

# Options for the Placement of the STT Front-End Electronics and the Selection of Transmission Cables and Consequences for the Time Resolution

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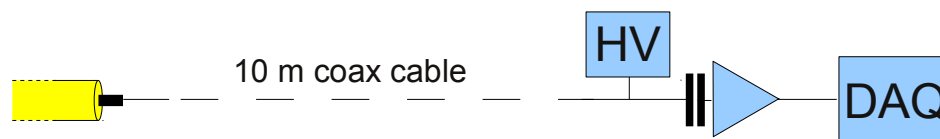
## Main options for read-out of the STT:

### The Krakow ASIC

To be installed inside PANDA

### The Jülich Fast Flash-ADC system

All electronics outside PANDA:



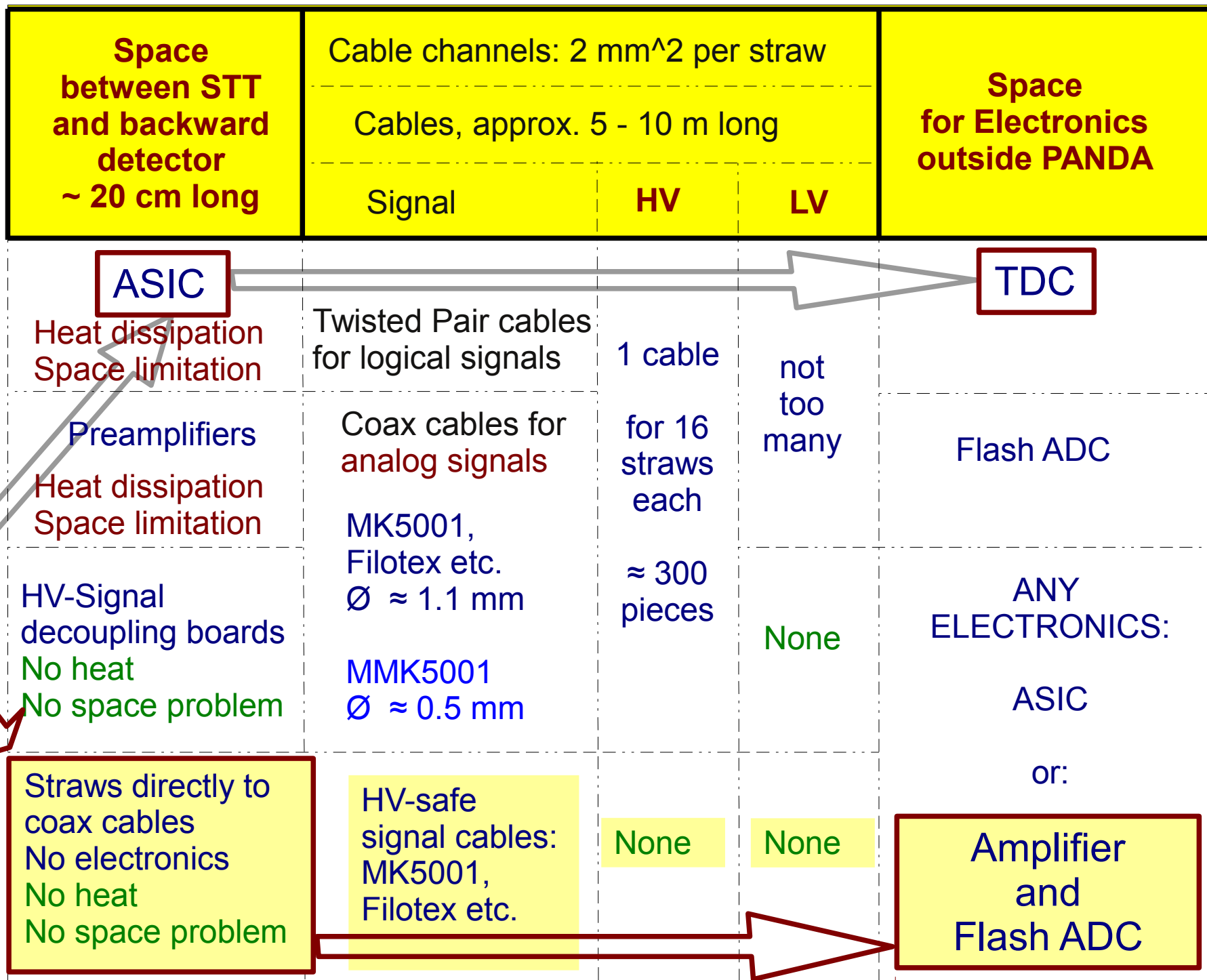
Time and charge information from real-time signal analysis

**Does electronics significantly limit the time resolution of the straw detector ?**

### Experimental techniques:

No complex tracking experiment

**Electronical time uncertainty estimated from noise and signal shape**



## Requirement and specifications as given in the TDR

- Single-hit spatial resolution in x and y:  $< 150 \mu\text{m}$   
(Assuming linear relationship and max. drift time of 200 ns: Time resolution  $<< 6 \text{ ns}$ )
- ASIC (TDR): 1-2 ns
- TDC resolution: 1 ns
- Gas amplification max.  $5 \cdot 10^4$  for limitation of ageing  
(This poses also a limit for the time resolution)

## Conditions during the measurements

- A single straw tube
- 80% Ar, 20% CO<sub>2</sub>
- HV = 2000 V
- Gas amplification  
derived from fast Fe-55 signal component  $\sim 2 \cdot 10^4$   
including ion tail  $\sim 8 \cdot 10^4$
- Source of events: Mainly Fe-55      Scaling to Cosmics and Sr-90 signals

