







Reminder:

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After more than 10 years of prototype program

- Q3 2019 Call for tenders for Fused silica bars successful
 - Sep 5, 2019Placed order for 98 bars with option for up to
8 more bars (need 96) with Nikon Corp, Japan.
- Sep 2019 Production started
 - March 20 Received shipment of first lot (5 bars)





GSI	Nikon
1	P23595-1-04
2	P23595-1-08
3	P23595-1-18
4	P23595-1-19
5	P23595-1-20







THS IS TO CERTIFY PURCHAS	NAT ALL SWITHETIC FUSED SLICA NATERI E ORDER(S) HAVE BEEN PRODUCED IN CON AND DRAWINGS LISTED (ALS AND PARTS INCLUDED IN ALL SHIP FORMETY WITH THE REIGUIREMENTS OF IN THE PURCHASE ORDERS.	KENTS ON THE FOLLOWING SPECIFICATIONS		Nikon
	Cestomer	Information			
Gustomer Name	GSI Helmholtzzentrum für Schwerionen	arachung GmbH			
Customer Part Name	Radiator Bar	PO No.	4500181248		
	Where Mede	al lafe smaller		- 11	
Halasial Conda	NIKON MESER	an anormation	W/00/017.1		
Marchai Graue	NETO'0	Material Int No.	0005051.04	II	
Navi Neterence No.	16304317	ColC Insue Date	2020/2017	II	
		Cuc have bare	2020/2017	- 11	
	Raw Materia	I Specifications'		——————————————————————————————————————	
Internal Transmittance	≥99.9%/cm at 365nm				End 1
Inclusions	No inclusions larger than 2µm			— II	
Homogeneity	High optical homogeneity				llen
Strise	No significant visible striae				Iten
	Dimensional	Specifications'			Length (mm)
Length	1200 +0/-0.5mm				congertining
Width	53 +0/-0.5mm				
Thickness	17 +0/-0.5mm				Midth Immal
Parallolism	<0.5mrad				avious (mm)
Squanness	<0.5mrad				
TTV	<25µm				
	Polished S	pecifications'			Thikness (mm)
Surface roughness (Faces and sides)	<5A rms				
Surface roughness (Ends)	<10Å rms				
Edges	Sharp no bavel				Parallelism [mrad]
Surface quality	Total area of imperfections on	bar surfaces and edges <75mm ²			
	-				Squarenes
Comments :					
Additional Data ((N))					
					Surface roughness [A RMS]
		111 1			
		Hathur /	la auto		
		Authorized Signature	agana	— II	
	NRON CORP.	DRATION	0		TTV [µm]
	Production Department Produ 10-1. Asamizedal 5-chome. Misewikiw Riske	clion Technology Division mihara-shi, Kenagawa 252-0328 Janan			
	to a second s				Edge

		Data Sh	eet								
likow		Data On	001	Lot No.	YKG						
INUT				Material lot No.	P235						
	Polishing lot No.	1-1-									
	Side 2										
		Side 2	//	/							
		ł	///								
			Face 2								
		F800	Side 1								
	/	///									
	End 1										
		-									
	Item		Specification	tool / method	Result						
Length from		Side 1	1200+0/-0.5	CNC Measurement System	1199.89						
Length (mm	a	Side 2	1200+0/-0.5	CNC Measurement System	1199.89						
		End1	53+0/-0.5	CNC Measurement System	52.91						
Width [mm]	1	Middle	53+0/-0.5	CNC Measurement System	52.92						
		End 2	53+0/-0.5	CNC Measurement System	52.91						
		End1	17+0/-0.5	CNC Measurement System	16.95						
Thikness (mr	n]	Middle	17+0/-0.5	CNC Measurement System	16.94						
		End 2	17+0/-0.5	CNC Measurement System	16.94						
Parallelism (m	The	Face-Face	<0.5	CNC Measurement System	0.07						
 arananani fun 		Side-Side	<0.5	CNC Measurement System	0.30						
Sq	uareness [mrad	1	<0.5	CNC Measurement System	Pass						
		Face 1	<5	Zygo "NewView"	3.5						
		Face 2	<5	Zygo "NewView"	2.8						
Surface roughness	A RMS1	Side 1	<5	Zygo "NewView"	4.9						
e en reces rouginious	(, , , , , , , , , , , , , , , , , , ,	Side 2	<5	Zygo "NewView"	4.5						
		End 1	<10	Zygo "NewView"	5.1						
		End 2	<10	Zygo "NewView"	6.1						
		F	<25	CNC Measurement System	13.9						
TTV [um]		Face-Face									
TTV [µm]		Face-Face Side-Side	<25	CNC Measurement System	13.0						
TTV [µm]	Edges	Side-Side	<25 Sharp no bevel	CNC Measurement System Visual inspection	13.0 Pass						

Nikon QA data looks very good, all specs are met or exceeded

- Surface roughness face/side < 5Å end < 10Å
- Parallelism < 0.5 mrad
- Squareness < 0.5 mrad
- TTV < 25 μm

