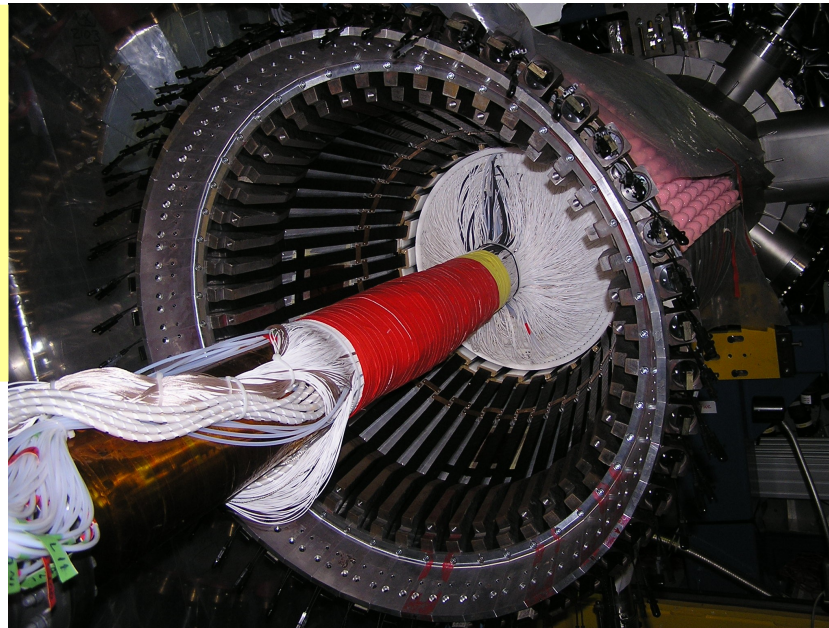
Signal shapes optimized for analysis with the FADC



Common Cables for Signals & HV

WASA@COSY:

Filotex 75 Ω
1.2 mm \varnothing
5 m long
operating voltage
1400 V over 8 years

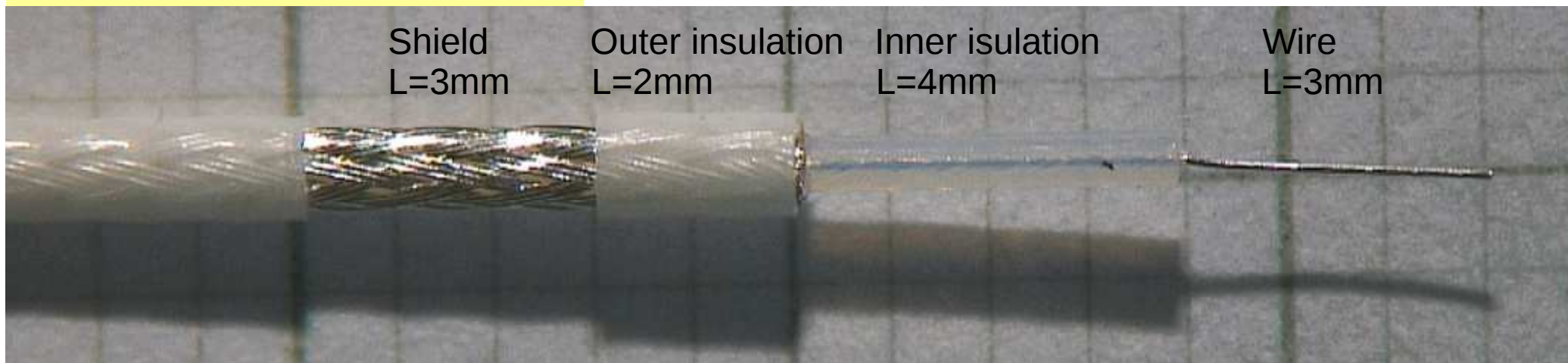


PANDA STT Demonstrator:

MK7501
1.1 mm
12 m long
HV test at factory: 1000 V
routinely operated at 1900 V
Lab tests: stable at 4 kV