## Electronic equipment

- TRA16 current amplifier (Working horse during our previous in-beam measurements):

Input impedance	= 96 $\Omega$	(to be optimized for cables)
Current gain	= 380	
Bandwidth	= 60 MHz	
Rise time for delta pulses	= 5 ns	
Peaking time	= 8 ns	
RMS noise voltage	= 2.5 mV	
ENC	= 5600 e-	

- Fast amplifier (275 MHz bandwidth) for exploring the limits of the detector
- 200 MHz digital oscilloscope

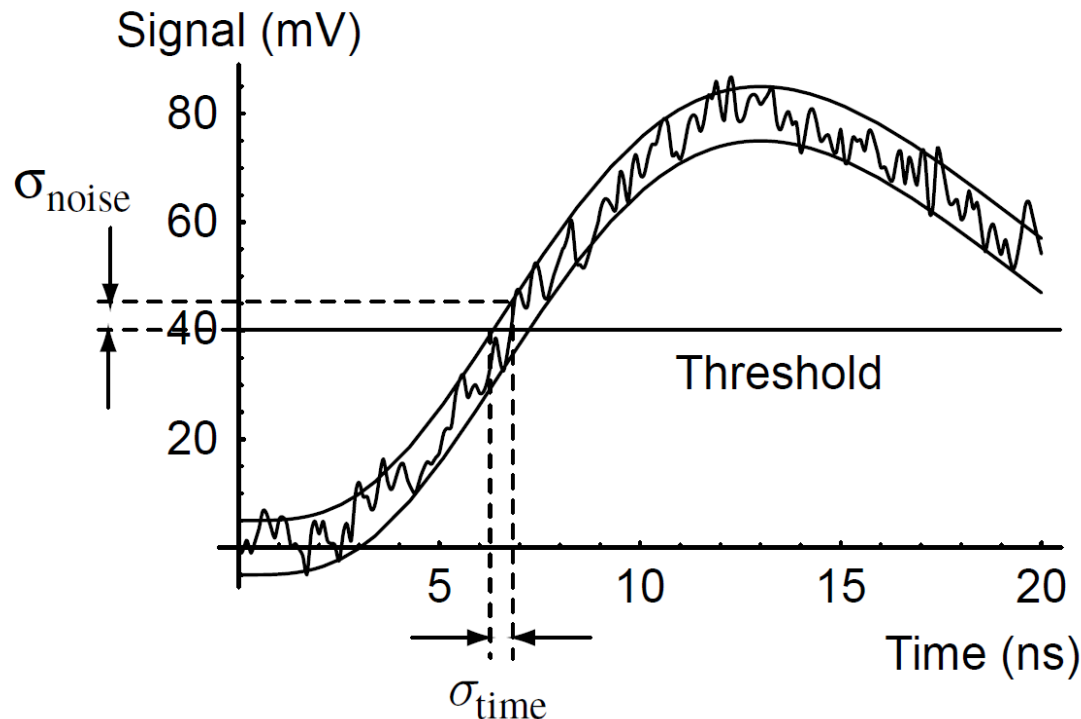
## Measurements

- Signals and noise voltage
  - Transmission of initial signals through long, thin cables
  - The role of impedance matching between straw and amplifier
- Electromagnetic interference
  - This appears often unexpectedly and spoils the detector performance

## What do we learn from the signal shape and the noise magnitude ?

The uncertainty of the determination of the arrival time of a signal is limited by the **slope of the leading edge** and the **noise voltage**:

$$\sigma_{\text{time}} = \sigma_{\text{noise}} / dV/dt$$

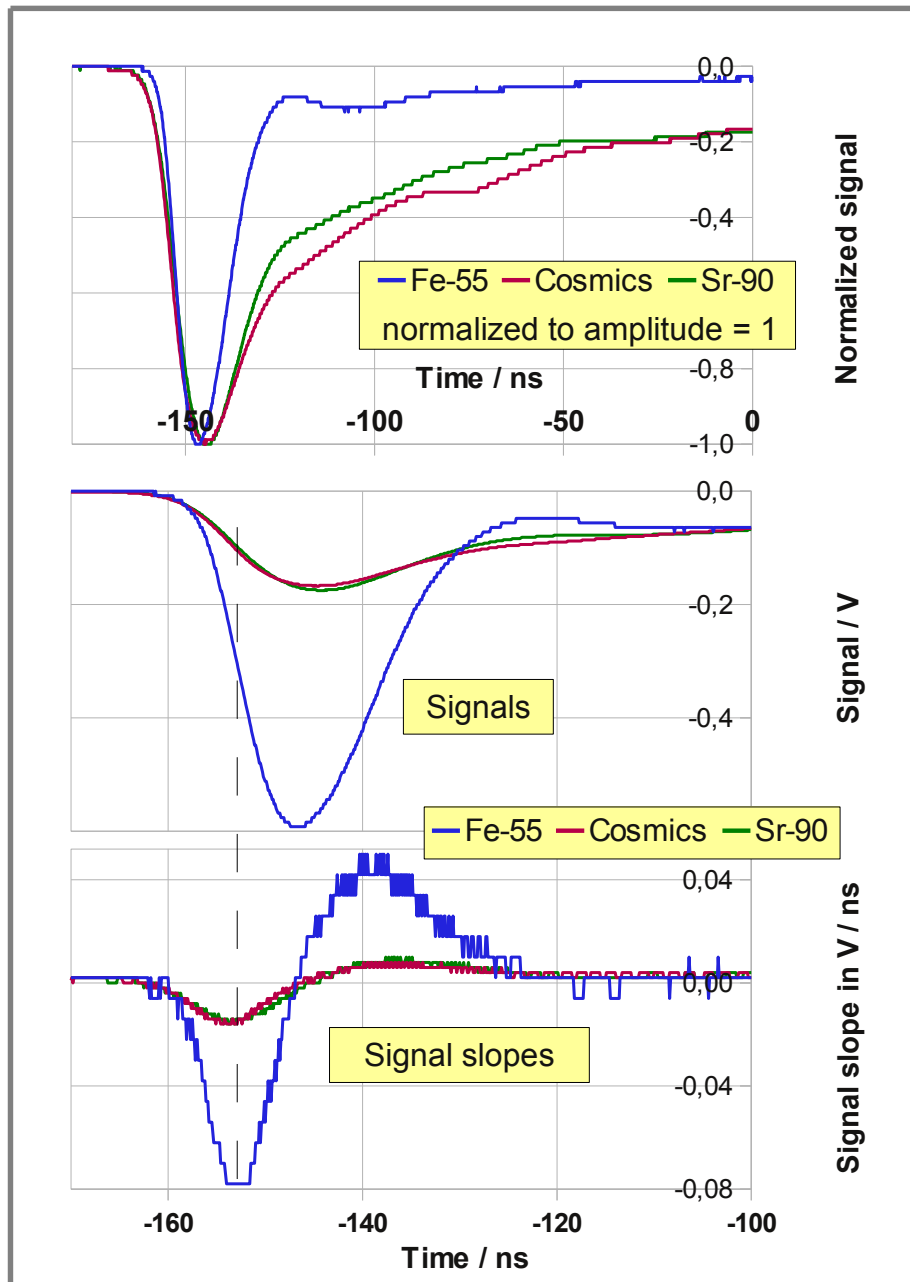


This noise is an intrinsic feature of the system.

Not to be confused with induced parasitic signals (EMI, see later). These have to be reduced with technical measures.

Fixed-number statements about the resolution of a timing system are not possible  
The timing resolution is usually strongly amplitude dependent

# Fe-55 signals as a model for average pulse parameters of track signals



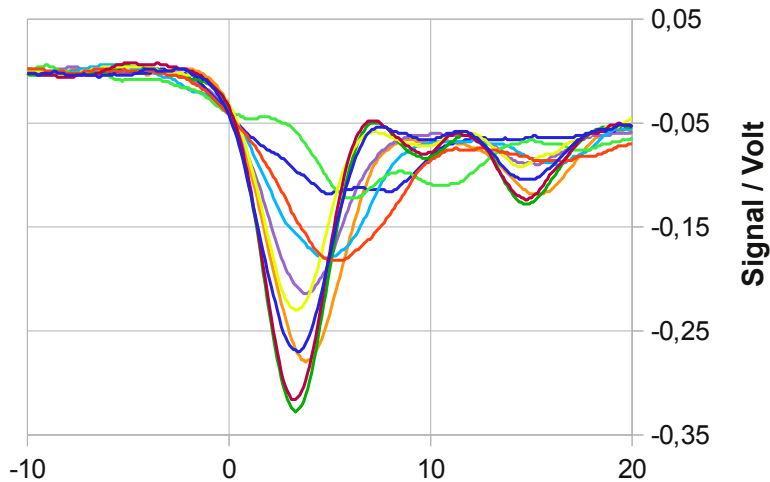
Signals averaged over 128 events

	<u>Amplit.</u> [mV]	<u>Slope</u> [mV / ns]	<u>Time uncertainty</u> [ns]
RMS noise	3.5		
Fe-55	590	80	0.044
Cosmics	168	18	0.19
Sr-90	176	18	0.19

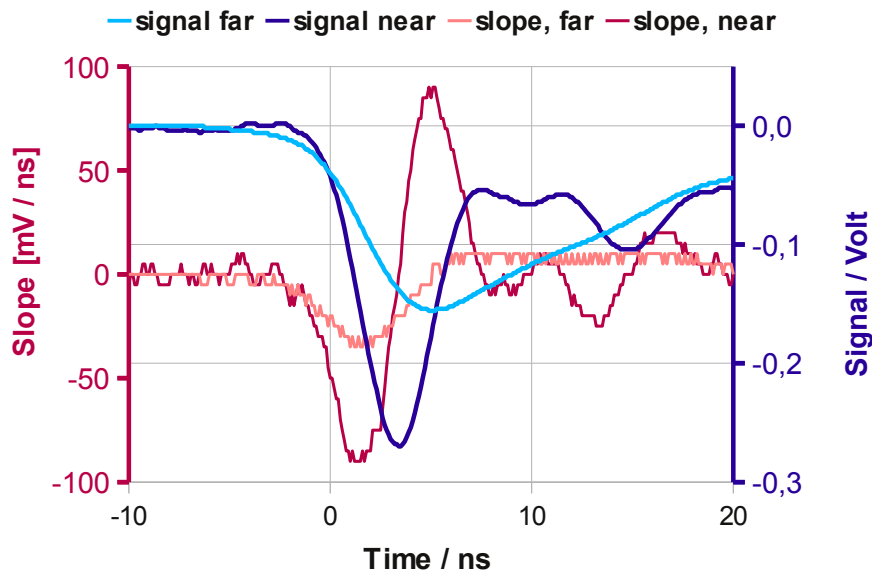
# How fast do amplifiers have to be ?

