

# Commissioning of the SIS18 Micro Spill Cavity

Experiment 29.11.2023

Machine Meeting (HADES) 19.12.2023

K. Groß, H. Klingbeil (RRF)

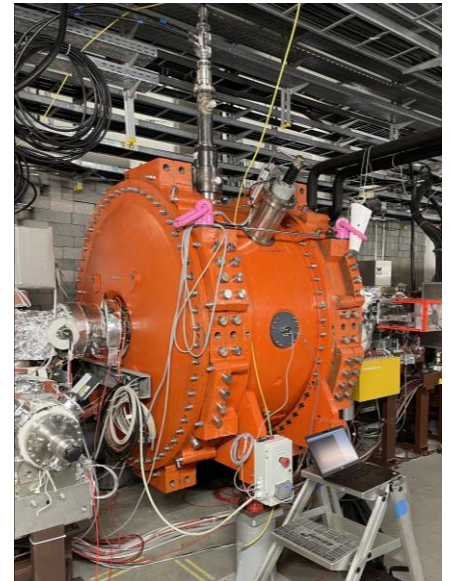
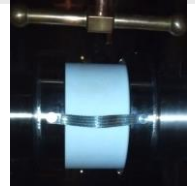
# Parameters of the Micro Spill Cavity GS11BE6

## Requirements and Limits

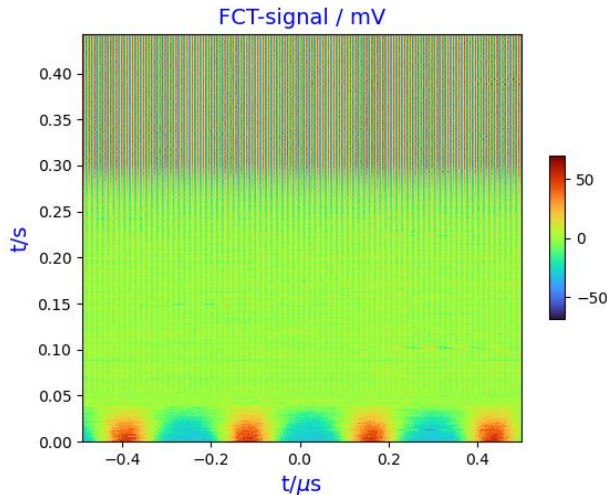
- Access SIS18 required before & after operation to remove short-circuit
- Conditioning required, warming-up & cooling-down time
- Locally operated (BG 1.016)
- Frequency range 81 to 81.8 MHz  
(down to 79 MHz with low voltages – sparks)
- Gap voltage amplitude up to 25 kV
- Impedance without shortcut about 500 k $\Omega$ ,  $Q_0 \approx 5000$

## Settings on 29.11.2023

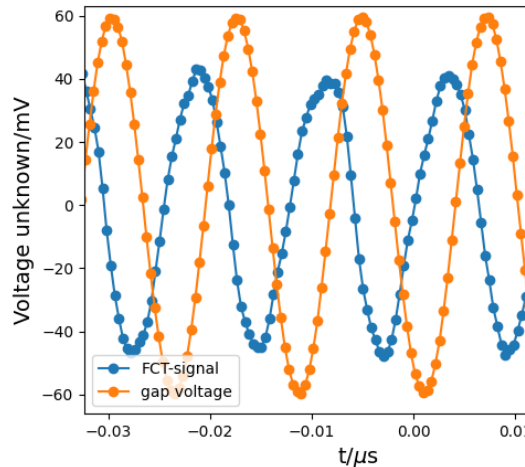
- Conditioning 1:40 h,  $^{14}\text{N}^{7+}$ , 300 MeV/u, 2 s flattop,  
8 s slow extraction, h=90 (81.4366 MHz / 904.9 kHz)



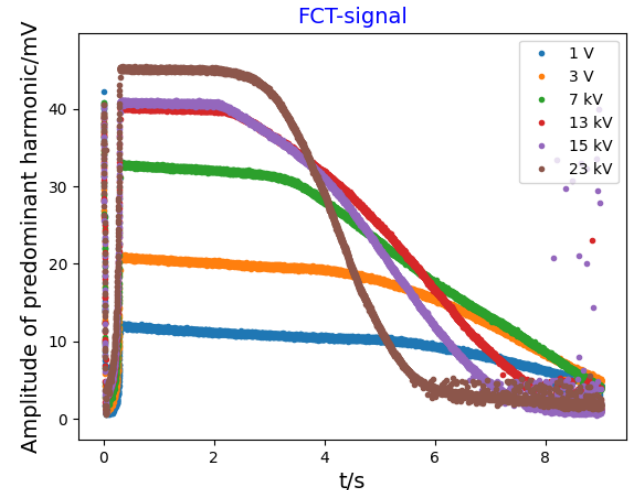
- Preliminary results, detailed analysis still has to take place
- Beam current measurements in SIS for 100 V to 23 kV,  $\approx 10^9$  particles / 1 mA
- Spill measurements in HHD (Ablass-Expert & TDC)



