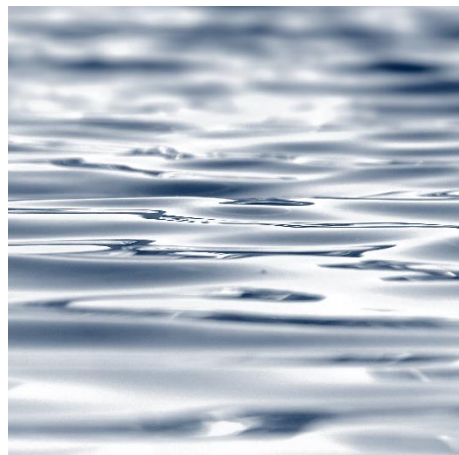


*Miteinander forschen  
Wirtschaft stärken  
Perspektiven schaffen*



# Energy recuperating 4-quadrant power supply for inductive loads

Superconductivity for Sustainable Energy Systems  
and Particle Accelerators

GSI Darmstadt, 18<sup>th</sup> – 20<sup>th</sup> October 2023

**U. Zerweck, N. Gust, A. Wesenbeck, F. Donat,  
T. Jande, S. Rackow, S. Richter, A. Kade**

# Motivation



– Test of superconducting magnets

– Available:

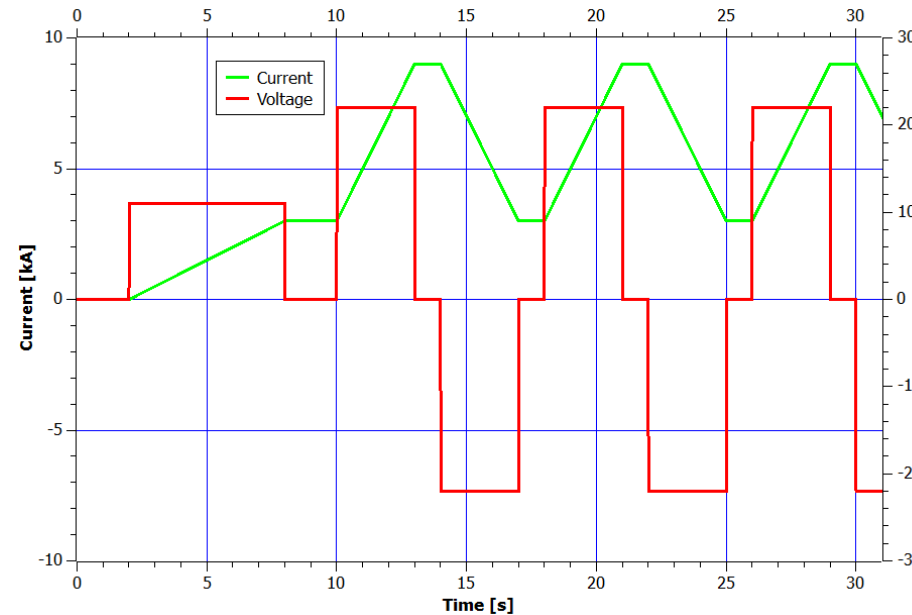
Laboratory grid supply:  
400 V 3~ 130 A 90 kW

Helium infrastructure + rest:  
400 V 3~ 100 A 70 kW

High current power supply:  
400 V 3~ 30 A 21 kW

– Needed:

High current power needed:  
25 V 1- 14 kA 350 kW



SIS300 dipole magnet:

$L = 11.4\text{mH}$

$I_{\text{max}} = 8926\text{ A}$

$U = 22\text{ V}$



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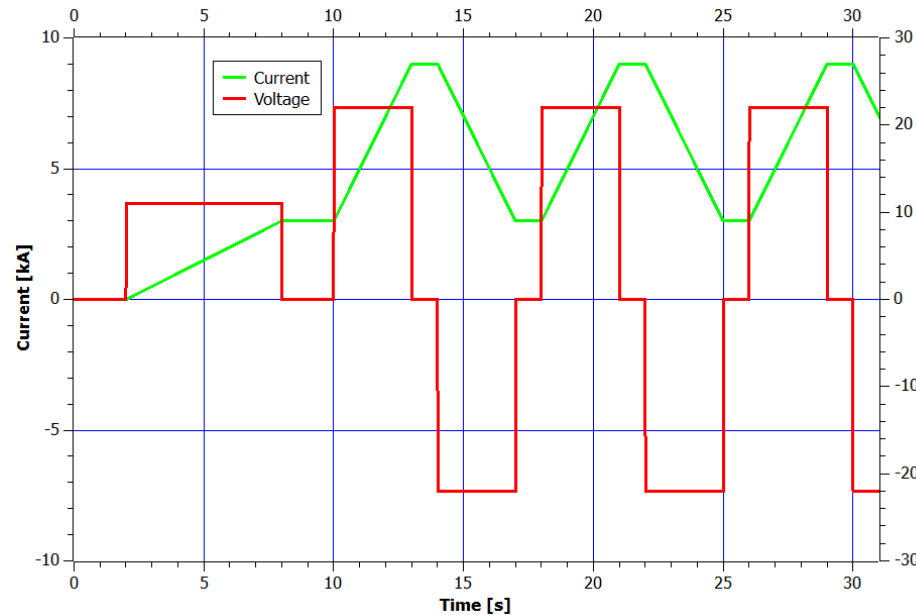
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- ▶ How To: drive an inductive load  
recuperate inductive energy  
store recuperated energy  
store MJ safely, control kA with mV sensitivity
- ▶ Test results of capacitor bank, 4-quadrant converter and quench protection
- ▶ Test with GSI SIS300 magnet (9 kA, 0.5 MJ)

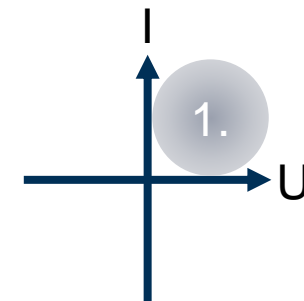
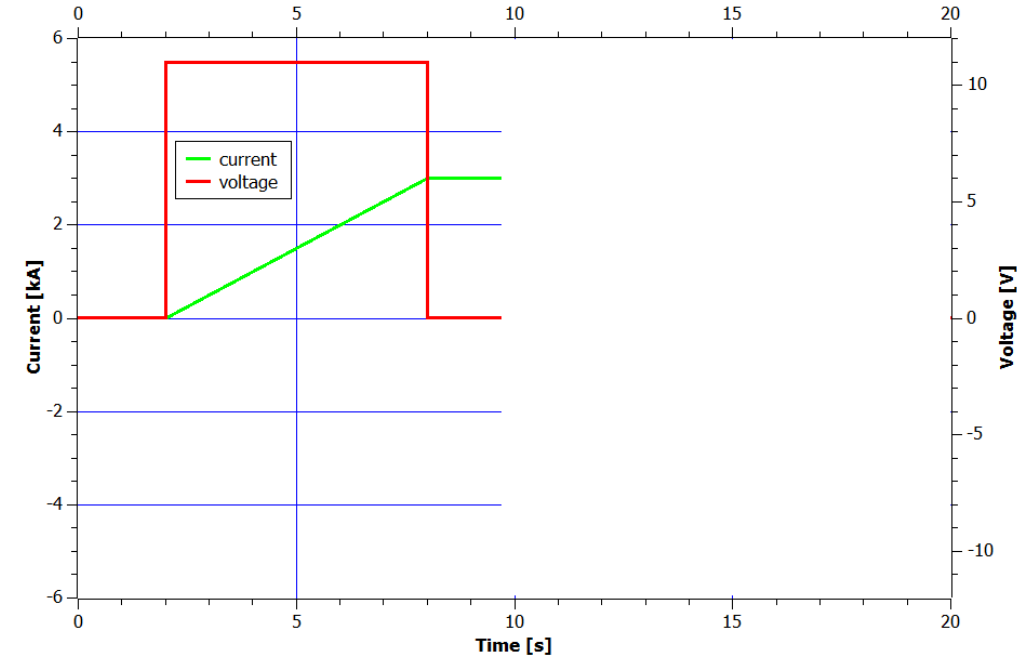
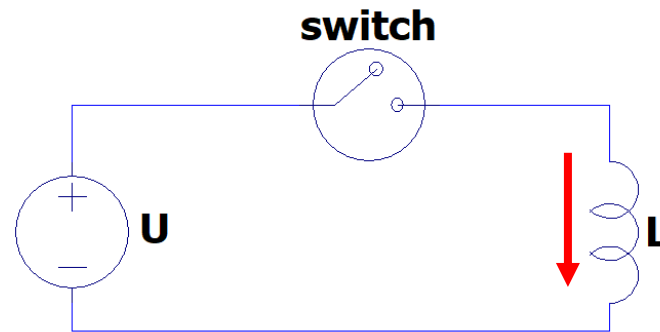
# Current through an inductor



- voltage = torque, current = speed, inductance = moment of inertia
- apply dc voltage on inductance via switch
- current rises linearly
- massive arcing when opening switch



[1]



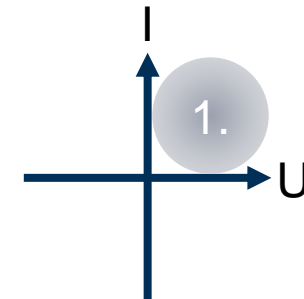
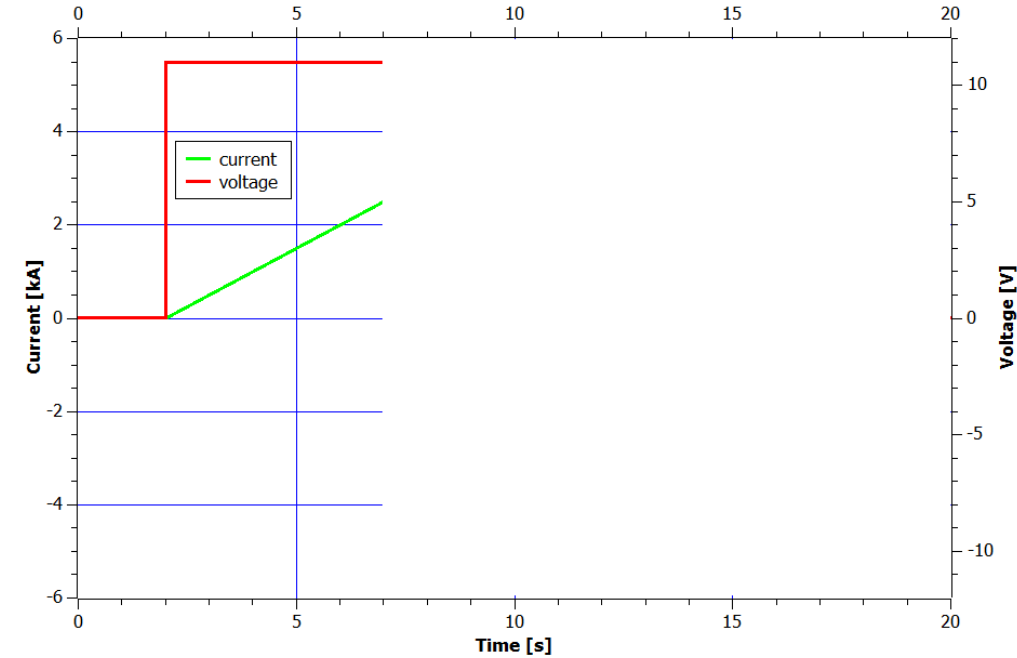
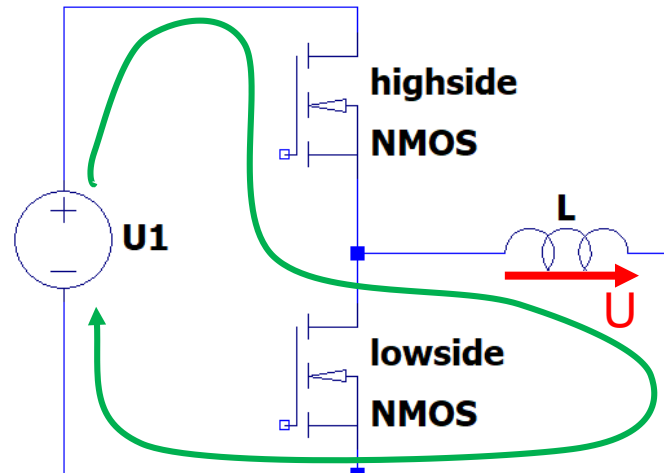
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- voltage = torque, current = speed, inductance = moment of inertia
- replace switch by MOSFETS
- highside increases current