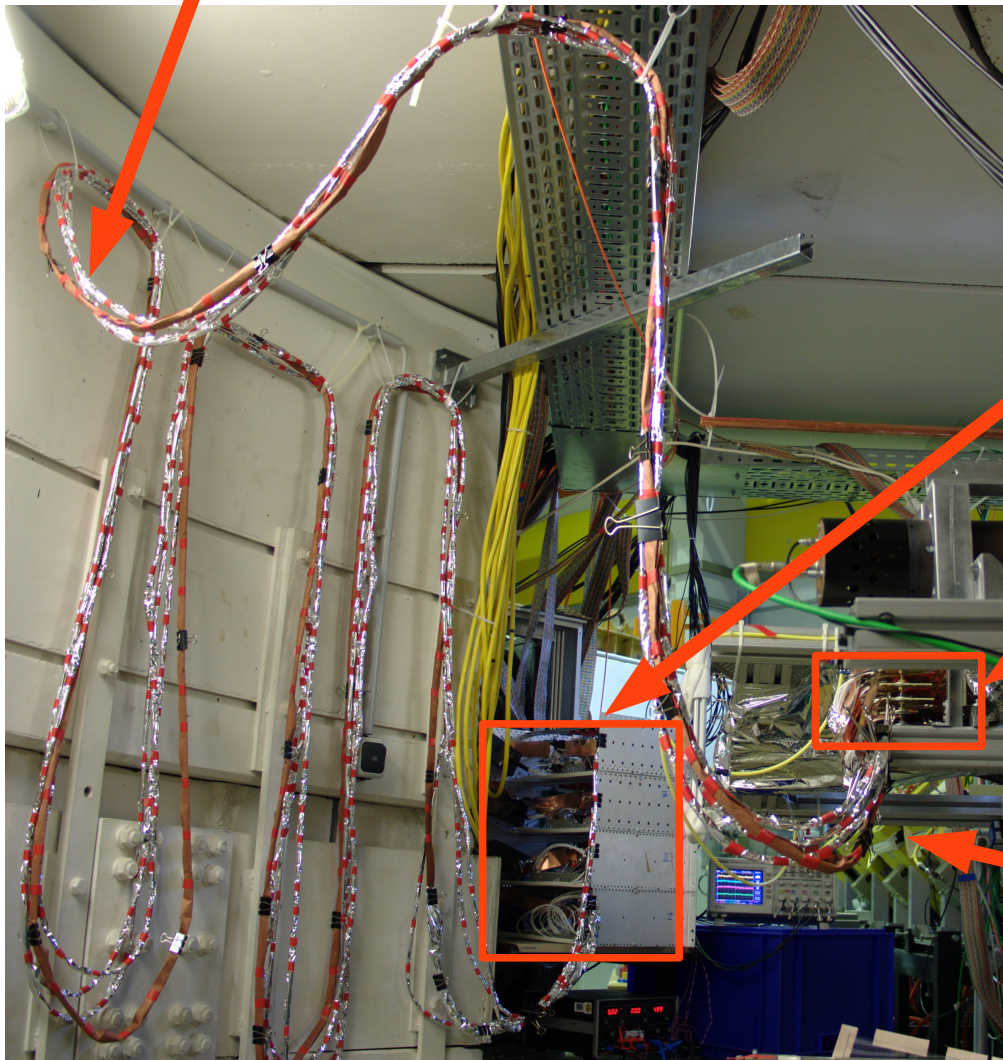
Don't be a slave of ratings:

3M Twisted Pair Flat Cable
Voltage Rating:
USA: 300V Canada: 150V EU: <50V
tested up to 7 000 Volts !



Cable Connection between the STT and the amplifiers during in-beam tests

Bunches with 32
coaxial cables
Shielding: 12 μm
Mylar + 2x50 nm Al



Crates with preamplifiers

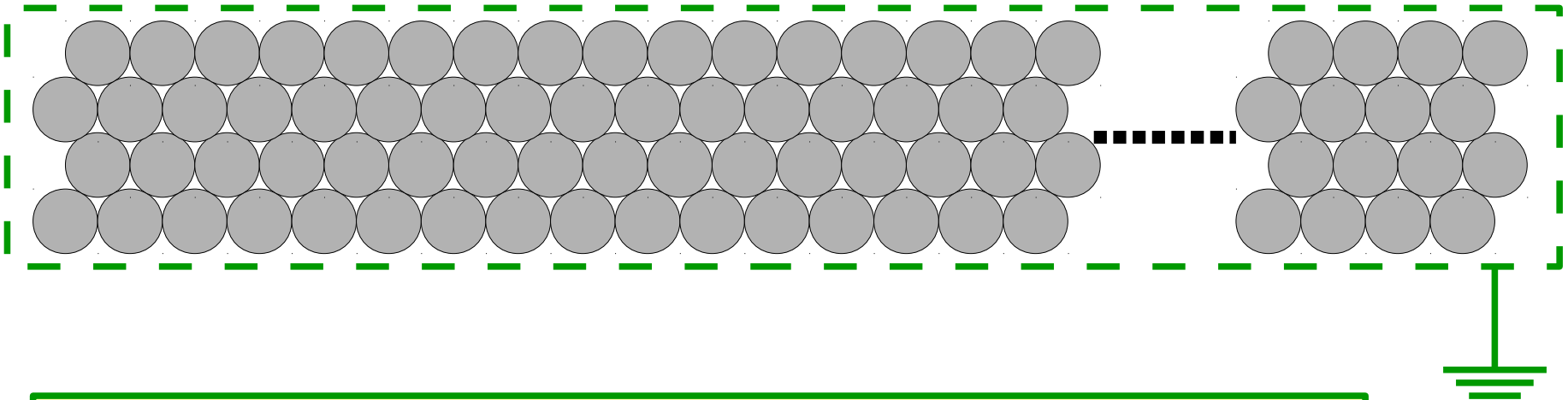
Connector end of the
STT prototype

Beamline

Packing of Signal / HV Cables

4500 cables MK7501
Total Cross section = 4720 mm²
for dense packing

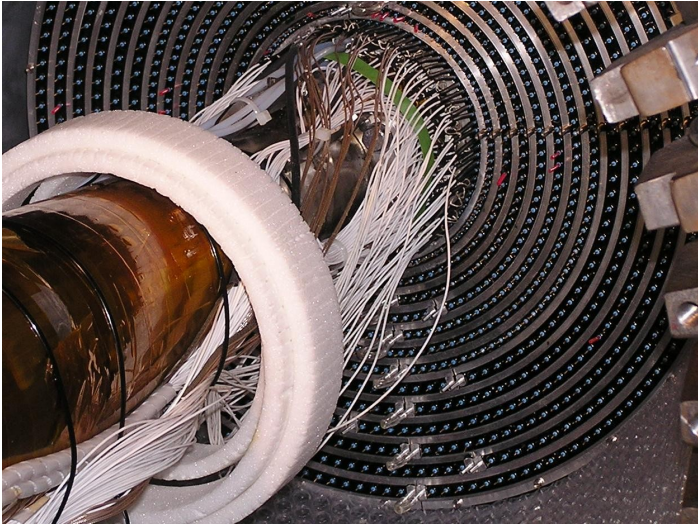
Shielding material
e.g.
12 μm Mylar
+ 2 * 50 nm Al