Figures:  $h = 4 \rightarrow$  capture @  $h = 90$



rf signals at 81,345 MHz

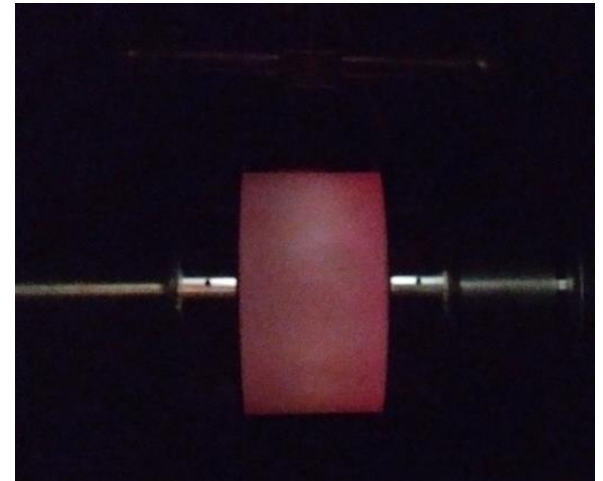
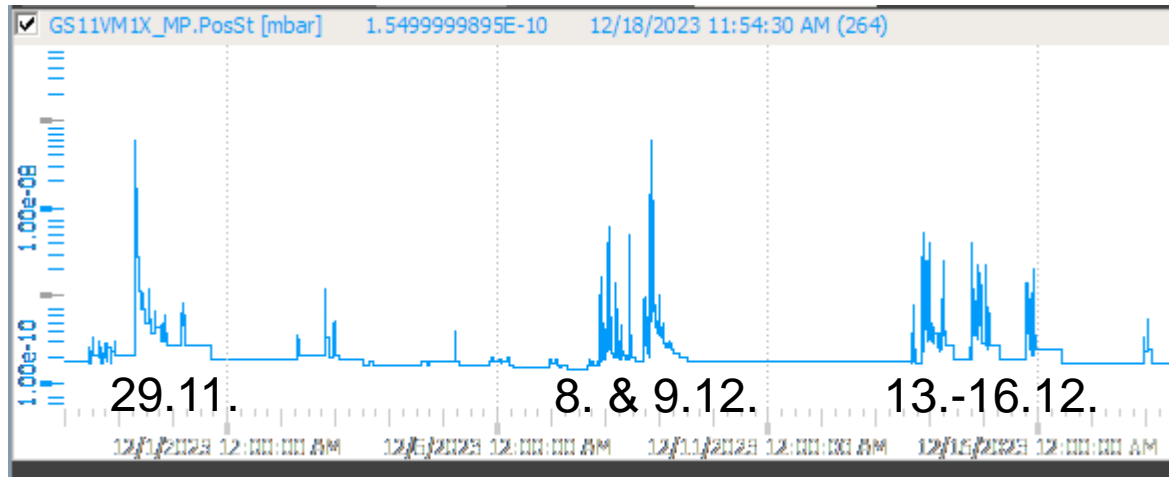


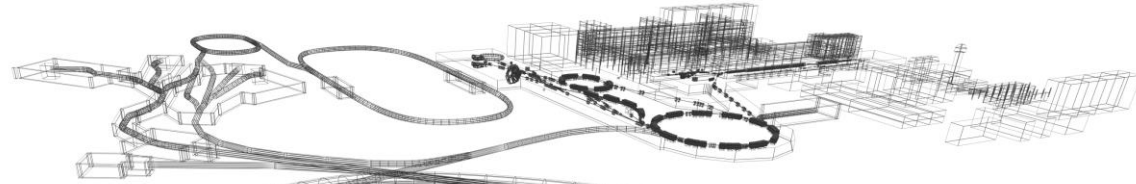
decreasing current during extraction

# Remarks on Cavity Impedance and Vakuum

Additionally tested:

- Successful acceleration of  $1.5 \cdot 10^{10}$  particles, 15 mA
- Induced voltage was  $< 100$  V