[1]



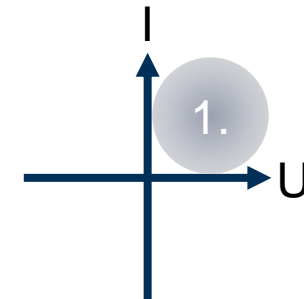
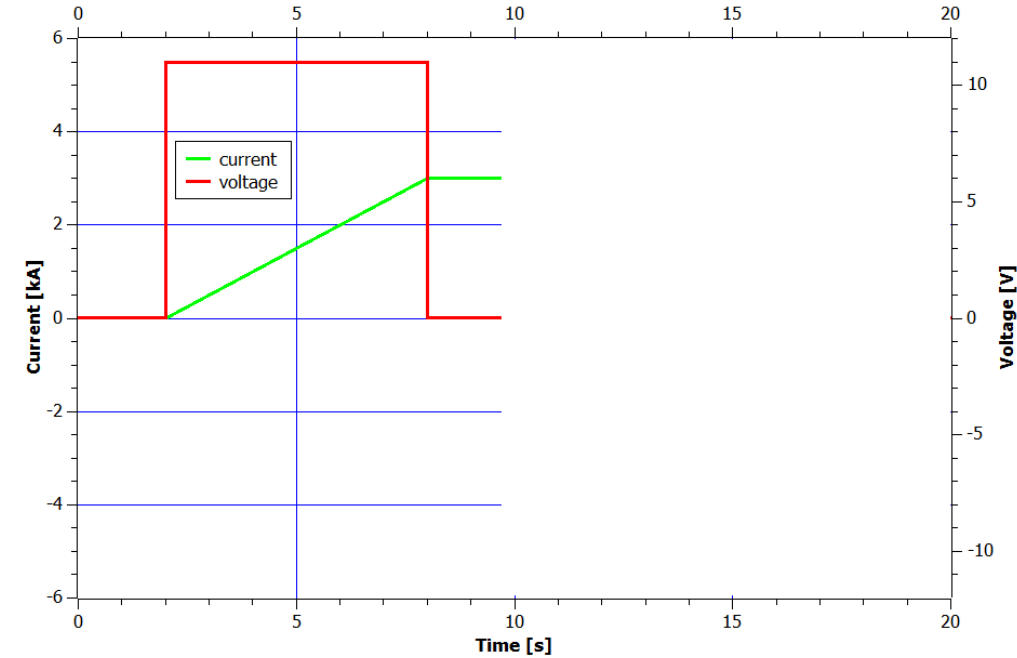
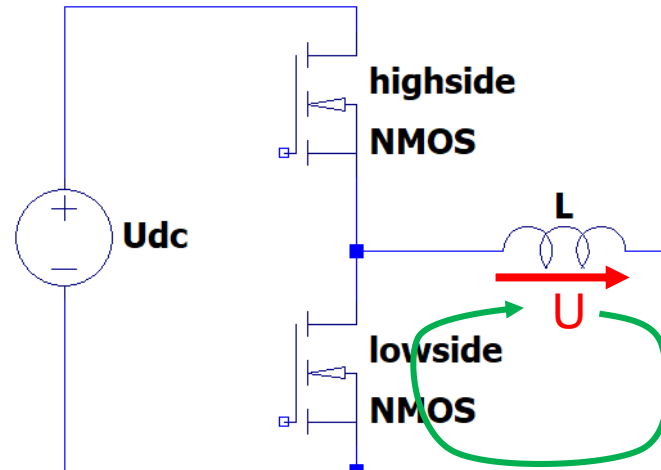
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- highside increases current
- lowside keeps current rolling



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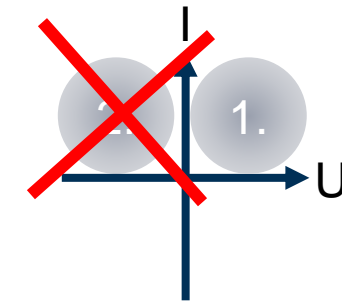
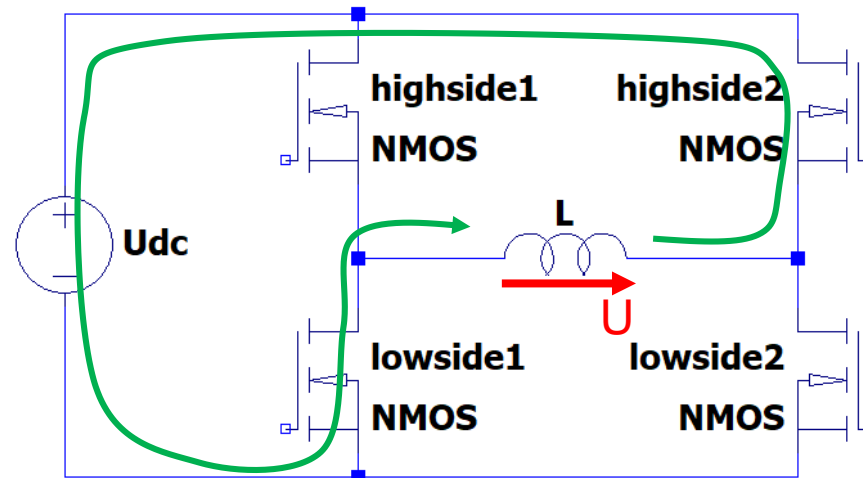
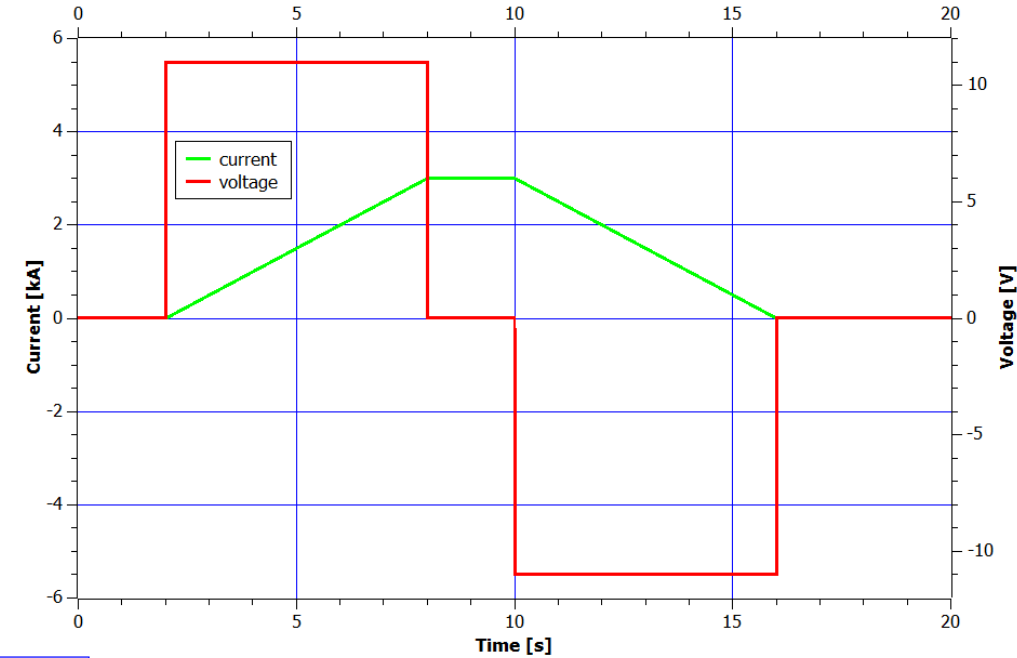
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- recuperation into power supply



[1]

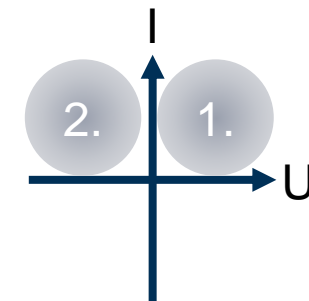
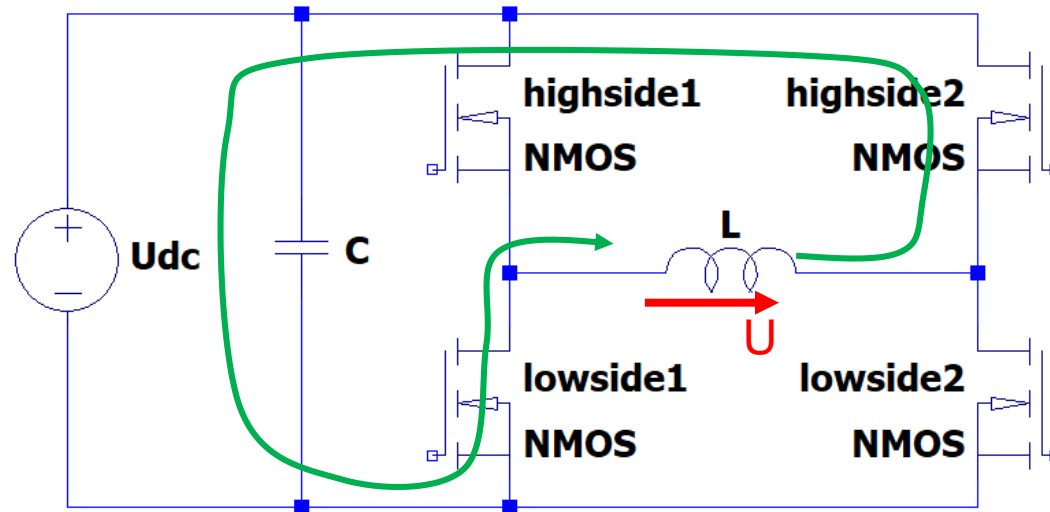
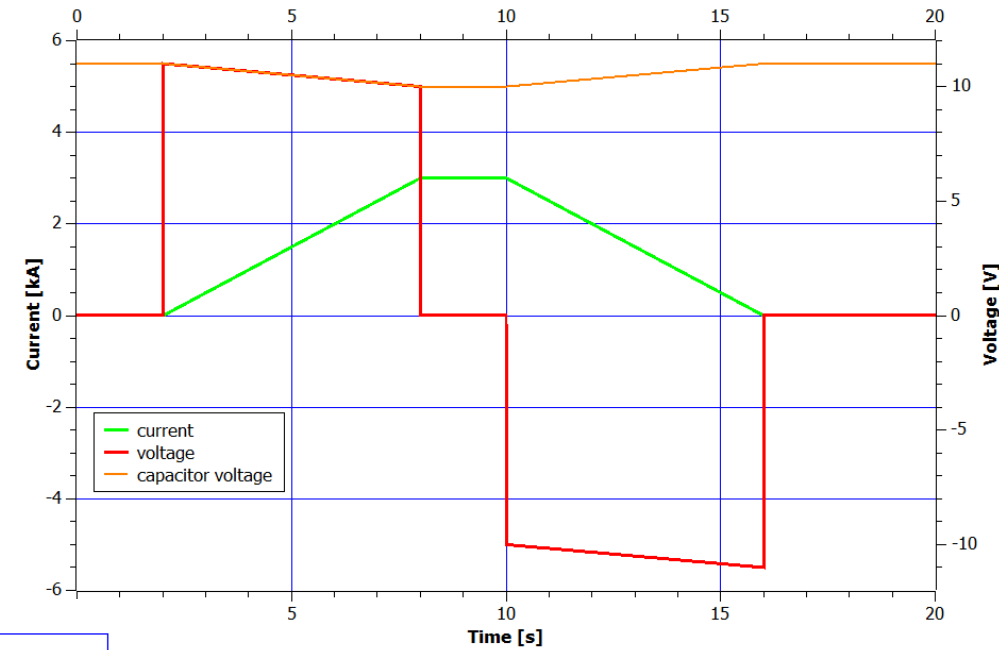