## The only application of a very fast (275 MHz bandwidth) amplifier

STT-1, Fe-55 source at the amplifier side



STT-1 Fe-55 Signals and signal slopes



- Fe-55: Absorption of 6 keV x-rays
- Well localized cluster of  $\sim 200$  electrons.
- A single signal component is expected

### Measured signal rise times / ns:

near end  $5.7 \pm 2.7$

far end  $6.5 \pm 2.7$

Amplifier response  $< 1.3$  ns

### Conclusions:

Signal shapes are defined by

- the physics of signal generation
- signal damping during passage of the straw
- amplifiers need not be very fast

### Estimated time uncertainty:

Source position: far end

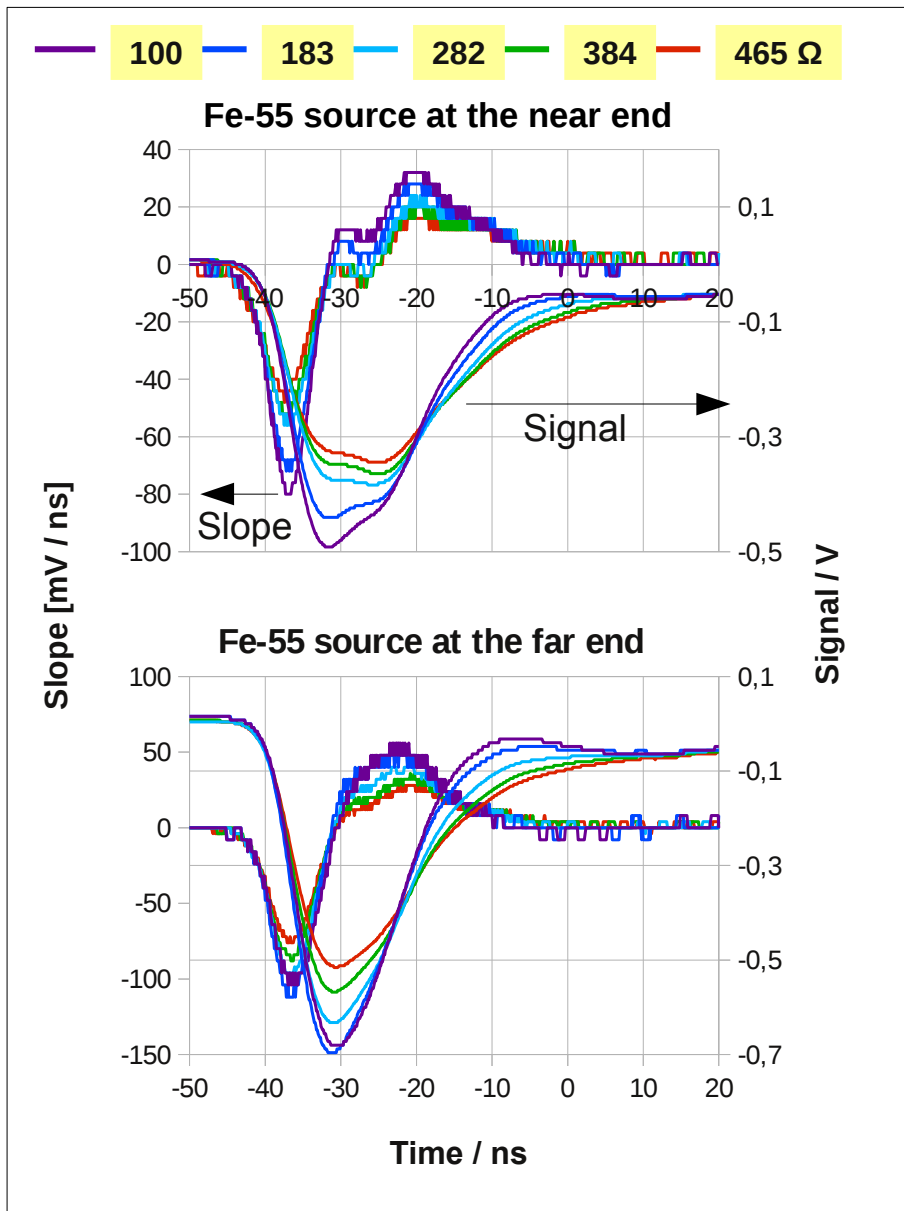
91 ps

(near end

36 ps)

(with RMS noise voltage = 3.2 mV)