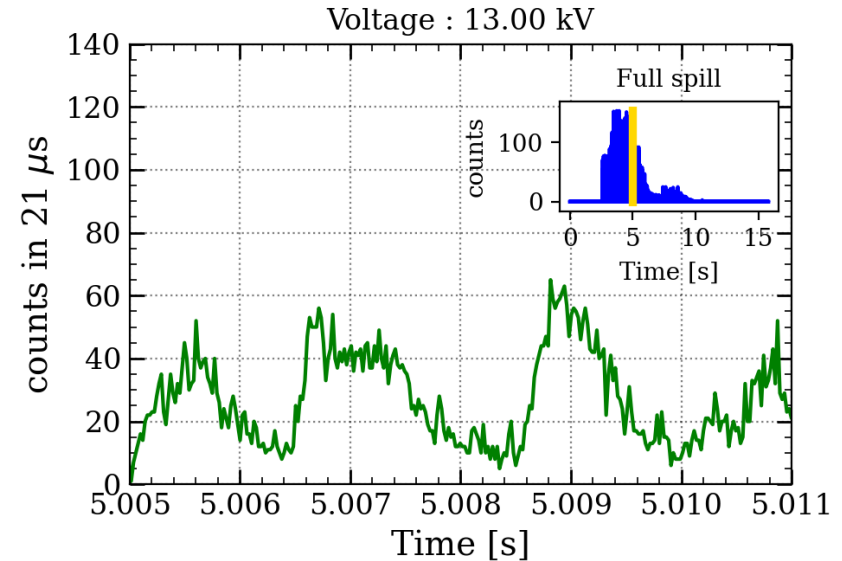
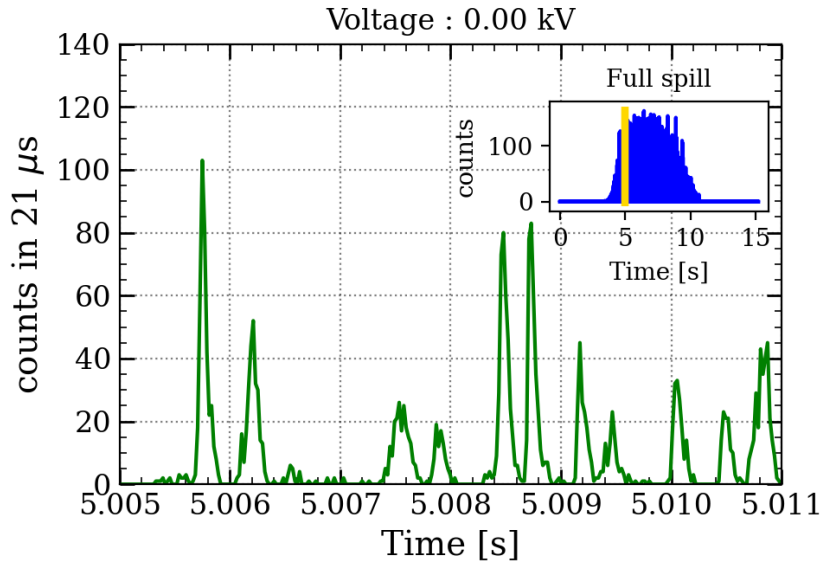


# Spill Quality Evaluation of the SIS18 Micro Spill Cavity

Jiangyan Yang, Peter Forck, Rahul Singh (BEA)  
Stefan Sorge (APH)



## Spill structure in 6 ms



Results: significant improvement for 80 MHz bunching.

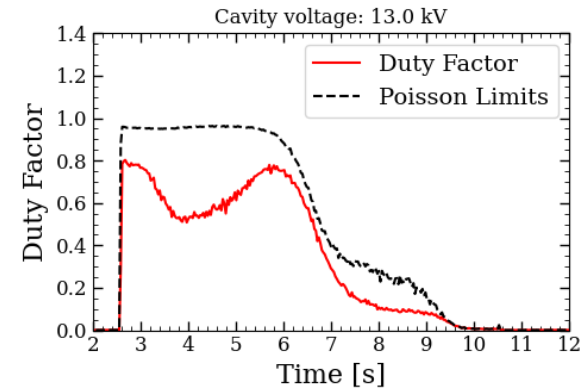
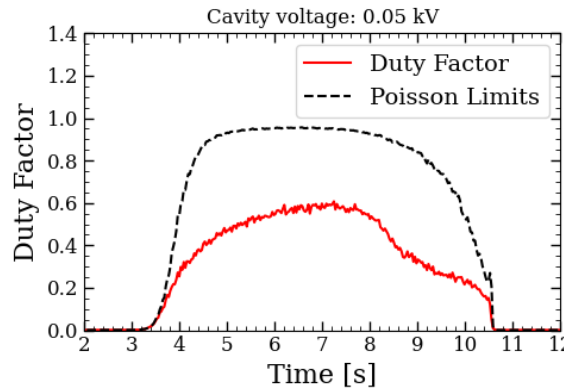
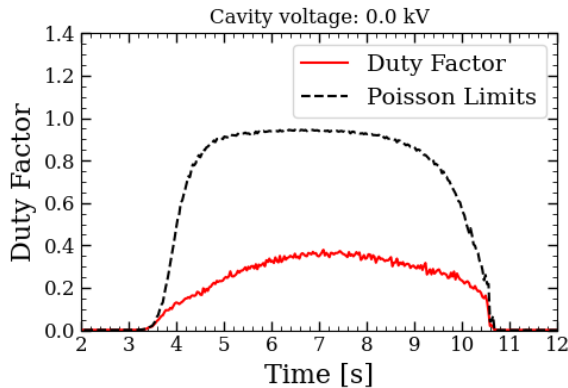
# Spill quality evaluation: time dependent duty factor