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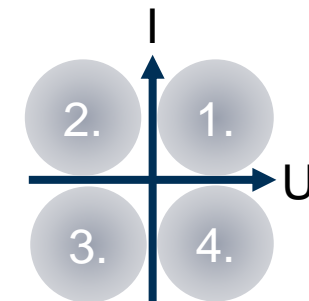
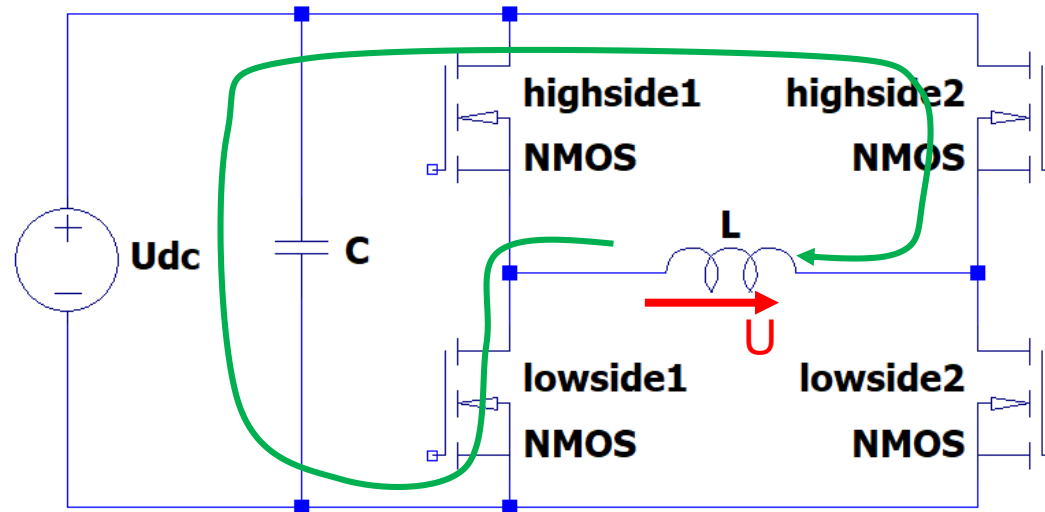
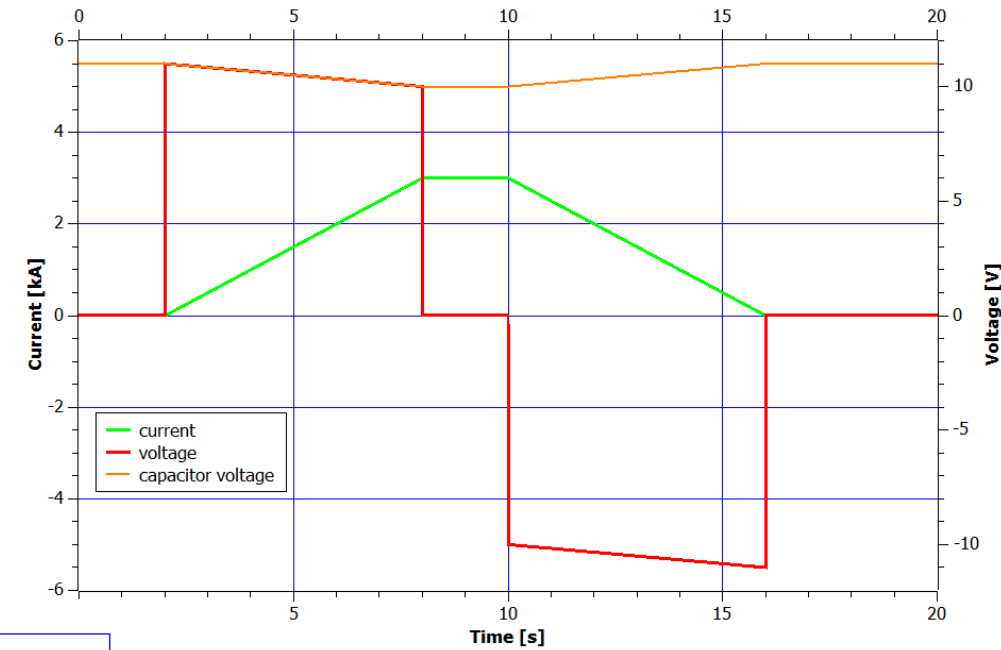


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–  $E_L = 1/2 L I^2 = 500 \text{ kJ}$   
 $\rightarrow E_C = 1/2 C U^2 = 5 \text{ MJ}$



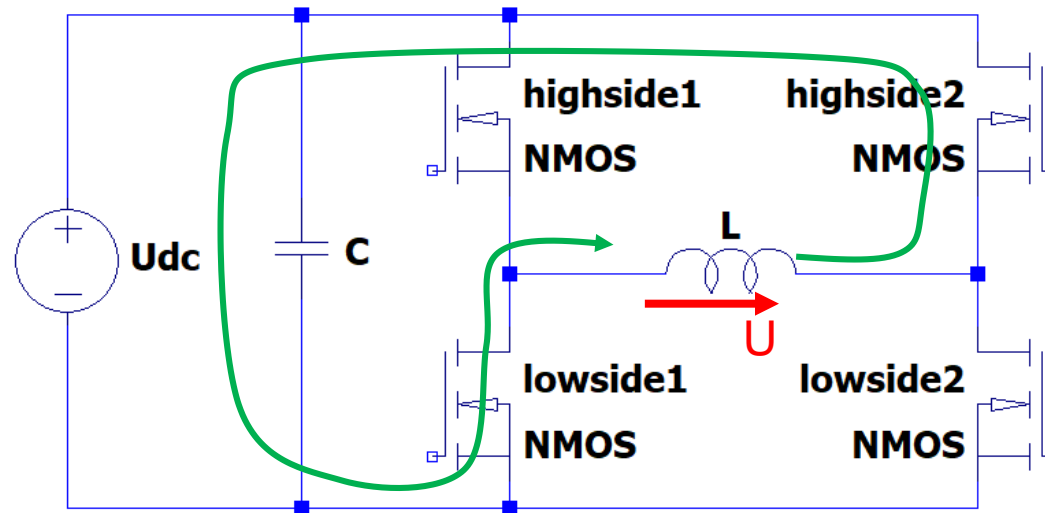
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- 2.7 V Supercapacitors

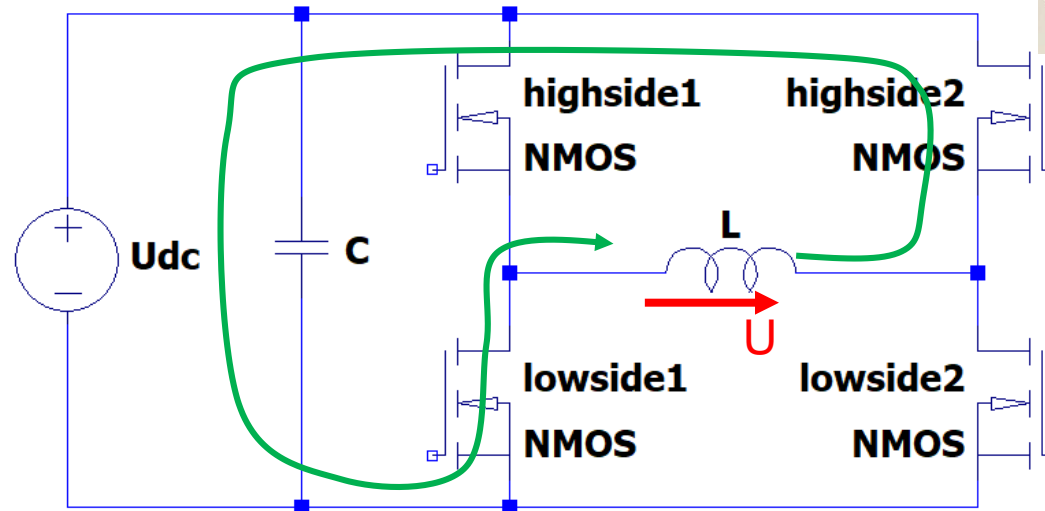


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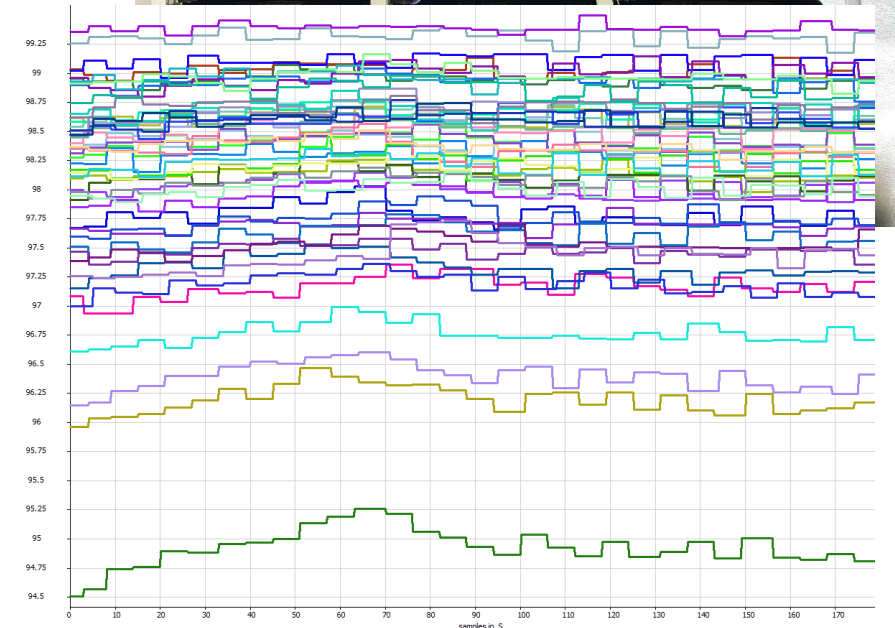
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- 10x → 27 V<sub>max</sub>
- 10x 3x in one rack insert
- 15,3 kF in 17 inserts



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- security:
  - active MOSFETS
  - passive fuses
  - short circuit proof
- ILK temperature sensor multiplexer:
  - each capacitor monitored individually ( $\mu\text{C}$ )