# Impedance matching between straw and amplifier input



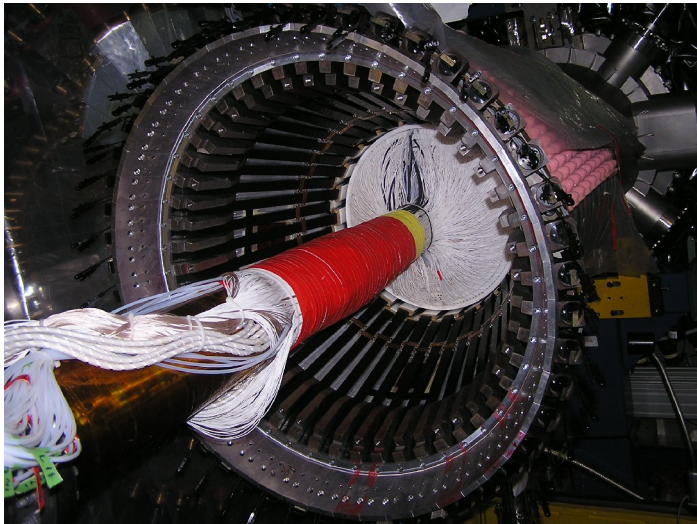
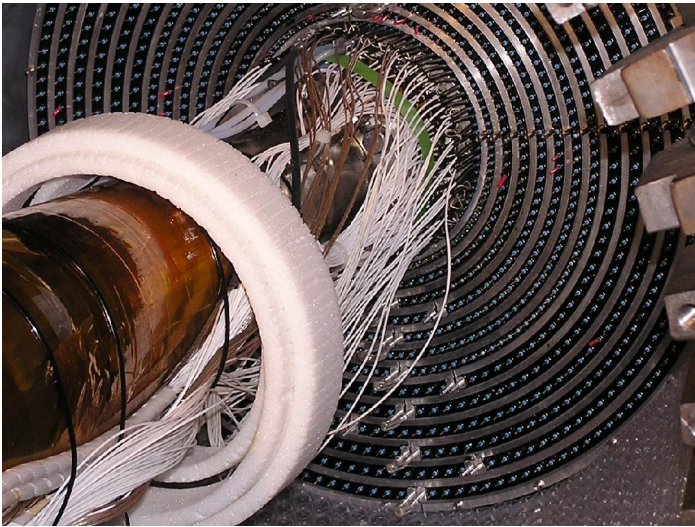
- Standard 60 MHz amplifier used from now on
- Straw impedance  $\sim 373 \Omega$
- Resistors placed between Straw and amplifier
- Source: Fe-55

- Largest amplitudes and signal slopes  
Without impedance matching
- No effect on the noise voltage  
 $\sigma_V = 3.5 \pm 0.1 \text{ mV}$
- Best values for the time uncertainty:  
near end: **44 ps**  
far end: **31 ps**



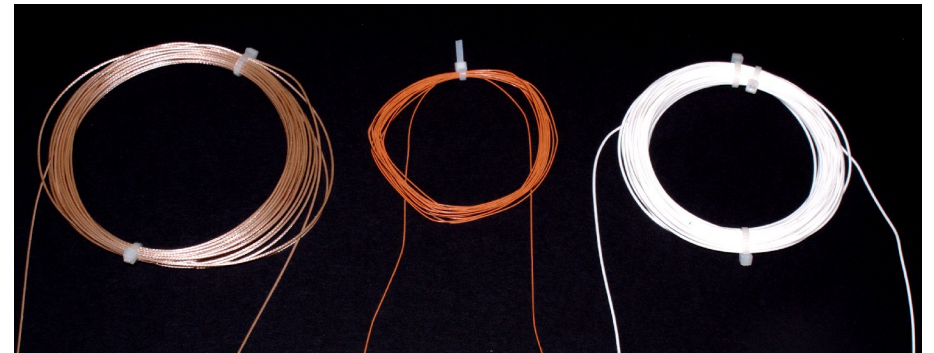
## WASA: Common cables for signals & HV

Cables plugged directly onto straw pins  
Cable type: Filotex 75  $\Omega$   
1.2 mm  $\varnothing$   
5 m long



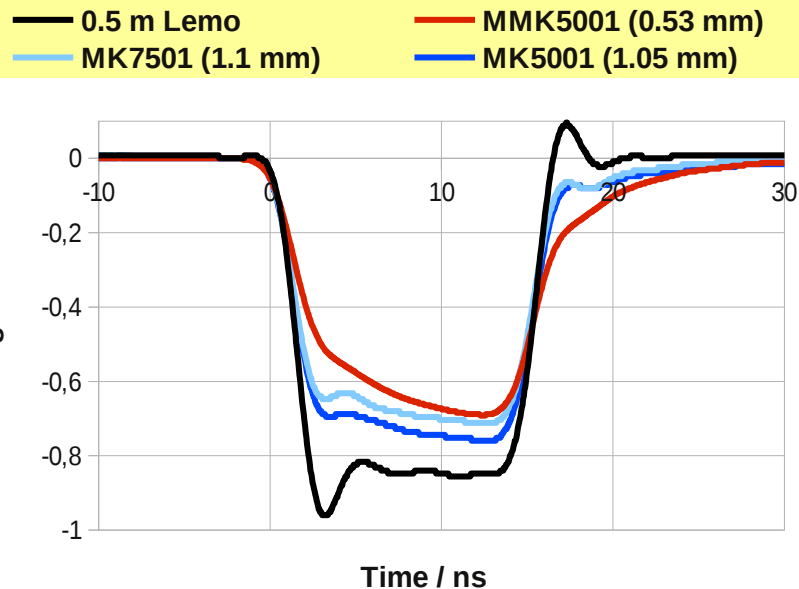
## PANDA: Cables candidates investigated

MK5001	MMK5001	MK7501
1.05 mm	0.53 mm	1.1 mm
HV test at factory:		
1000 V	-----	1000 V



# Standard NIM signals transmitted through thin and very thin cables

Pulse distortion in thin coax cables



Length of cables:

Lemo 0.5 m

thin cables 5 m

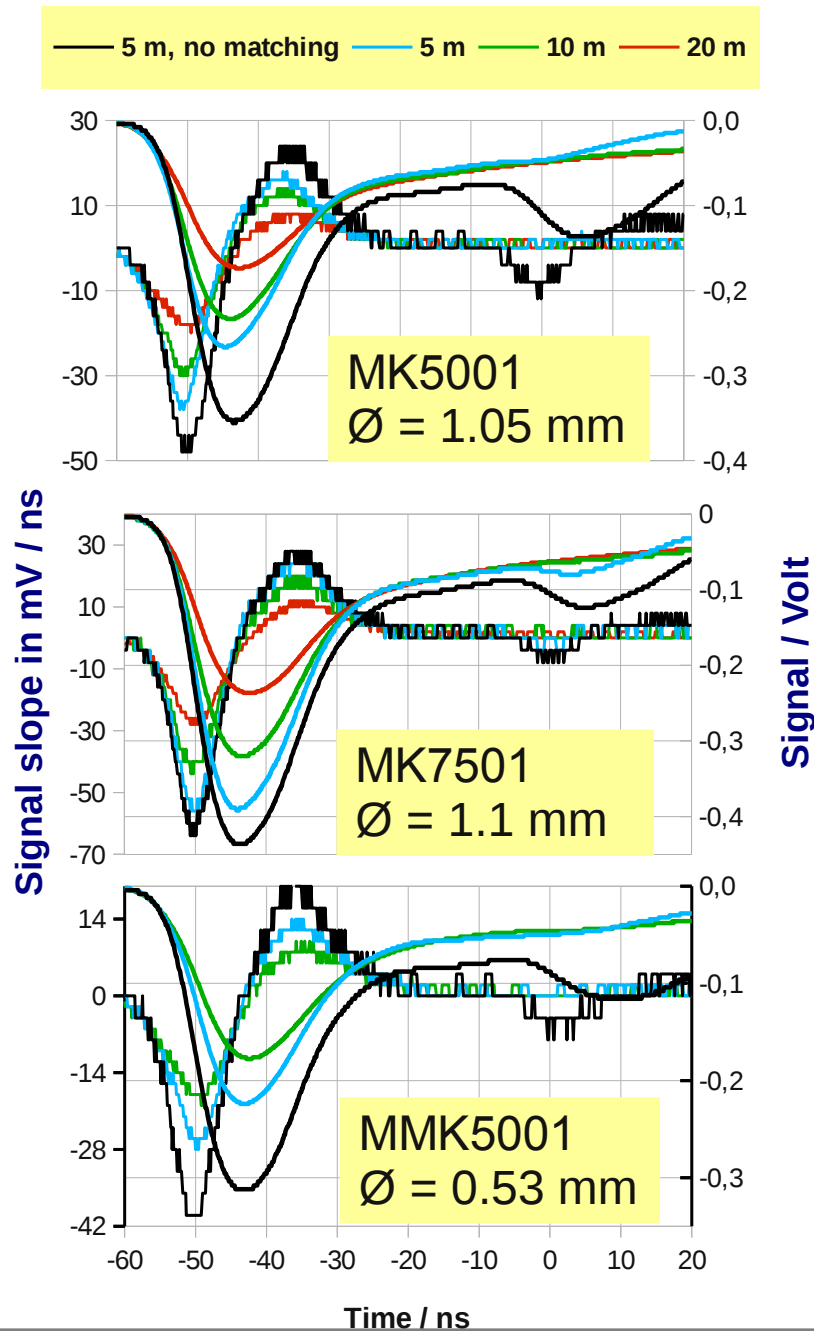
Conclusion:

~ 1.1 mm cables: ~ 20% amplitude reduction

0.53 mm cable: ~ 30 % amplitude reduction,  
less steep

**Rise times still shorter than in initial straw signal**

## Signal transmission through long, thin cables



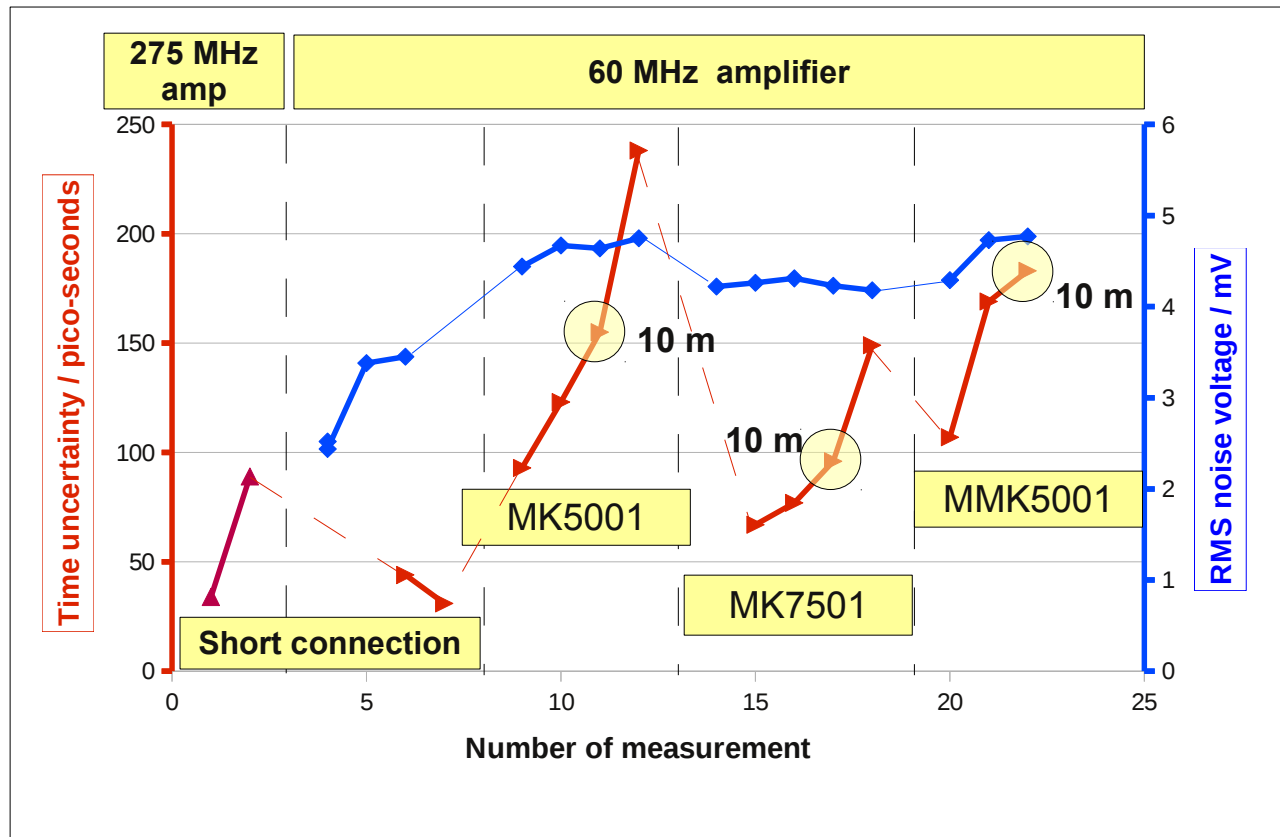
### Fe-55 signals

Cables 5; 10 and 20 m long  
placed between straw and amplifier

Importance of impedance matching at the  
amplifier input: see reflections

Solution with shunt resistor is temporary:  
Amplifier with optimized  
input impedance  
will improve signal

# Estimated electronical time uncertainty



Fe-55	short connection	44 ps
Sr-90 or cosmoics	Normalization: * 4.4	190
Reduction of gas amplification (from $8 \cdot 10^4$ to $5 \cdot 10^4$ )		<b>300 ps (= minimum for any timing technique)</b>

These estimates are based on the assumption that

- timing is derived from the steepest slope
- there is no walk due to leading-edge timing etc.

**These aspects are treated in the DAQ digital pulse processing; see talk of Ljuba Jokhovets**

Sr-90 or cosmoics	thin cable, 10 m long	<b>680 ps</b> (corresponds to 23 $\mu\text{m}$ )
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## Another kind of „noise“: Electromagnetic interference in radiation detectors

**This can be avoided !**

### **Critical points:**

- ground connection between detector and amplifier
- sensitivity along the whole straw

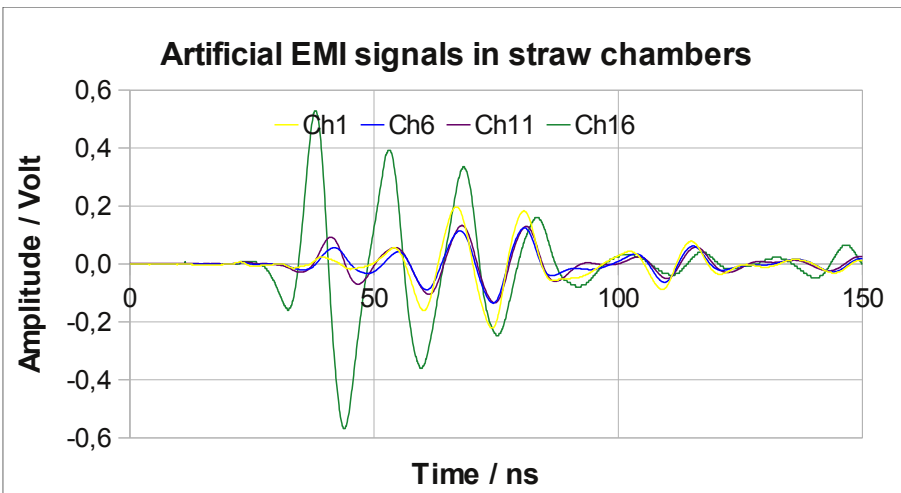
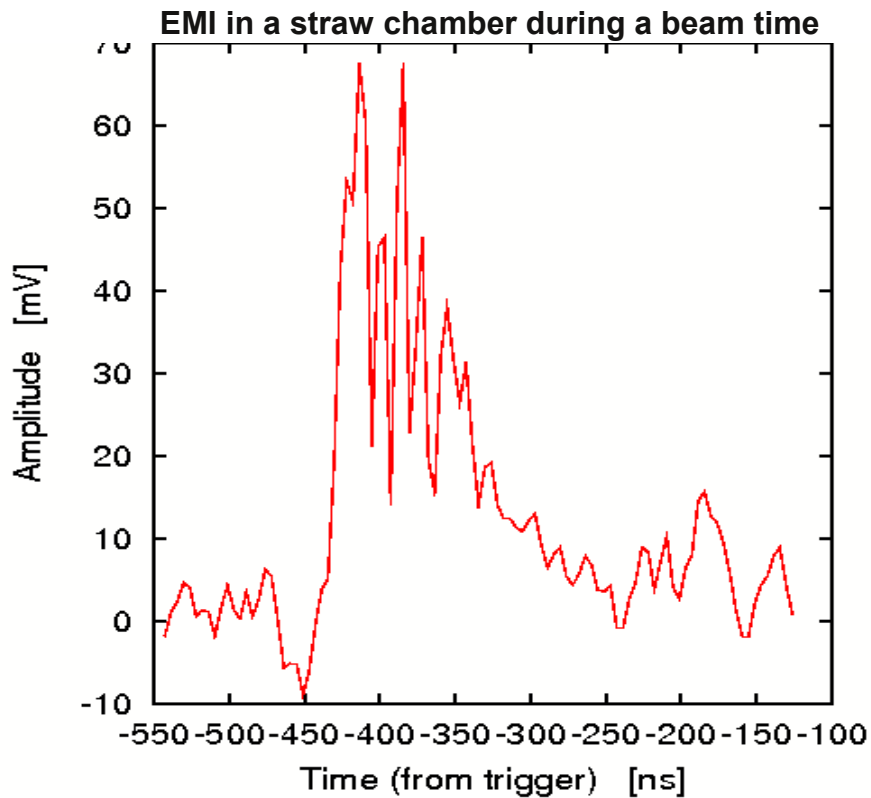
### **Sources:**