Date bar numer				Lot						Ler	ngth		Width			Thickness	Parallelism			
	Nikon QA	Received	GSI	Nikon	Material	Polishing		Polishing		Side 1	Side 2	End 1	Middle	End 2	End 1	Middle	End 2	Face-Face	Side-Side	
	2/17/2020	3/4/2020	1	P23595-1-04	YK04317-1	1	1	1	1	1 1	1199.89	1199.89	52.91	52.92	52.91	16.95	16.94	16.94	0.07	0.30
	2/17/2020	3/4/2020	2	P23595-1-08	YK04317-1	1	1	2	1	1 2	1199.75	1199.74	52.78	52.78	52.78	16.95	16.95	16.95	0.05	0.08
	2/17/2020	3/4/2020	3	P23595-1-18	YK04317-1	1	1	2	1	1 1	1199.89	1199.89	52.90	52.91	52.91	16.95	16.95	16.95	0.01	0.04
	2/17/2020	3/4/2020	4	P23595-1-19	YK04317-1	1	1	2	1	1 1	1199.87	1199.87	52.92	52.91	52.92	16.95	16.95	16.95	0.05	0.37
1	2/17/2020	3/4/2020	5	P23595-1-20	YK04317-1	1	1	1	1	1 1	1199.89	1199.90	52.91	52.92	52.91	16.95	16.94	16.94	0.10	0.12

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Visual inspection





Quality of internal bar surface (laser scanning system) Bar shape (laser and autocollimator)

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Visual inspection

- At first glance (eye, halogen light):
- clean surfaces, no residue from cleaning or packing, very sharp corners
- At second glance (Laser scanning setup):
- shift of beam spot when bar is scanned through laser
- At third glance (Autocollimator)
- "perfect" parallelism of faces
- fuzzy image for parallelism of sides





Quality of internal bar surface (laser scanning system) Bar shape (laser and autocollimator)

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Ends and sides show fuzzy image – Values for parallelism and squareness can not be determined



sides

ends



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When the laser beam passes straight though the bar, the shape of the sides has not influence.

Any deviation of the laser spot position on the wall from the initial position provides hints regarding refractive index variations over the bulk.

The deviation can be in the x- and/or y-direction.





Laser tests – effect after internal reflections

Primary photon propagation direction in a DIRC is along the length of the bar – check if the effect is larger or similar for photons bouncing never/few times/many times between the two bar faces



- n: number of internal reflections
- The bar was scanned over its thickness from face2 to face one
- The shift is shown relative to the spot position of each first laser entrance

Impact of effect is smaller for larger internal photon angles



coefficient of total internal reflection (48 reflections)

Determined transmission probability (along long bar axis) and

Transmission scan examples:

- $T \approx 99.6\%/120$ cm at 442 nm (bar 1)
- T ≈ 98.2%/120cm at 325nm (bar 3)

Reflection coefficient examples:

- $R \approx 0.9998$ at 442nm (bar 2)
- $R \approx 0.9984$ at 325nm (bar 3)

Good T/R results so far, meet DIRC requirements

Laser scanning setup – measurements





Steering of Laser Beam by the Bulk Material



When the laser beam passes straight though the bar, the shape of the sides has not influence.

Any deviation of the laser spot position on the wall from the initial position provides hints regarding refractive index variations over the bulk. (note that bar ends were found to be flat)

The deviation can be in the x- and/or y-direction.



Transmission mode, Laser moved over thickness of 17mm



Observed position shift during thickness (17mm) scan

Bulk Beam Steering (thickness scan, y deflection)











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Shift of Internally Reflected Laser Beam



Propagation of light inside of the bar with multiple internal reflections is the "normal" use-case in the DIRC.

The bar is moved (by the motor) through the laser beam, the beam is reflected internally 16 times from the sides



The laser beam should remain at the same height inside the bar and exit at the same height it enters the bar.

The laser spot on the wall ought to always be at the same position.

Any shift of the laser spot is a sign of reflections from a non-flat surface and/or steering from layers of varying refractive indices (striae).



Shift after 16 reflections from the sides at bar exit

Shift of Internally Reflected Laser Beam





"bulk steering effect" from side reflections 2-3 times larger for Nikon bars than for BaBar bar

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Shift of Internally Reflected Laser Beam





Detailed scan for bar #6, different laser entry positions No significant dependence of entry position along width Consistent result if bar is turned (end 1 -> end 2)

Observed "beam steering" results for all Nikon bars consistent with reflections from non-flat surfaces and/or steering from layers of varying refractive indices (striae) (cannot be distinguished by this method). Shift after 16 reflections from the sides of the Nikon bar 6 at bar exit









Check of deformation using external laser reflection

Simplified model: polygonal approximation

Laser beam deflected by local surface

Record laser spot displacement Δy

for different positions along 17 mm side





Check of deformation using external laser reflection

Example result for one position along bar length for bar 3

- > large positive laser spot displacement near top of side
- > no displacement near middle of side
- > large negative displacement near bottom of side

Calculate local angle θ , local sagitta Δx , side sagitta:

 $\theta \approx 0.05...0.15 \text{ mrad}$

 $\Delta x \approx 0.04...0.16 \ \mu m$

side sagitta $\approx 0.6~\mu m$





Values differ for bars and positions along length (same seen in CMM data)

Qualitative agreement: convex shape with few micron sagitta (details vary due to difference in measurement location)



Study of laser beam deflection from the sides



A flat surface would result in a constant beam spot position across the bar side.