Balance of capacitor cells during operation

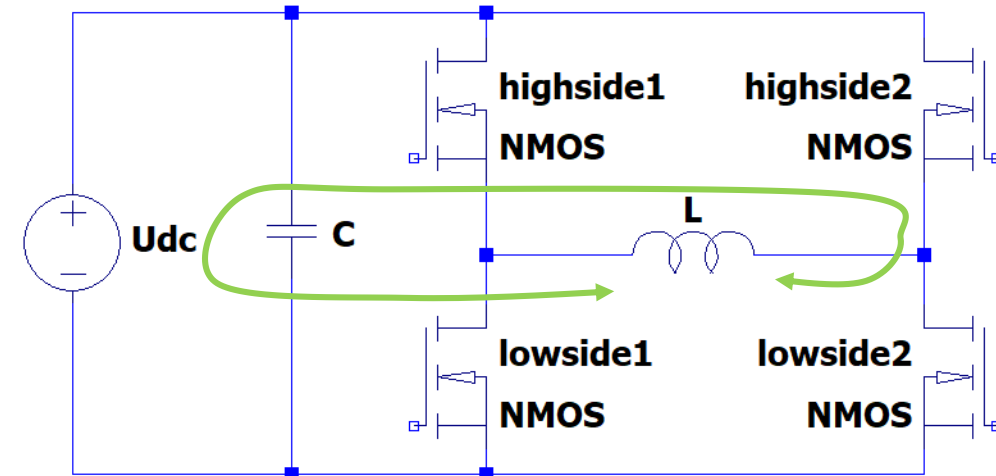
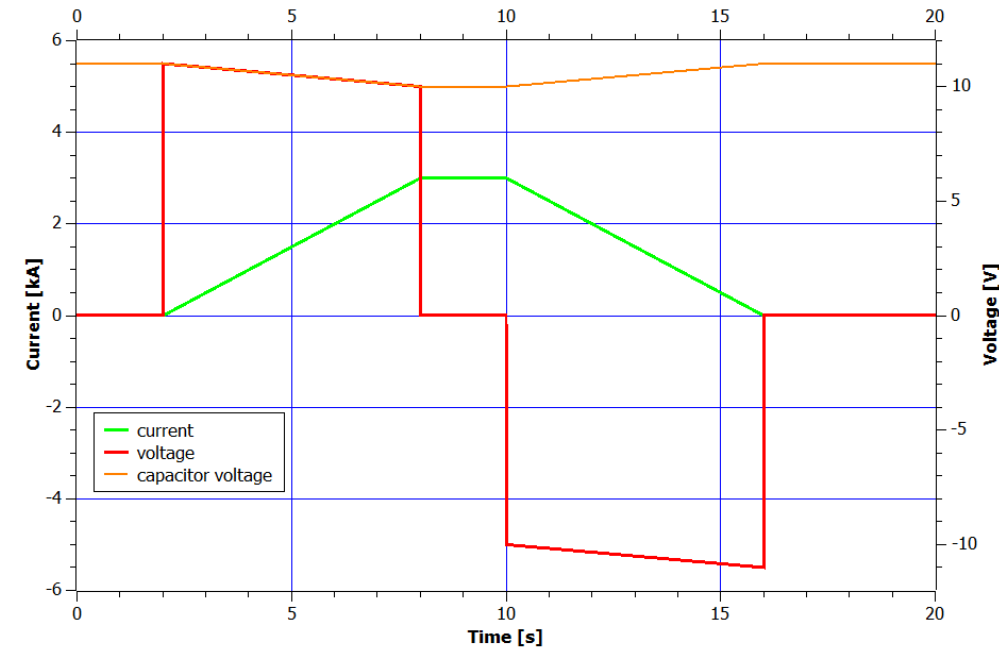
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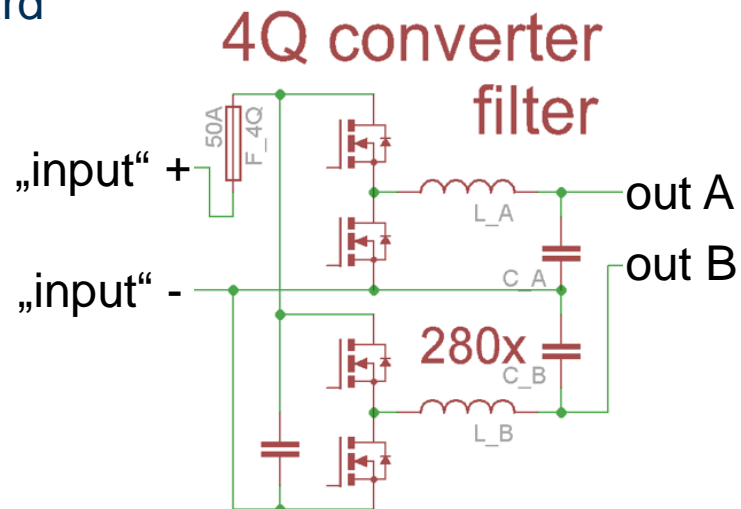
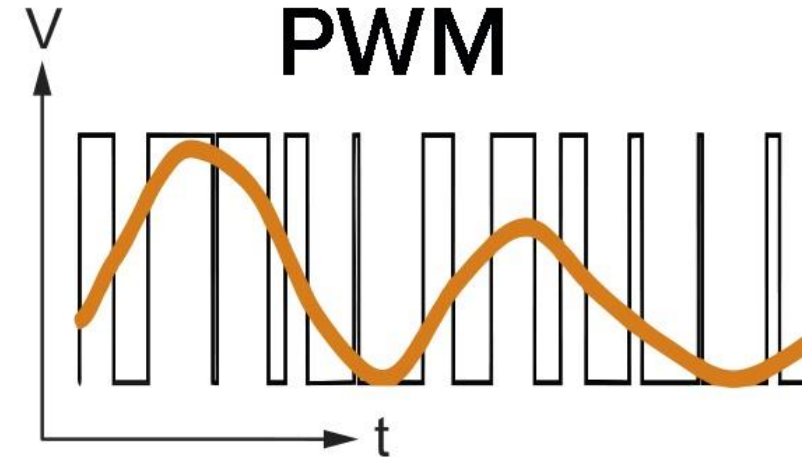
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# High-current voltage supply



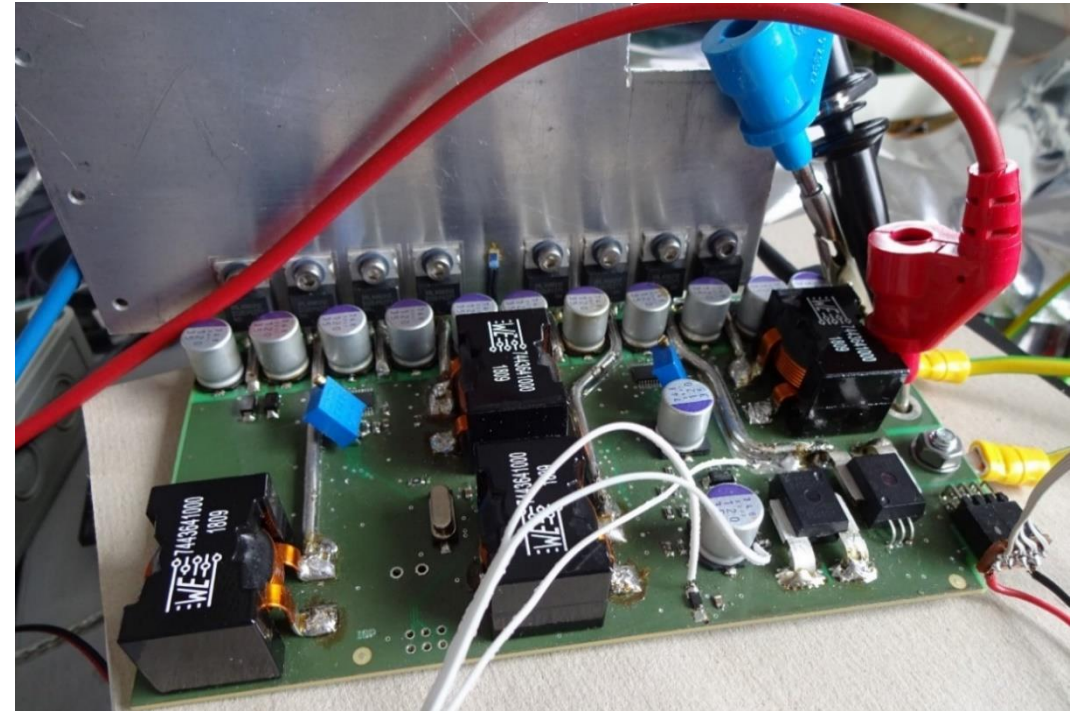
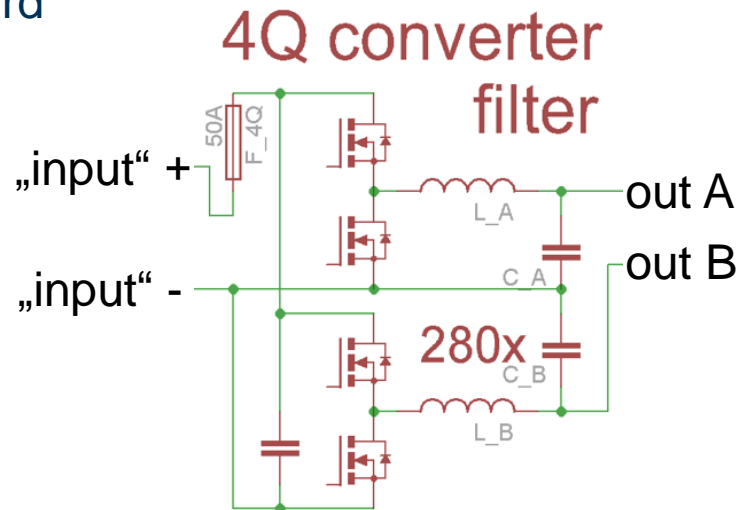
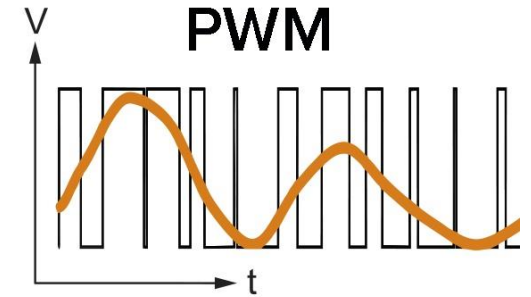
- **variable** output voltage required  $\approx 27\text{V}$
- pulse width modulation of output 0% .. 100%
- steep transients with high harmonics  $\leftrightarrow$  quench detection !
- filtering required, as close as possible
- 30 V 50 A per board



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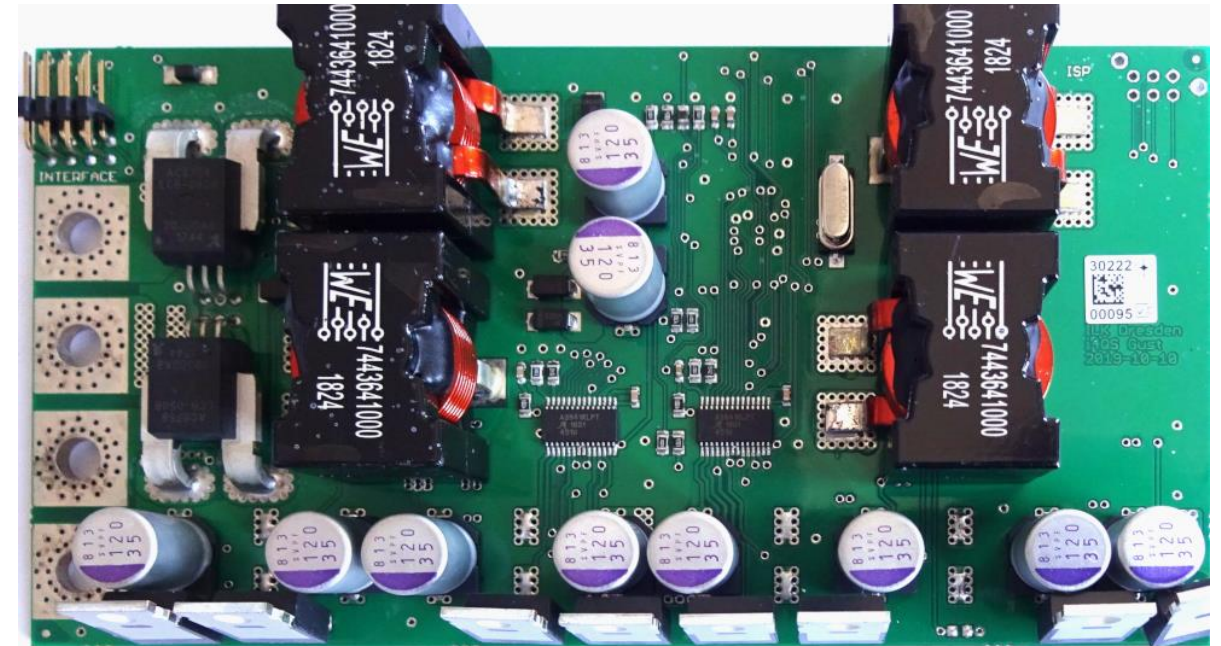
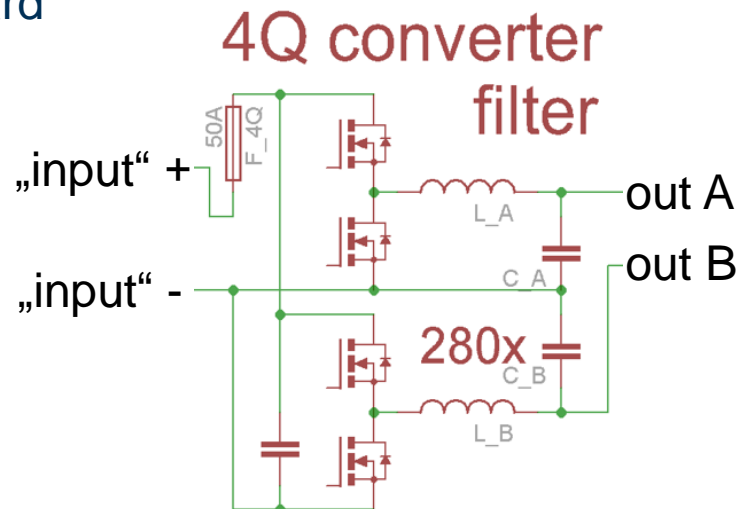
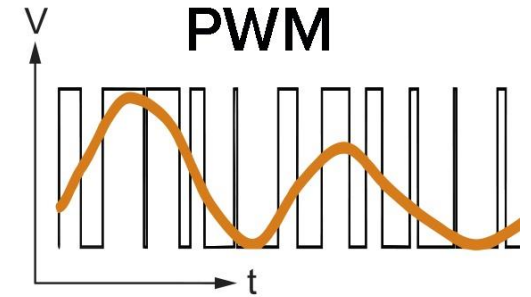