- Often unknown
- All powerful electrical devices
- Signal cables with logical signals (twisted pair and also coax)
- Clock signals of on-board electronics
- HV power supplies
- Worst case: coincident parasitic signals, e.g. from photomultipliers

### **Countermeasures:**

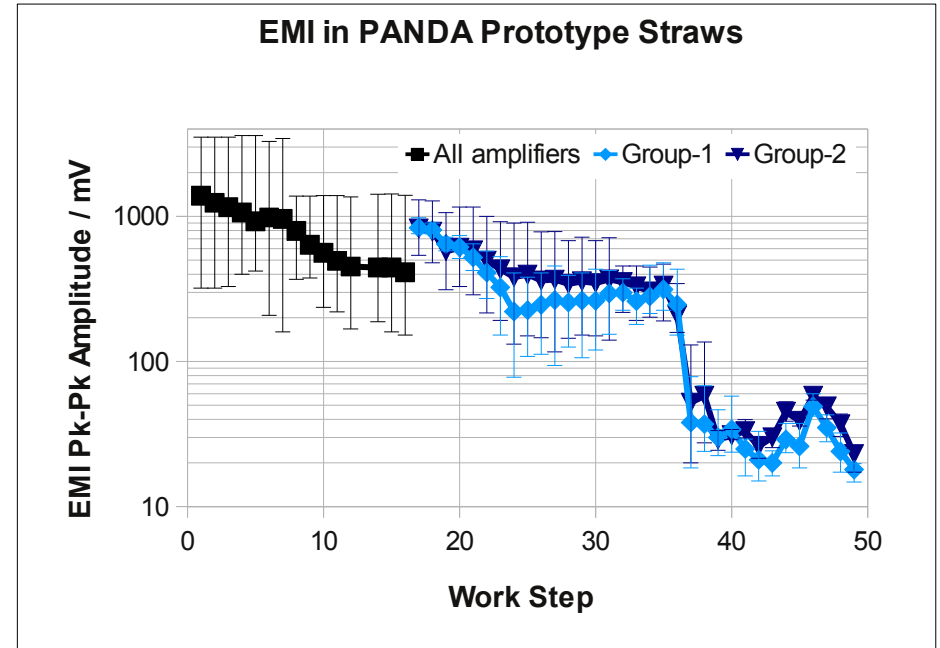
- a common shielding covering straws and electronics
- grounding
- identify source and render it harmless
- be patient

## Parasitic signals in straw chambers



## Application of counter measures:

- Shielding of straws, cables and electronics with 6  $\mu\text{m}$  Al-foil
- Ground connection via wide Cu foils



## Do we know anything about EMI inside PANDA ?

(PMs, signal cables, clock signals, HV harmonics)

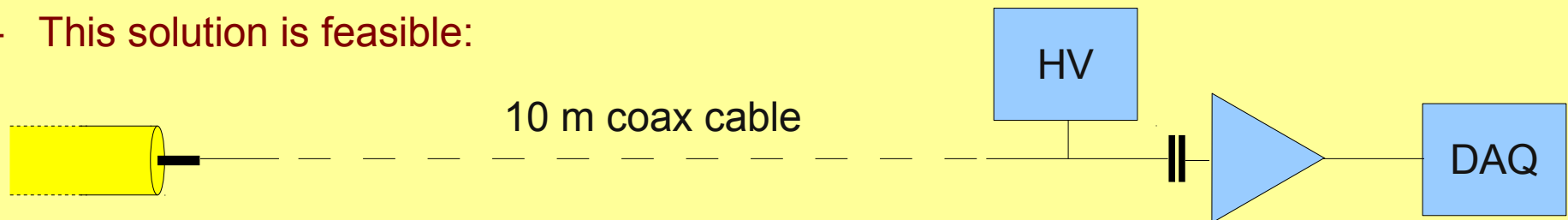
### Recommendation:

- Shielding of the whole STT with a tight jacket of Mylar + Al
- Electronics and the body of the STT on the same ground

A significant reduction of parasitic amplitudes happens only when the last hole in the shielding is closed

## Summary

- Initial straw signals are not extremely fast  
Thin cables make only moderate signal deterioration
- Impedance matching  
Not needed between the straws and the cables  
It must be precise at the amplifier input
- Time uncertainty of 680 ps expected for MIPs with 10 m thin transmission cable
- Shielding of the whole STT and the cables against EMI is necessary
- This solution is feasible:



## Near Future Strategy

### Amplifier:

- Design of an optimized version of the amplifier currently in use starting Nov 2013
- longer integration
- reduced power consumption, reduced range of output voltage
- adjustable impedance matching for straws and cables

### Cables:

- Large-scale in-beam tests with STT
- No strong effect on time resolution expected; it may not be significant

### Flash ADC system:

- Talk of Ljuba Jokhovets
- new design, more compact

### Measure time resolution as directly as possible

(with tracking experiments we are usually not sensitive enough):

- Deduce a precise trigger signal from straw signals
- Check the contribution of all major electronical ingredients

### Realistic larger-scale setup for in-beam test in 2014

- with almost final amplifier
- with long cables