The shielding around all cables has to extend
from the STT to the remote preamplifier
without any weak contact in between

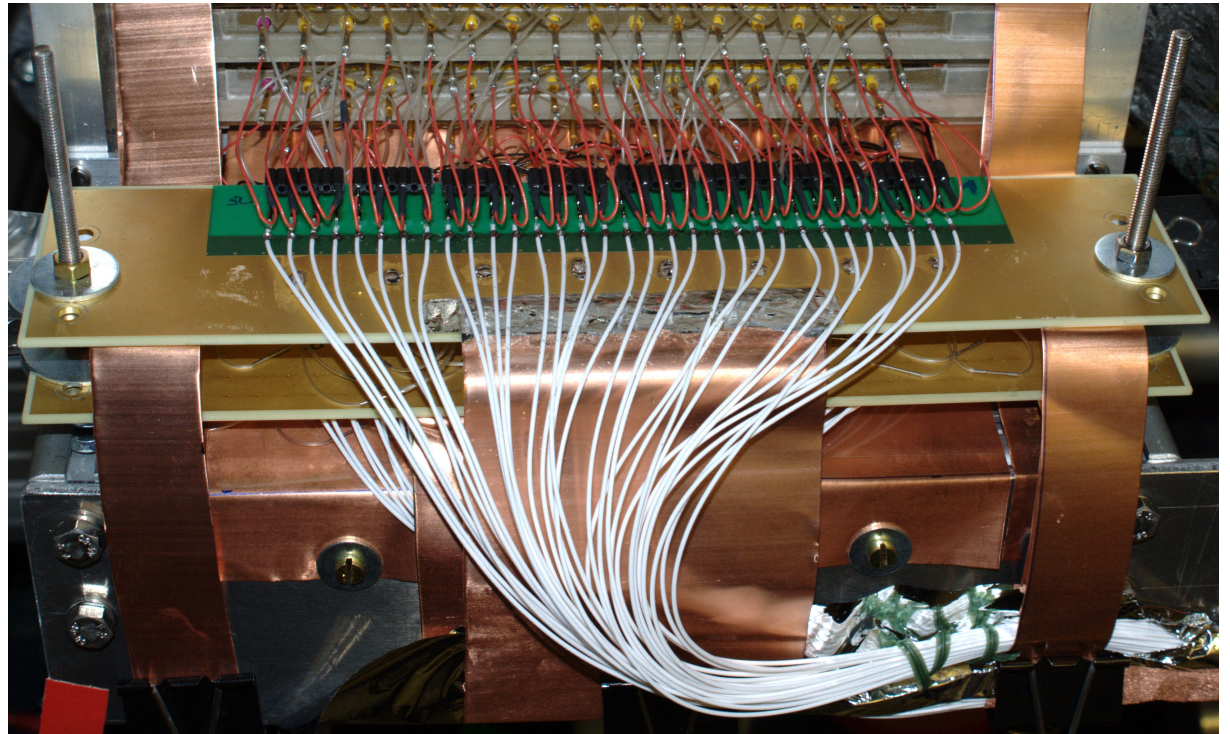
It has to ensure that
RF voltage differences
between the detector and the preamplifier ground
are $< 10 \mu\text{V}$

Cable Connection to Straw Detectors



WASA@COSY

Coaxial cables are individually plugged onto the central straw detector



Prototype for PANDA @COSY

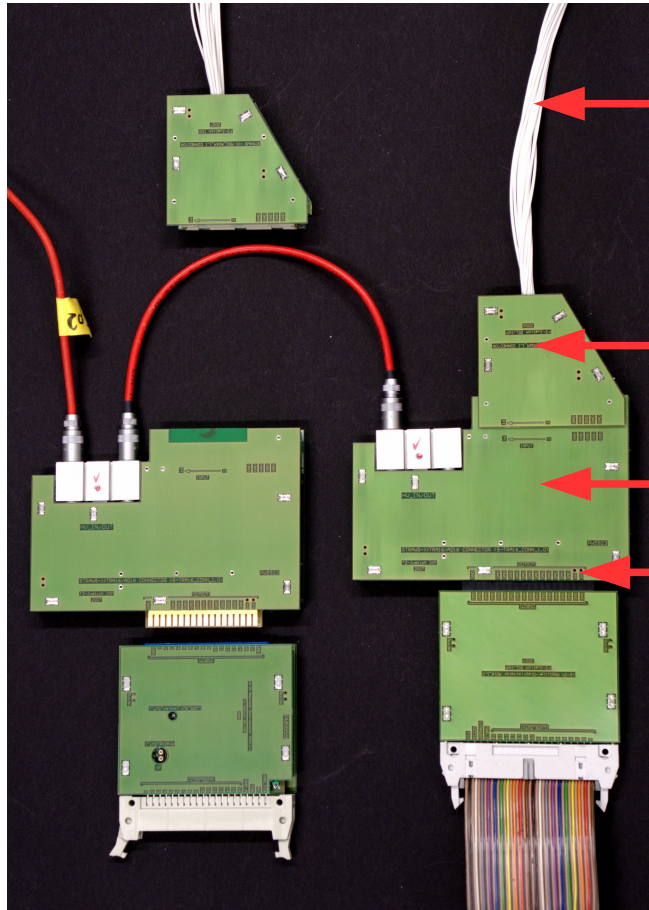
- 32 Coaxial cables are held by a PCB
- Short cables from the straws with multiple connector
- Ground connection with the body of the detector via Cu strips

To be changed:

- Short connecting cable will be twisted pair or coax
- Everything can become smaller