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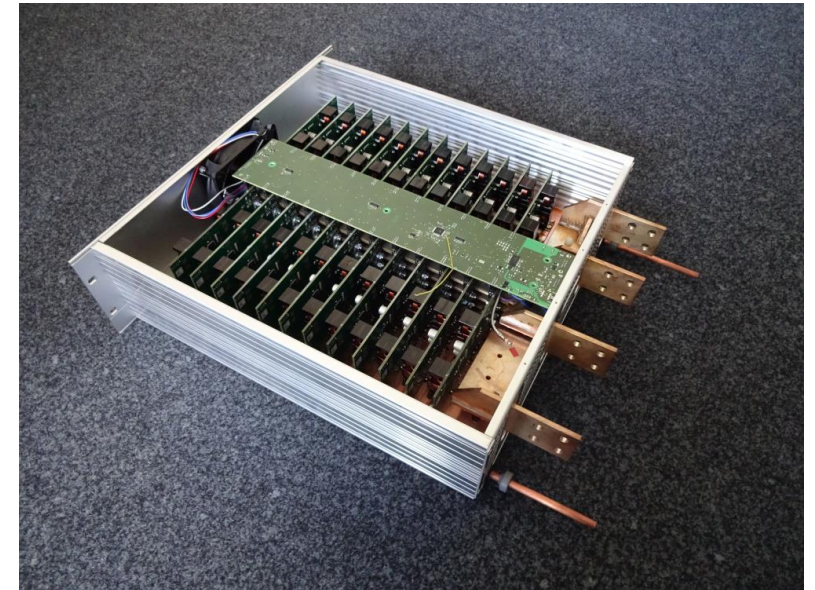
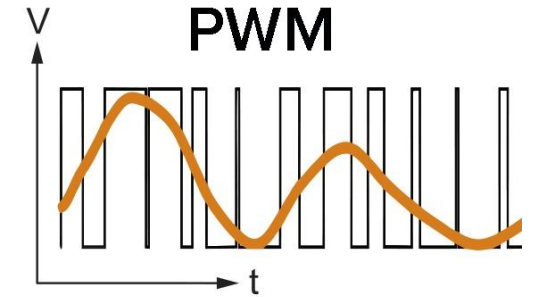
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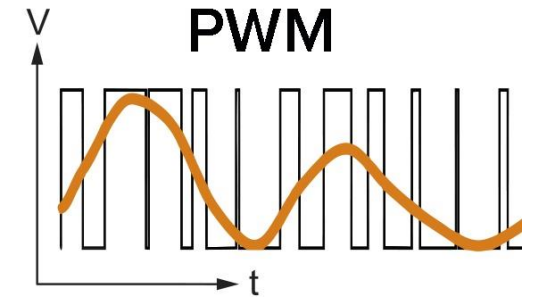
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- 20 boards per rack insert
- 20x output current regulation in parallel
- 1x setpoint distribution and data communication board



# High-current voltage supply



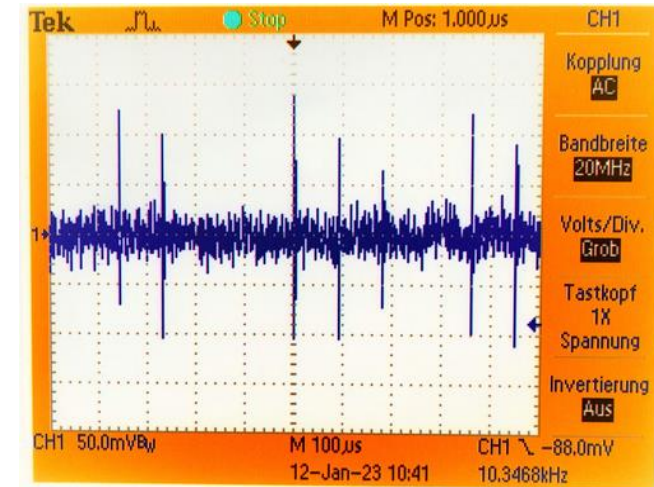
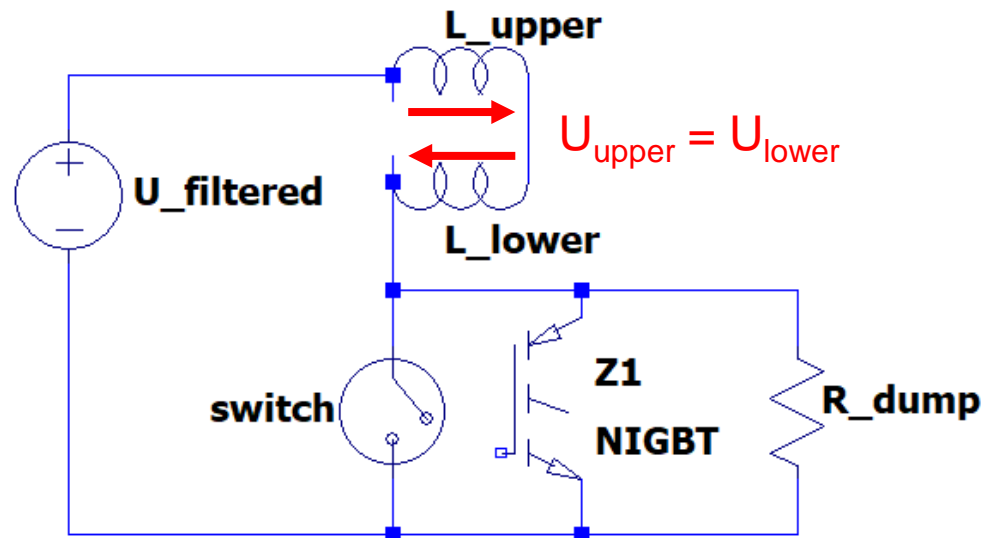
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- 14 rack inserts
- 280 4-quadrant musketeers – one (master) for all, all for one (magnet)



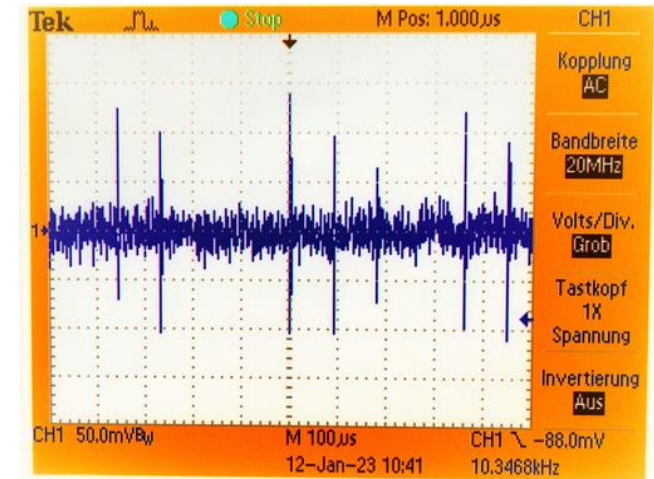
# Quench detection and protection



- filtered output: < 1 mV ripple, theoretically
- measured: 20/100 mV ripple. Culprit: grid power supply
- no noise from 4-quadrant converter measurable
- filtered detection: bipolar, <1 ms, >2 mV adjustable



4Q converter off

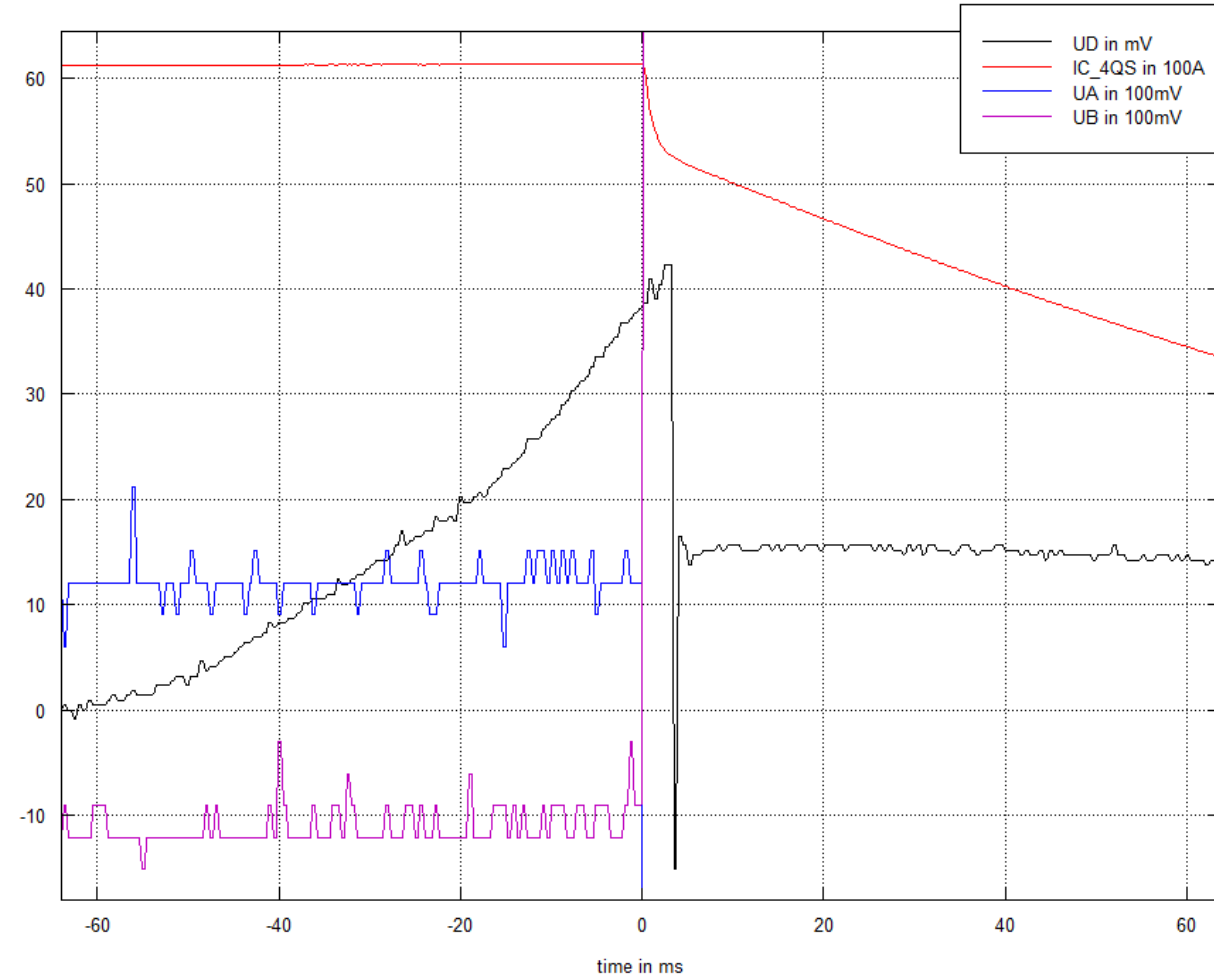
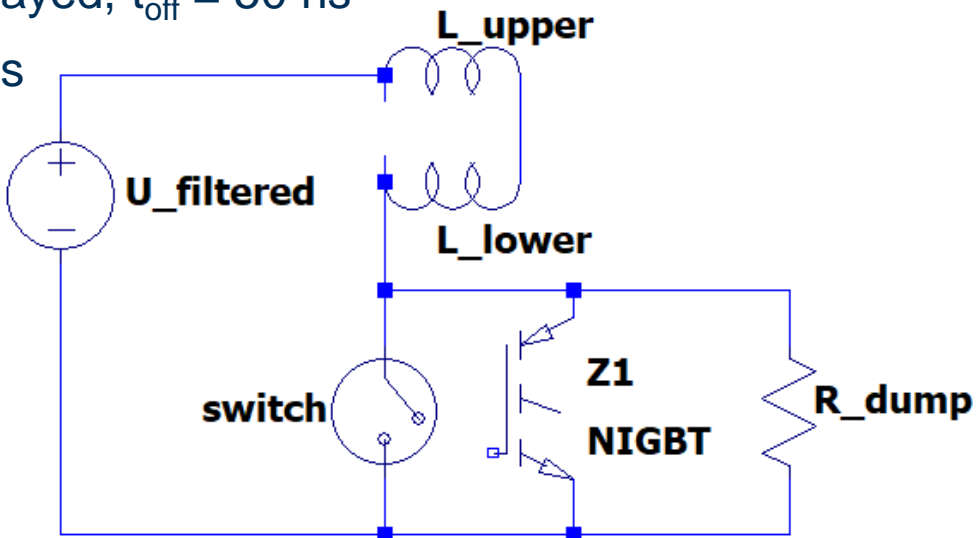