Duty factor:

$$F(t_i) = \frac{\mu^2(t_i)}{\mu^2(t_i) + \sigma^2(t_i)}$$

$\mu$ : mean value  
 $\sigma$ : standard deviation

Within time window  $T_{eva}$   
 $T_{read} = 21 \mu s, T_{eva} = 31.5 ms$



Results:

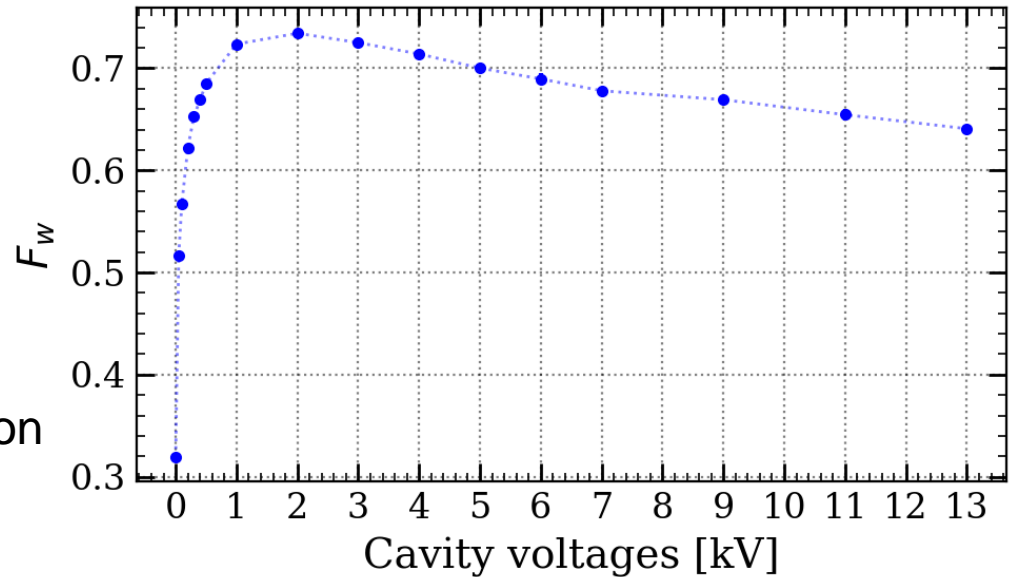
- The higher the duty factor, the better the spill quality
- The improvement of spill quality for bunching is obvious.

Weighted duty factor  $F_w$

$$F_w = \frac{\sum \mu(t_i) \cdot F(t_i)}{\sum \mu(t_i)}$$

$\mu(t_i)$  &  $\sigma^2(t_i)$ :

mean & variance within evaluation window



To be investigated: why is the 'best spill' measured at 2 kV



- **TRI (Transport and Installation)**  
Dirk Acker, Klaus Lück, Markus Grenz-Gustafson, Michelle Diebel, Kosmas Kalaitzidis et al.
- **Bau**  
Bjoern Benz, Johannes Kalenda
- **LRF (Linac RF)**  
Jens Zappai, Bernhard Schlitt, Gerald Schreiber et al.
- **VAC (Vacuum Systems)**  
Maria Cristina Bellachioma, Edgar Renz, Graziano Savino
- **BEA (Beam Instrumentation)**  
Peter Forck, Plamen Boutachkov, Timo Milosic, Jiangyan Yang, Oleksandr Chorniy
- **ARP (Accelerator Radiation Protection)**  
Ekaterina Kozlova, Alexey Sokolov
- **ATP (Atomic, Quantum & Fundamental Physics)**  
Alexandre Gumberidze
- **OPE (Accelerator Operation)**  
Christoph Böhm, Achim Bloch-Späth et al.
- **RRF (Ring RF)**  
Peter Hülsmann (jetzt DESY), Bernhard Zipfel, Christof Thielmann, Martin Hardieck, Janet Schmidt, Oliver Disser, Sebastian Lux, Thomas Winnefeld, Robert Balß, Uli Laier, Harald Klingbeil, Dieter Lens, Stefan Schäfer et al.
- **SIS (SIS100/SIS18)**  
Peter Spiller