Signal and HV / (De-)coupling in Front of the Amplifier / Flash-ADC

WASA@COSY (and ANKE@COSY):



Cables coming from the straws

Connector: HV in and Signal out

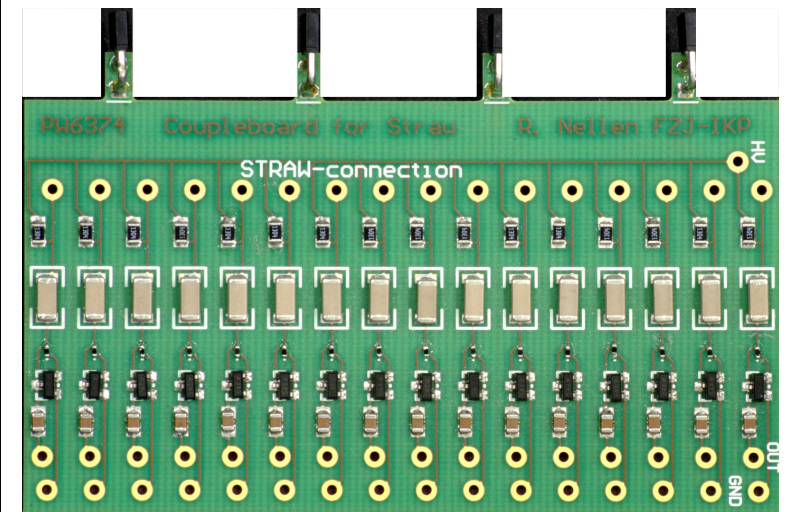
Both modules to be unified

This end to be tailored to the FADC input

Amplifier / Discriminator

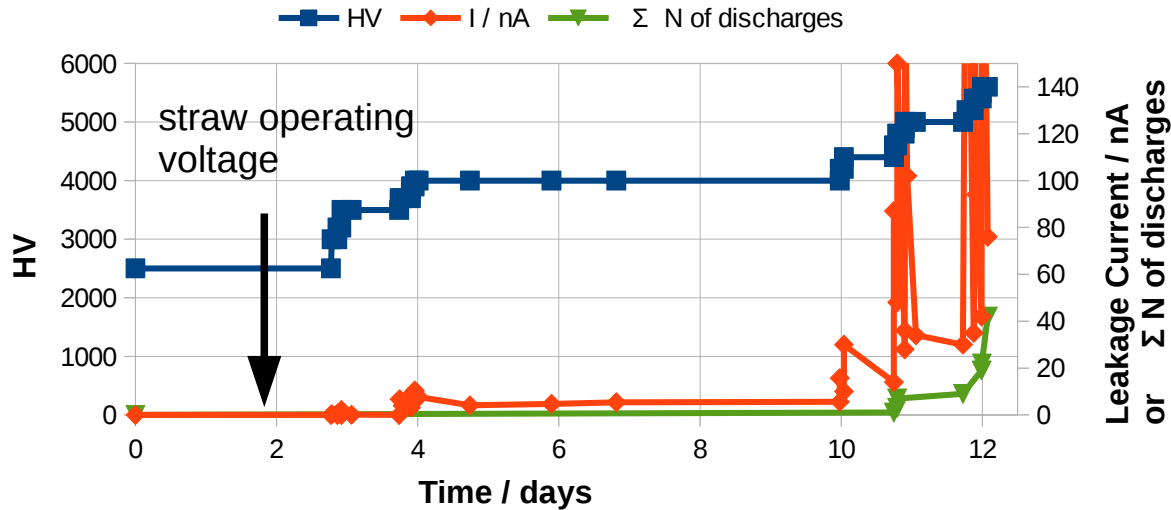
Prototype for the STT

To be built into the Signal / HV connector



HV Stability of Cables and Capacitors

HV Stability of MK7501 Cables



How close are we to the limit of HV stability ?

Are components destroyed at overvoltage ?
Is the effect of discharges reversible ?

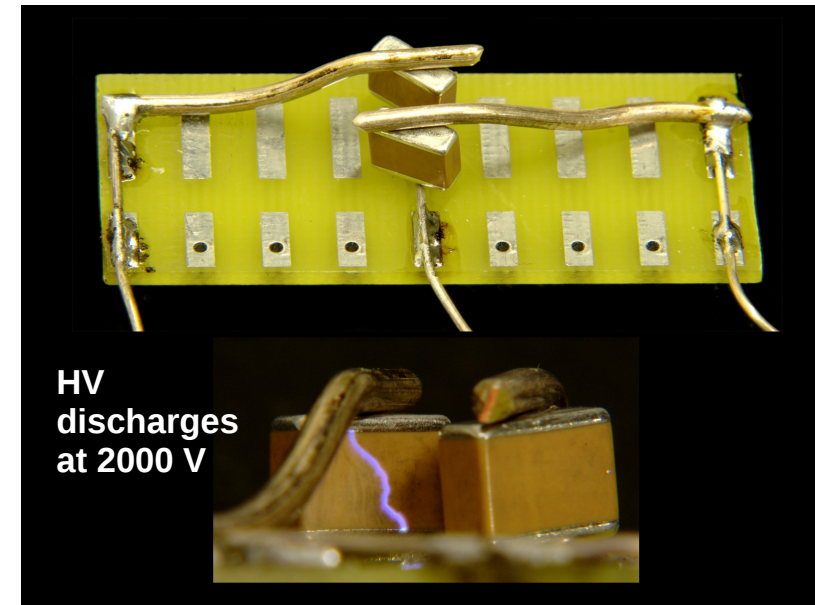
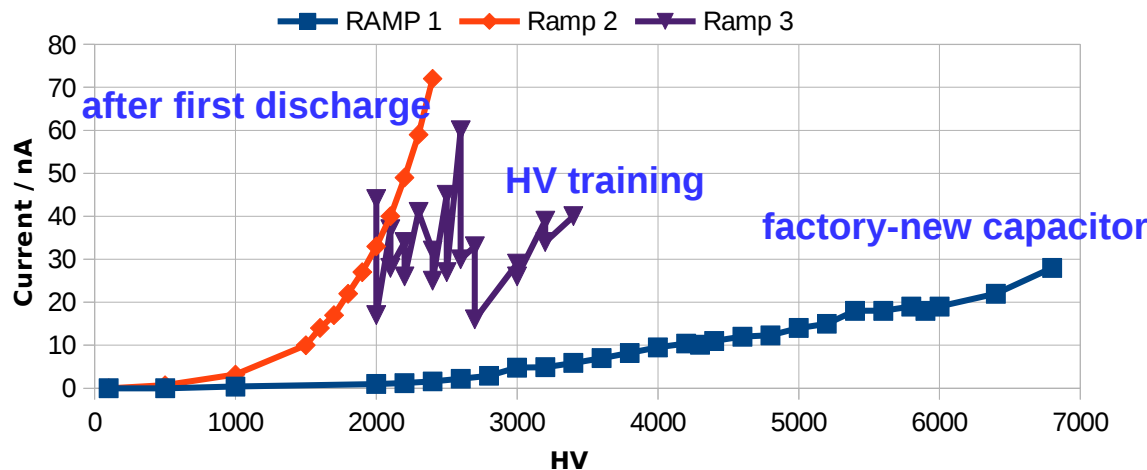
Cables:

- Robust also beyond limiting voltage

Capacitors:

- Sparking sometimes 1000 V below limit
- Depends on surface cleanliness
- Partial recovery after HV training

Leakage Current of HV Capacitors

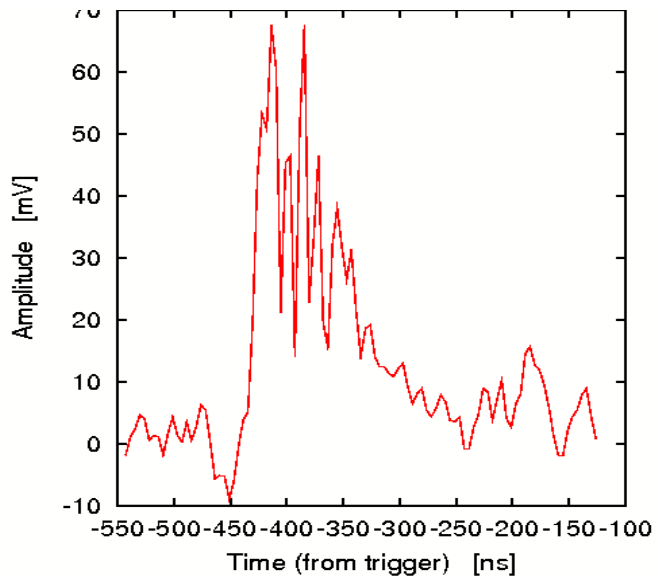


Electromagnetic interference: Parasitic signals in straw chambers and application of countermeasures

EMI inside and near PANDA ?

Usual sources:
PMs, signal cables, clock signals, HV oscillators ...

EMI in a straw chamber during a beam time



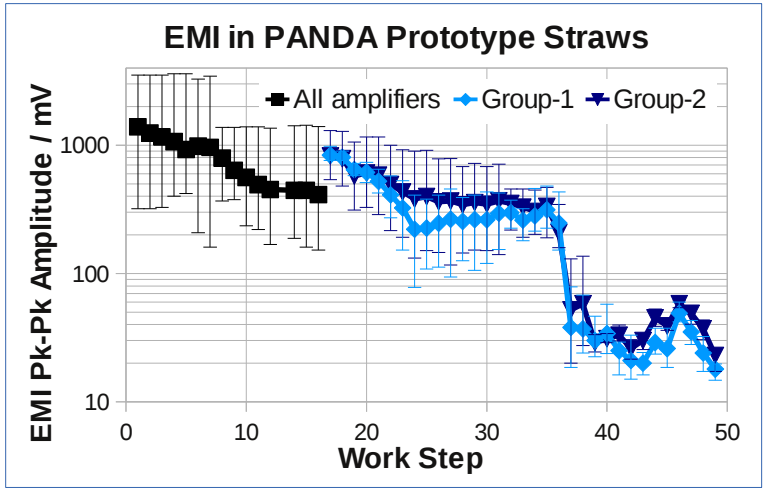
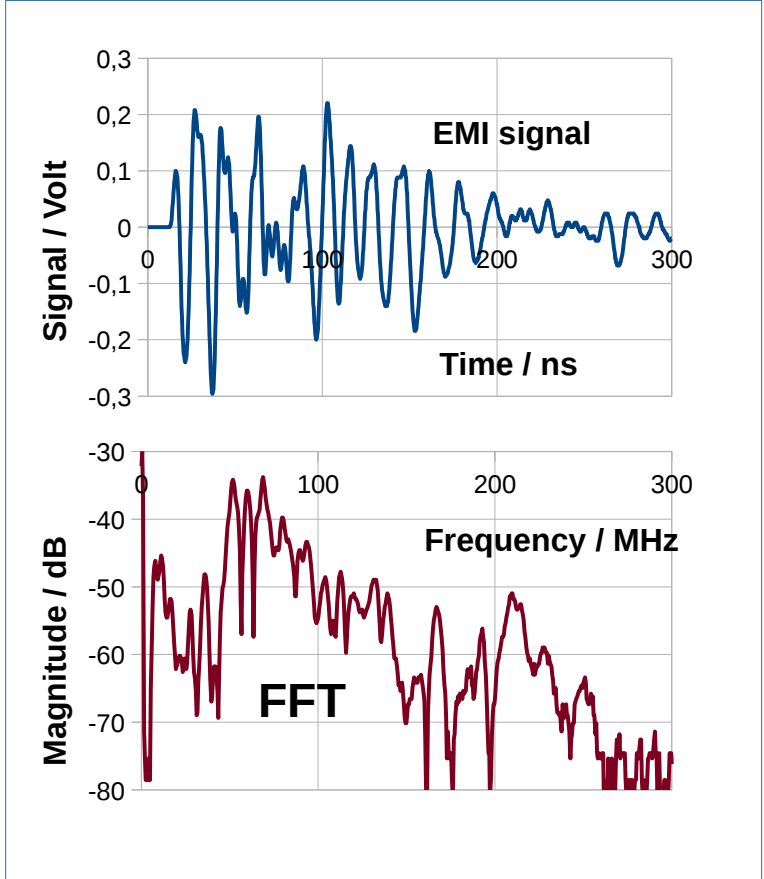
EMI countermeasures