4Q converter on, 1 kA

# Quench detection and protection



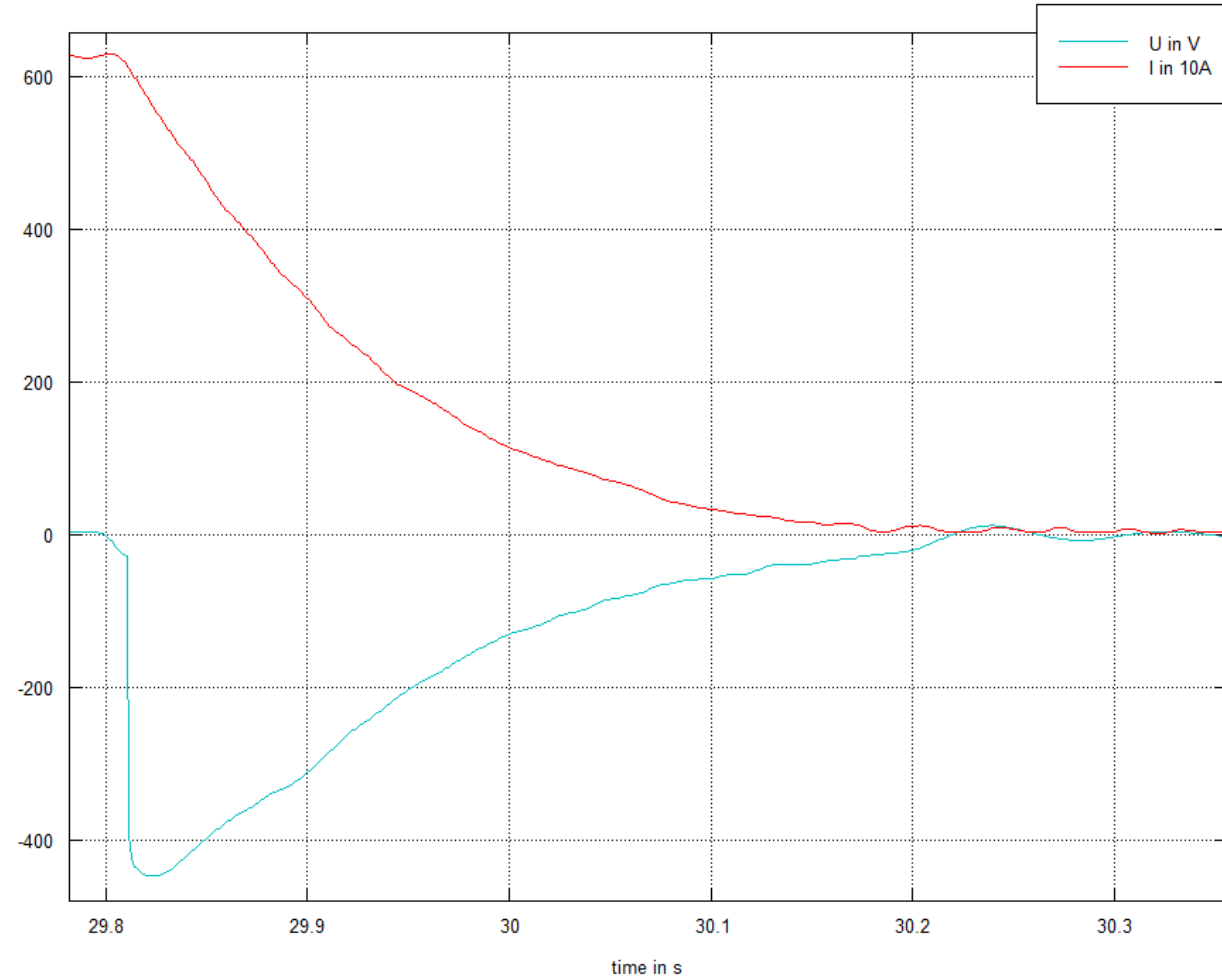
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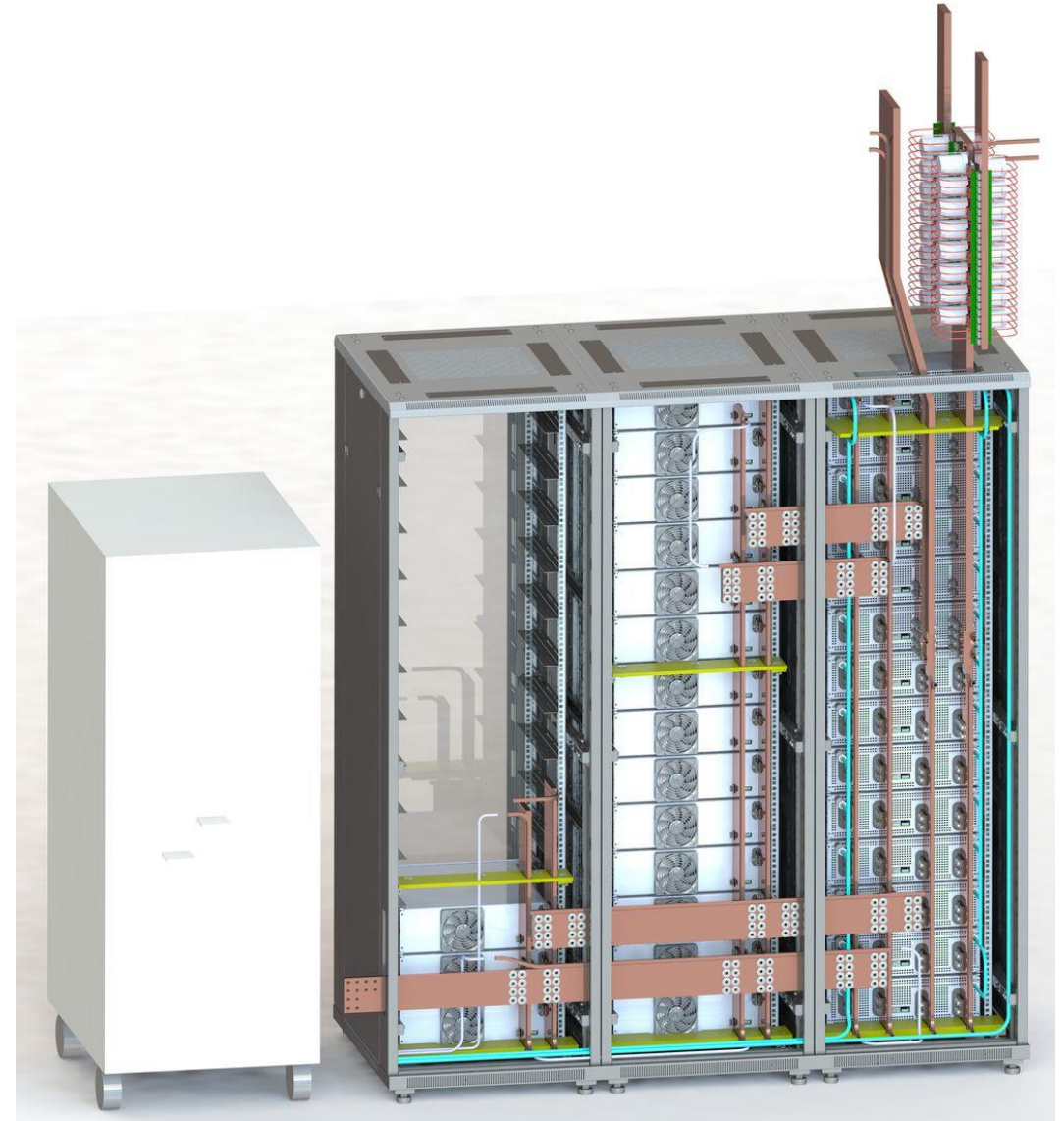
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# Test with GSI SIS300 magnet



SIS 300 magnet at ILK Dresden for testing:

- ▶ ramping with different rates and regimes (start and hold current, timing)
- ▶ determination of quench characteristics
- ▶ inductance 11 mH
- ▶ current 3 ... 9 kA
- ▶ magnetic field 1.5 ... 4.5 T
- ▶ ramp-rate up to 2 kA/s
- ▶ ramp-voltage up to 22 V
- ▶ magnetic energy up to 500 kJ



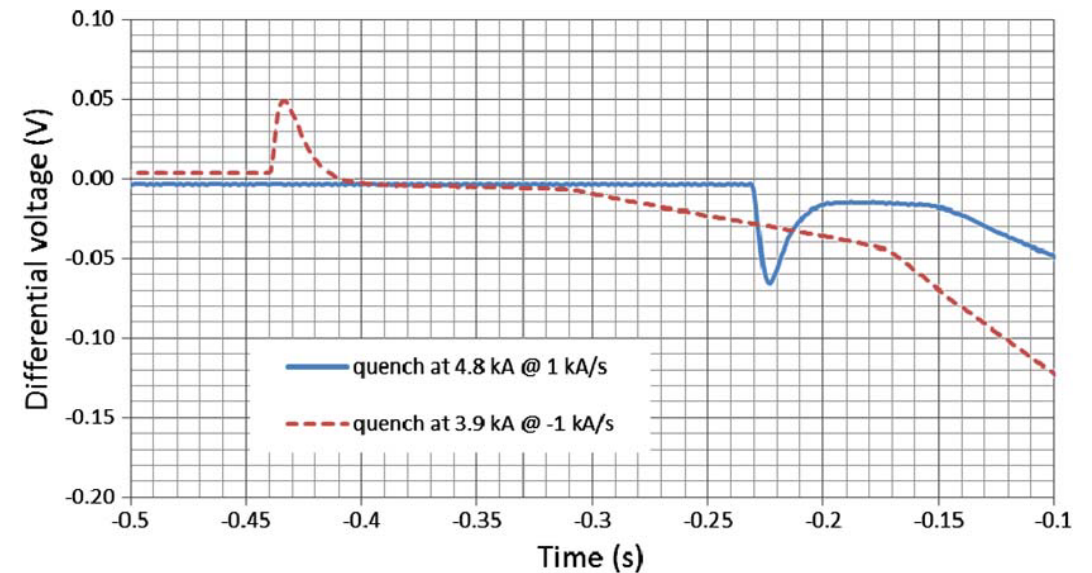


# Test with GSI SIS300 magnet



Test results from INFN-LASA, Milano, 2012

- ▶ 9 kA reached
- ▶ quenches if:  
too much  $\Delta I$  in combination with  
too much  $dI/dt$
- ▶ 50 mV coil difference voltage pulse  
60 ... 100 ms before quench
- ▶ pulse missing during training quench
- ▶ theory: sc loop current in coil head
- ▶ current loop compensates flux locally until  
quench
- ▶ flux redistribution in coil  $\rightarrow$  voltage pulse