A slope is caused by a convex or concave surface.

The reflection measurements from all bars

(see following pages) show a slope consistent with different non-flat (convex/concave/sloped line) shapes









The crossed lines are consistent with side surfaces with opposite curvature (convex plus concave)







The non-crossing lines are consistent with

"almost straight" slopes of the side surfaces.

- The following measurements (next 3 pages) show that, consistent with the Nikon CMM data,
 - the first impression of only convex shaped sides

surface was too simple; bar shapes deviations are more complex and vary along bar length. GSI Helmholtzzentrum für Schwerionenforschung GmbH



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Summary of Bar Shape Examples from CMM















Deviations from ideal bar shape shown for narrow sides, position 3mm from End 2 (Nikon CMM data, deviation scaled by factor 1000.)

Summary of Bar Shape Examples from CMM



GSI number	Nikon number					sid	e 1				side 2											
1	P23595-1-04	convex	slope	slope	slope	convex	convex	concave	slope	slope	convex	concave	convex	convex	convex	convex	slope	convex	convex	convex	slope	
2	P23595-1-08	concave	convex	concave	convex	convex	slope	concave	slope	concave	convex	slope	convex	slope	slope	convex	convex	slope	slope	convex	slope	
3	P23595-1-18	slope	slope	slope	slope	convex	convex	slope	concave	slope	slope	slope	slope	slope	slope	convex	convex	slope	slope	convex	slope	
4	P23595-1-19	slope	convex	slope	slope	concave	convex	slope	slope	convex	slope	slope	convex	slope	slope	slope	slope	slope	slope	convex	convex	
5	P23595-1-20	slope	slope	convex	slope	convex	convex	slope	convex	slope	slope	slope	convex	slope	slope	convex	convex	slope	slope	convex	slope	
6	P23595-1-03	slope	concave	slope	slope	convex	convex	slope	slope	convex	slope	slope	convex	convex	convex	convex	convex	slope	convex	convex	slope	
7	P23595-1-05	slope	convex	slope	slope	slope	concave	slope	slope	convex	slope	slope	slope	slope	convex	convex	concave	concave	concave	convex	convex	
8	P23595-1-07	slope	convex	slope	slope	convex	slope	convex	slope	slope	slope	slope	slope	slope	slope	convex	slope	slope	slope	convex	slope	
9	P23595-1-09	convex	convex	convex	concave	slope	convex	concave	concave	slope	slope	slope	convex	slope	slope	convex	convex	slope	slope	convex	slope	
10	P23595-1-13	slope	convex	slope	slope	convex	convex	slope	slope	convex	slope	slope	convex	slope	slope	slope	slope	concave	slope	convex	convex	
11	P23595-1-15	slope	convex	slope	slope	convex	convex	slope	slope	slope	slope	convex	concave	convex	slope	convex	convex	slope	slope	convex	concave	
12	P23595-1-17	slope	convex	slope	convex	slope	convex	concave	slope	convex	convex	convex	convex	convex	slope	concave	slope	convex	convex	convex	convex	

Illustration of the type of the side shape deviation, using the 10 CMM measurements provided across the length of the bars.

Note that the shape category changes across the length of the bar.

(Based on Nikon CMM data, shape definition as shown above;

"slope" may be curving inward or outward, may be close to concave or convex in shape)





Simulation of striae on DIRC performance





Nikon measurements: Maximal deviation of less than 7 ppm

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Simulation of non-symmetric shape on DIRC performance



Nikon measurements: Maximum Sagitta around 10 mum

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- QA for acceptance of the Nikon bar ongoing series of Zoom meetings with Nikon
- The Nikon CMM data and our laser measurements show combinations of convex and concave shapes and that these shapes vary across the length of the bars, not what we initially expected
- Result from Test and Simulation:
 - Striae and Deformation of Sides are no reason not to accept the bars
- Those tests delayed the determination of possible subsurface damage
- Setup needs to be prepared or adapted to "beam steering bars"
- First results from internal reflection measurements for 442nm are promising





Thank You





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Simulation of the laser beam (390 nm) along the bar. The bar has 100 layers which create 10 ppm gradient of refraction index. Position shift X along the bar thickness (outer bands for 3 mrad angle between laser beam and bar axis; inner for 2 mrad; upper two bands for photons with angle increasing in the direction of higher refraction index, lower two - opposite direction) :

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