in the presence of a reproducible RF field

Shielding of

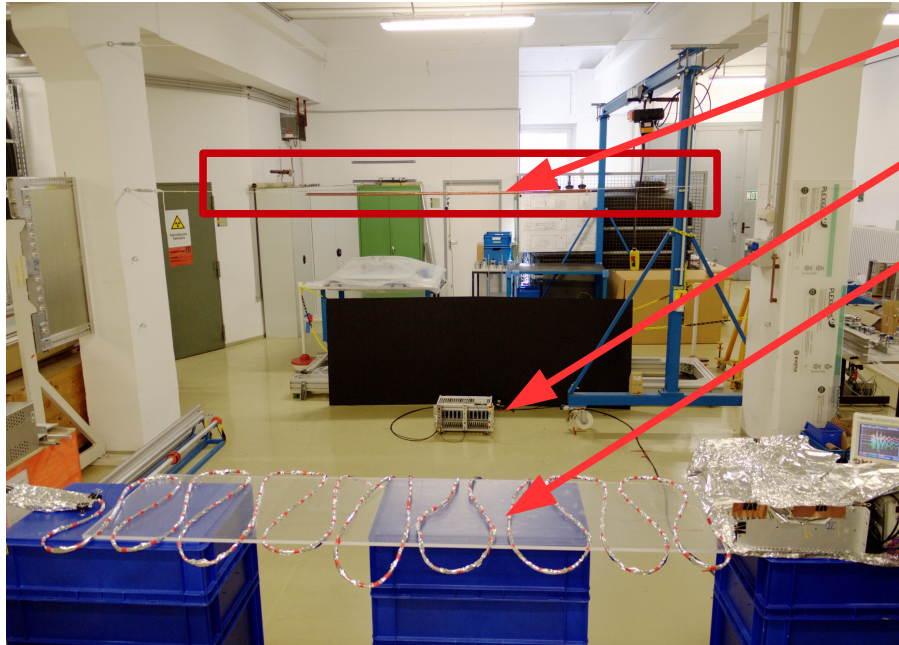
- STT
- Cables
- Amplifiers

with 6 μm Al foil



Electromagnetic Interference in Straw Detectors

EMI test area for detectors and electrical components

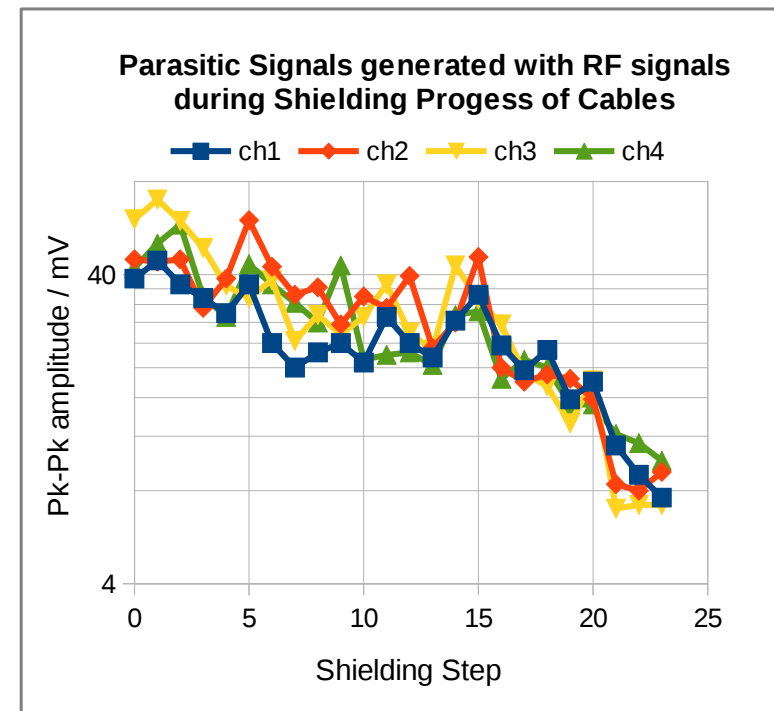


Transmitter dipole

Pulse generator

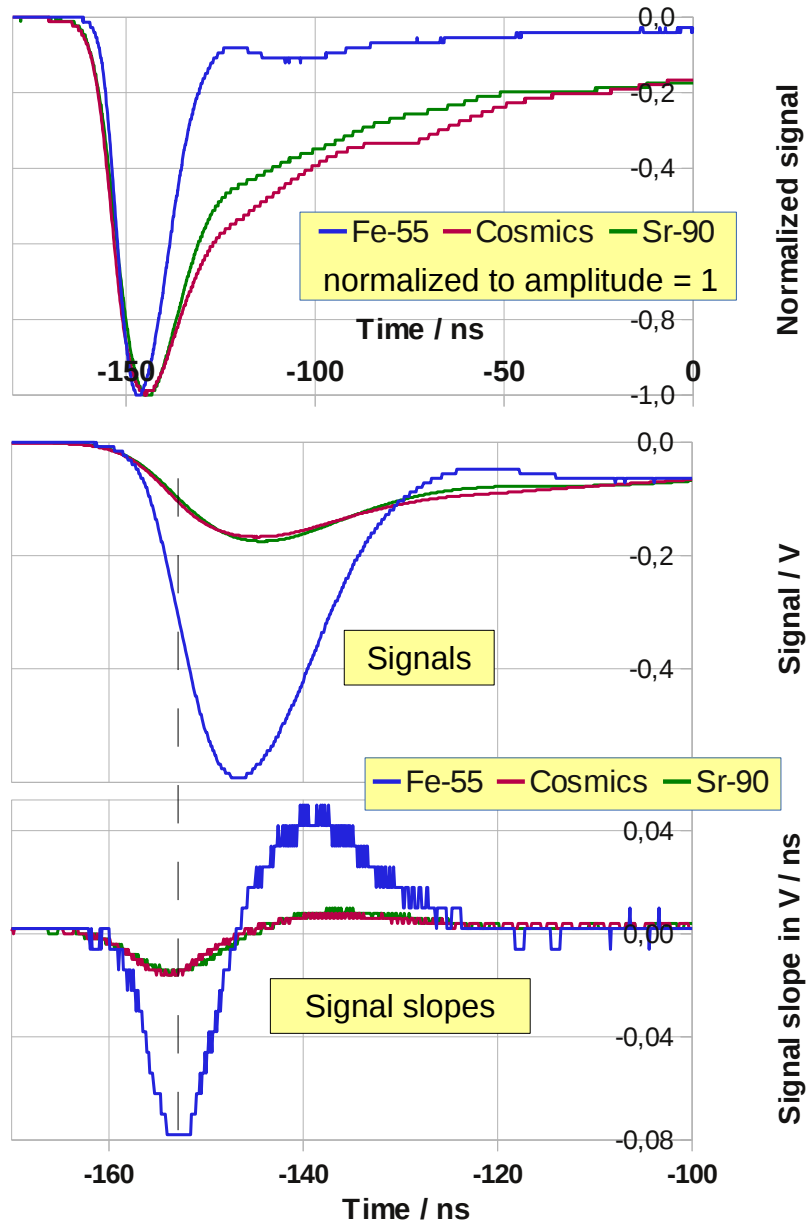
Object under test

Reduction of induced signals during shielding progress



Fe-55 signals as a model for average pulse parameters of track signals

Fe-55, Sr-90 and Cosmics Signals averaged over 128 events

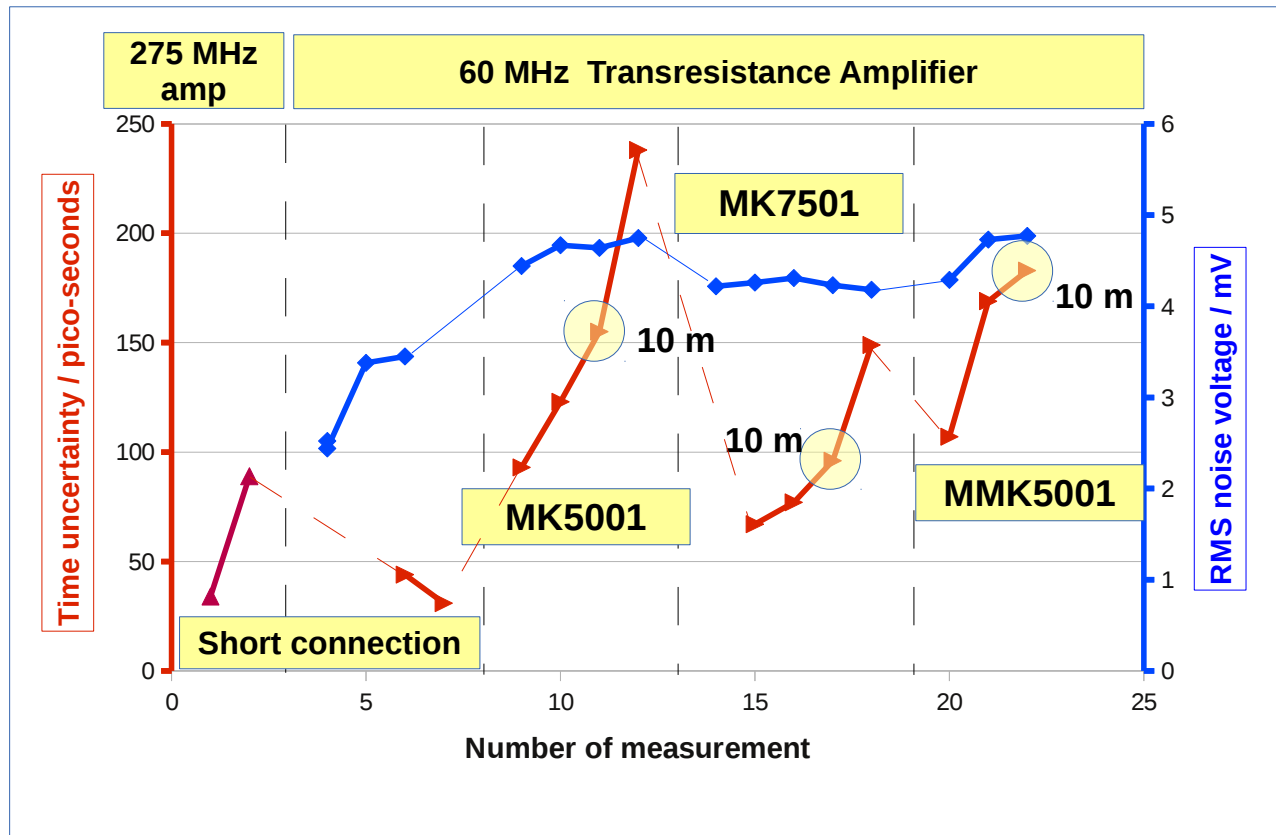


Time resolution

	<u>Amplit.</u> [mV]	<u>Slope</u> [mV / ns]	<u>Time uncertainty</u> [ns]