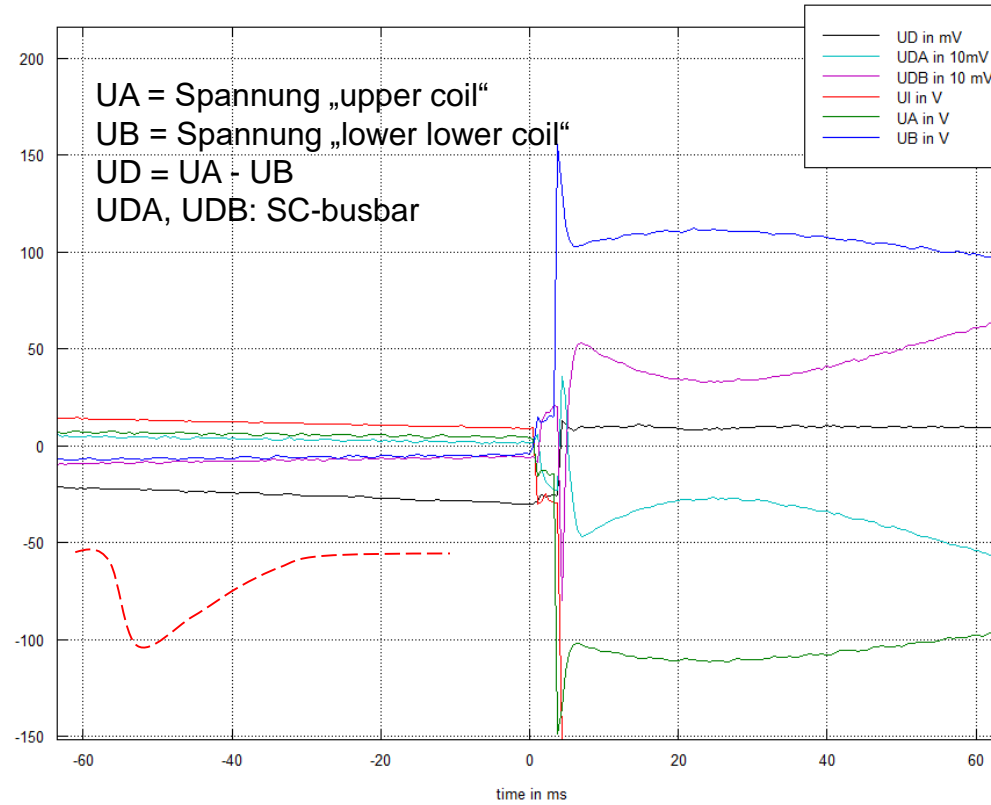
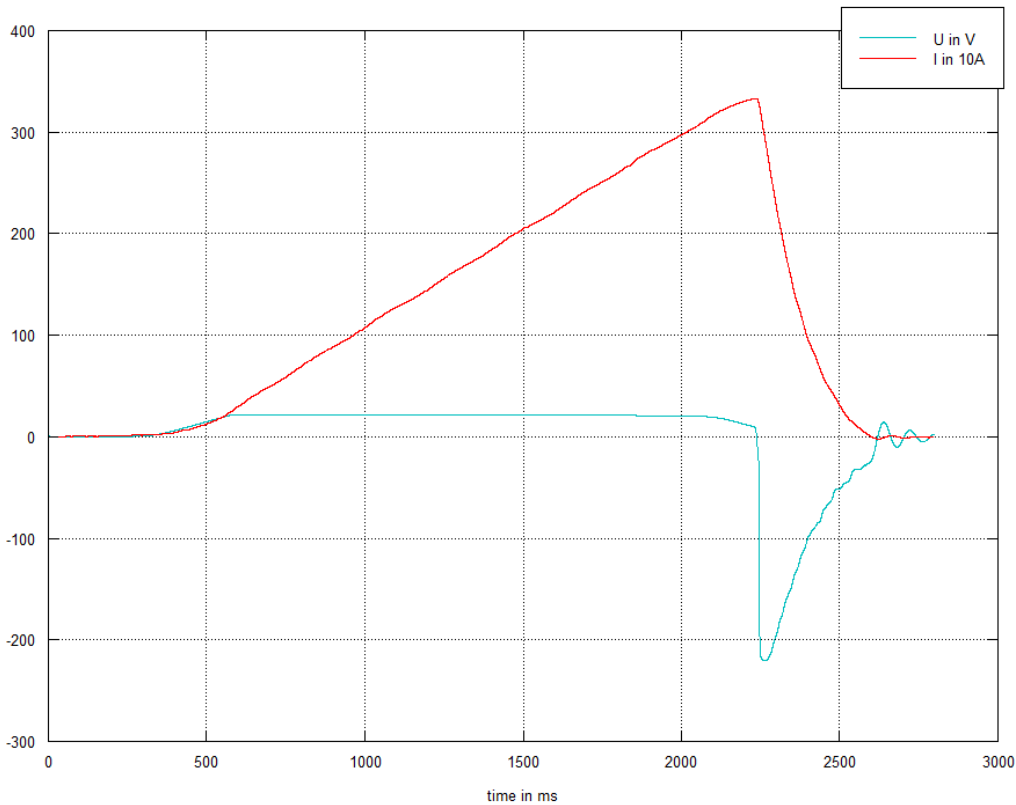


# Test with GSI SIS300 magnet



## Measurement #1

- ▶ 0 A → 3191 A @ 1900 A/s  
triggered @ -20 mV with -0.12 V/s  
peak ramping power 64 kW

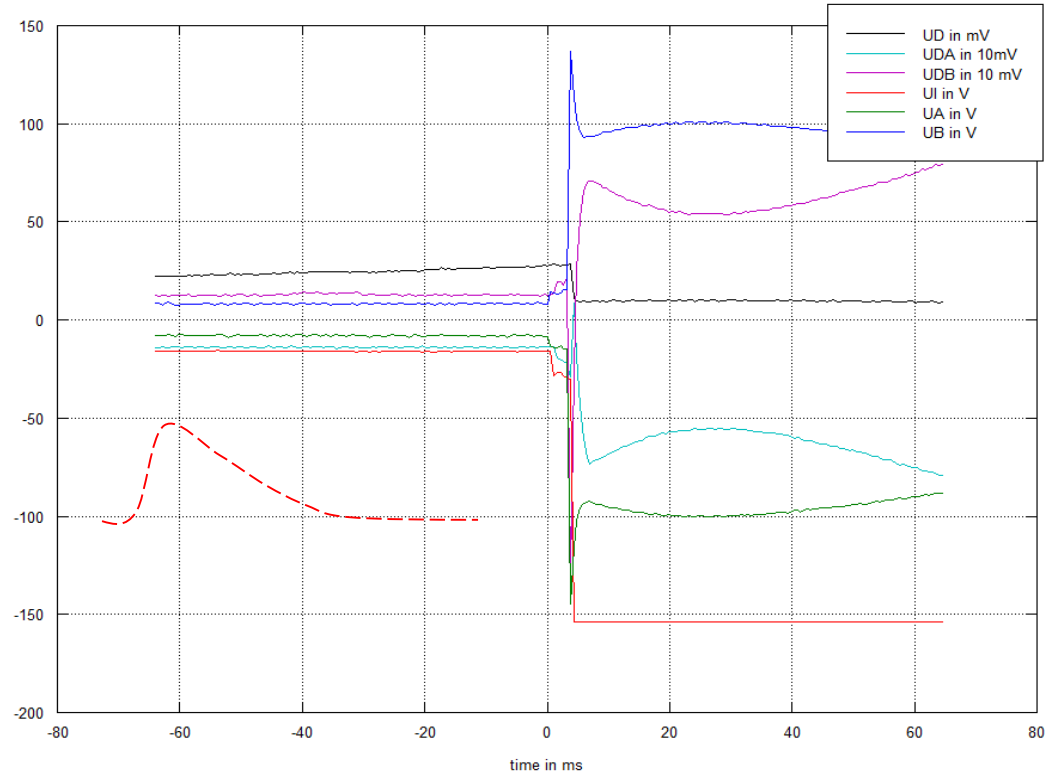
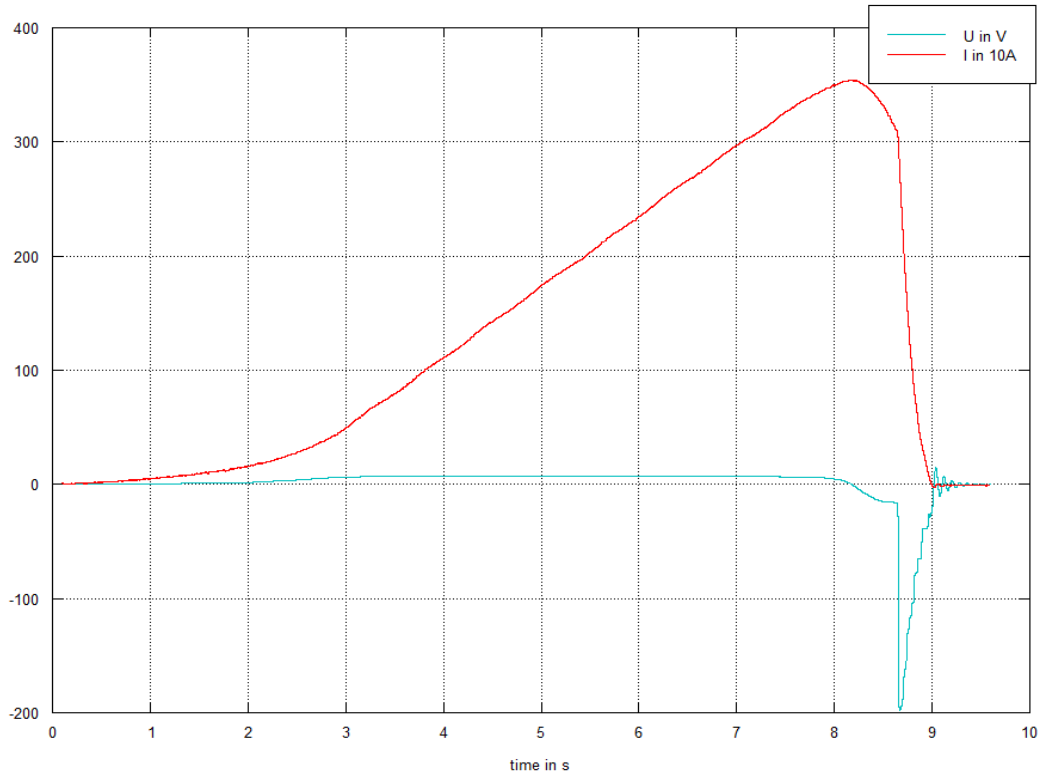


# Test with GSI SIS300 magnet



## Measurement #5

- ▶ 3540 A → 3100 A @ -1,6 kA/s  
triggered @ +30 mV with +0,09 V/s  
peak ramping power -50 kW

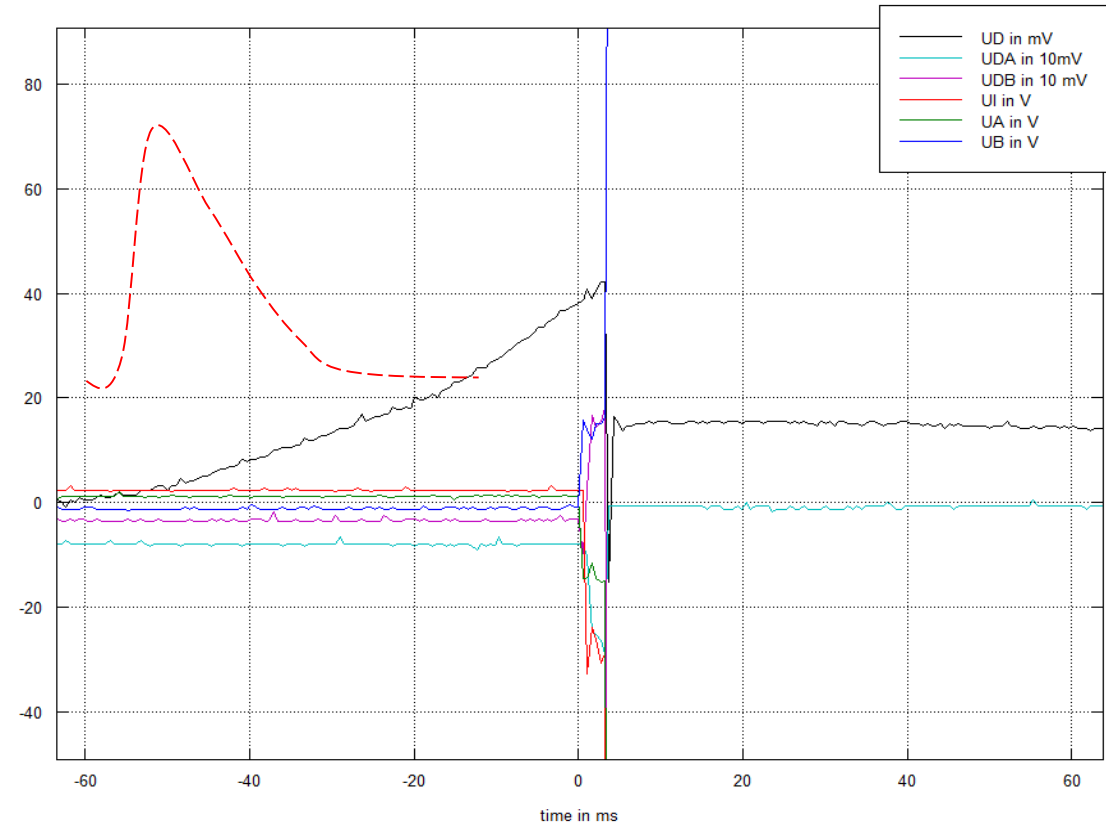
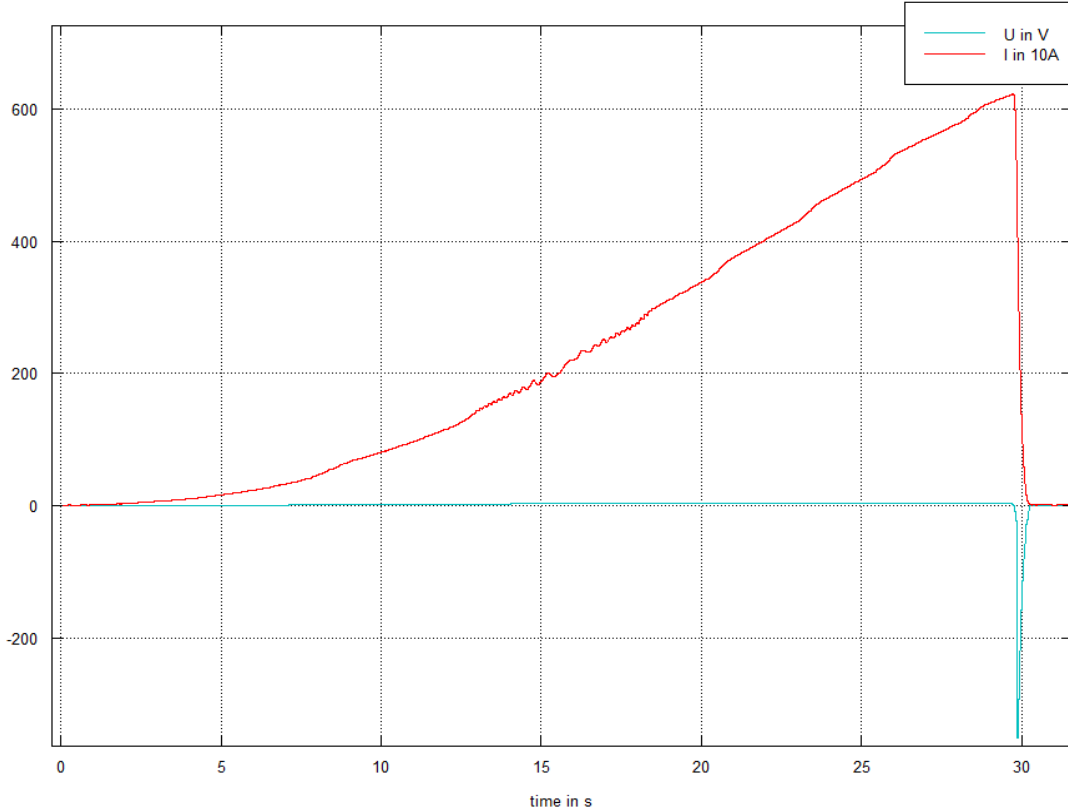


# Test with GSI SIS300 magnet



## Measurement #21

- ▶ 0 A → 6310 A @ +0,20 kA/s  
triggered at +40 mV with +0,67 V/s  
peak ramping power 23 kW, quench 2.8 MW

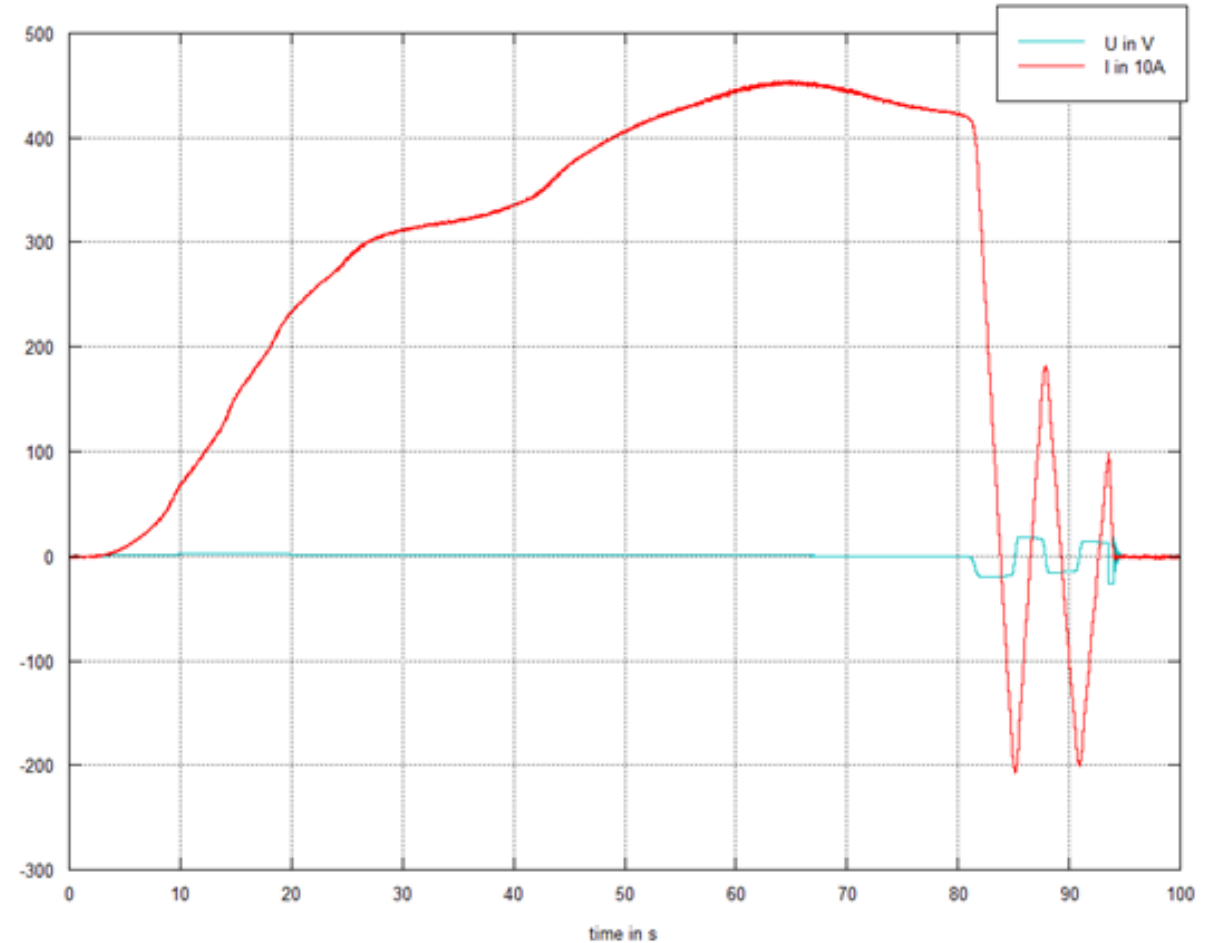


# Test with GSI SIS300 magnet



## Measurement #18

- ▶ +4.3 kA → - 2 kA @ -1,7 kA/s  
no trigger at 20 mV threshold
- ▶ quench expected at +0,1 kA
- ▶ peak ramping power -84 kW



# Test with GSI SIS300 magnet




Two modes of quenches are observed:

- ▶ Magnet quenches in upper coil if ramped fast (no. 1-5, 7-13, 15, 19, 20), differential voltage is inverted from ramp rate
- ▶ Magnet quenches in lower coil if ramped slow (no. 6, 10, 14, 16, 21)
- ▶ Results need more clarification

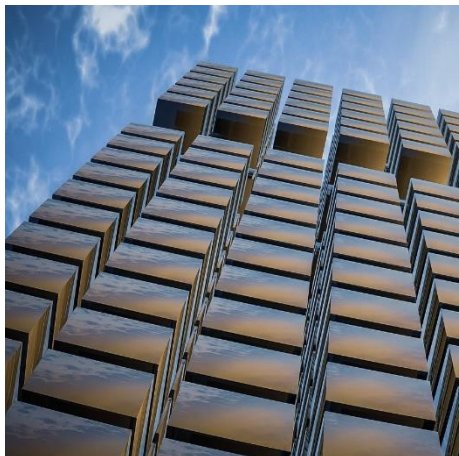
Quench	Initial current in A	Quench current in A	Ramprate in A/s	UD in mV
1	0	3191	1905	-20
2	0	3180	1515	-30
3	0	3350	1666	-30
4	0	3320	1894	-30
5	3540	3100	-1583	28
6	0	3080	333	40
7	0	4870	375	-92
8	0	4020	715	-100
9	0	3660	1430	-83
10	0	3660	1500	-70
11	0	3695	1765	-78
12	0	3920	820	-100
13	0	4190	577	-100
14	0	5810	333	100
15	0	4800	416	-91
16	0	5610	285	100
17	0	4520	100	73
18	0	4400	100	-20
19	0	3380	1953	-30
20	-500	3530	1765	-40
21	0	6320	200	40

# Conclusion



- ▶ The recuperative 4 quadrant supply system works
- ▶ Ramping of magnets: -23 V ... +23 V; -14 kA ... +14 kA
- ▶ High efficiency 97 % (capacitors + converter); total 94 ... 90 % (+ thin copper hoses)
- ▶ Grid power: only ~10 % (e.g. 20 kW / 220 kW)
- ▶ Noise of converter: <10 mV; grid power supply 
- ▶ Current regulation works, was improved in the meantime
- ▶ High compactness (3 cabinets 19")
- ▶ Adjustable fast quench protection system (reaction time < 5 ms)

*Miteinander forschen  
Wirtschaft stärken  
Perspektiven schaffen*



# Thank you for your attention!

## Questions???

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# References



[1] <https://www.fotocommunity.de/photo/schwungrad-maexken/44108211>