RMS noise	3.5		
Fe-55	590	80	0.044
Cosmics	168	18	0.19
Sr-90	176	18	0.19

Estimated electronical time uncertainty

(previous amplifier, no active timing, close (50 cm) to straw chambers or with 5 / 10 / 20 m cable)



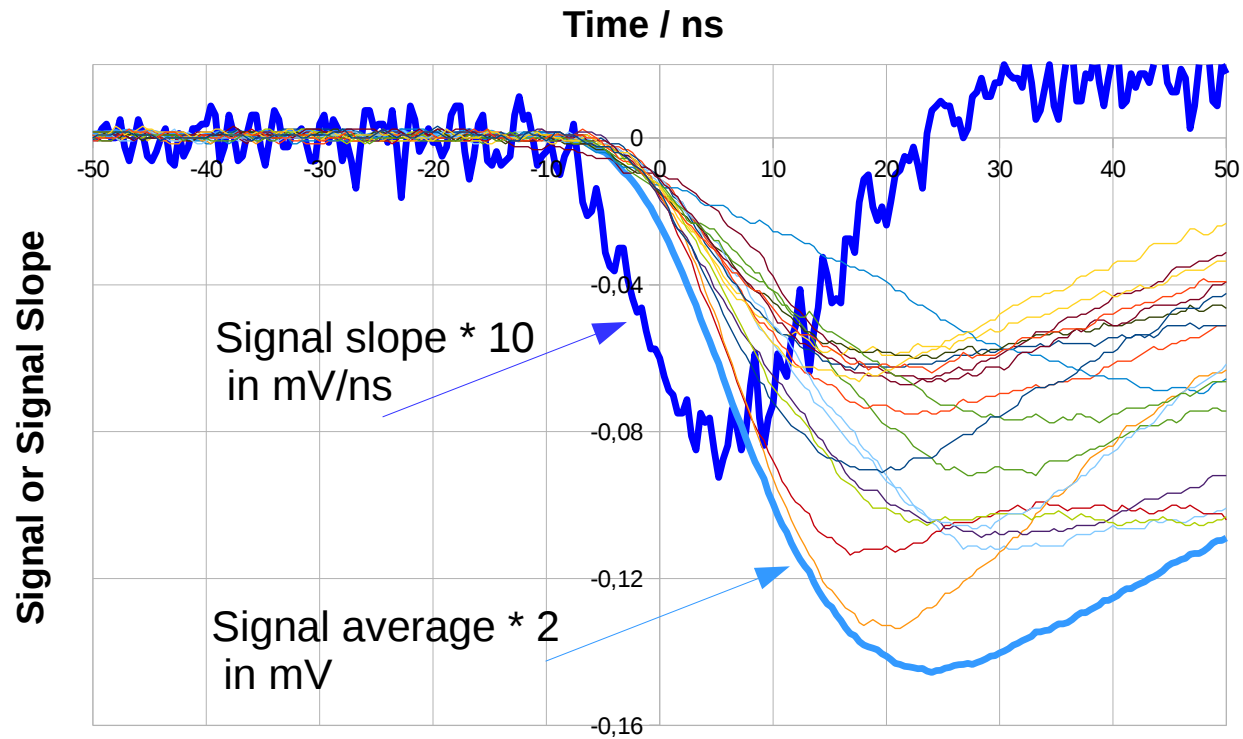
Assumption: timing is derived from the steepest slope, there is no walk

Fe-55	short connection	44 ps
Sr-90 or cosmics	Normalization: * 4.4	190 ps
Reduction of gas amplification	$8 \cdot 10^4 \rightarrow 5 \cdot 10^4$	300 ps
Sr-90 or cosmics	thin cable, 10 m long	680 ps ($\triangleq 23 \mu\text{m}$)

Signals with proton beam

COSY beamtime October 2014:

Protons, 1.0 GeV/c, Ar/CO₂=90/10, 1800 V,
Remote low-noise amplifier



**Estimated time resolution
including all contributions in the analog chain
= 100 ps (Δ 3 μ m)**

The STT operated with remote electronics fulfills TDR specifications !

- **128 channels with low-noise amplifier successfully tested under beam conditions**
- **Shaping optimized for STT signals**
- **1.1 mm \varnothing cables are safe under HV**
- **Efficient protection against Electromagnetic Interference**
- **Spatial resolution near 150 μm achieved**

Next steps:

- **Design, production and tests of the HV / Signal decoupling connector**
- **Test of this with the current electronics**
- **Prototype of the new FADC including the low-noise amplifier**
- **Measurements at the STT demonstrator at COSY**
- **Operation at PANDA**