A 3D wireframe model of the SIS100 superconducting magnet ring, showing its complex, multi-segmented structure. The ring is composed of numerous individual magnet segments, each with a grid-like internal structure. The segments are arranged in a large, roughly circular loop with several smaller sections and connections. The model is rendered in a light gray wireframe style, highlighting the intricate geometry of the magnet assembly.

# **Superconducting magnets for SIS100 (from design to series testing)**

Anna Szwangruber et al., department of superconducting  
magnets, GSI

Achievements which will be presented in this talk were only possible with a long term highly professional contribution of the colleagues from SCM, ENG-NCM, CRY, ENG, EPS, VAC, QA, BB, TRI, MEWE, collaboration and business partners of GSI.

# Outline

- Introduction
- SC magnets for SIS100
  - why sc technology?
  - magnet design
    - main magnets
    - corrector magnets
- SIS100 dipole magnets
  - development
  - lessons learned from prototypes
  - series production
- Testing of series dipole magnets
  - Testing strategy
  - GSI test facilities
  - Main measurement systems
  - The team for dipole testing
  - Test results
- Next activities at test facilities for sc magnets
- Summary

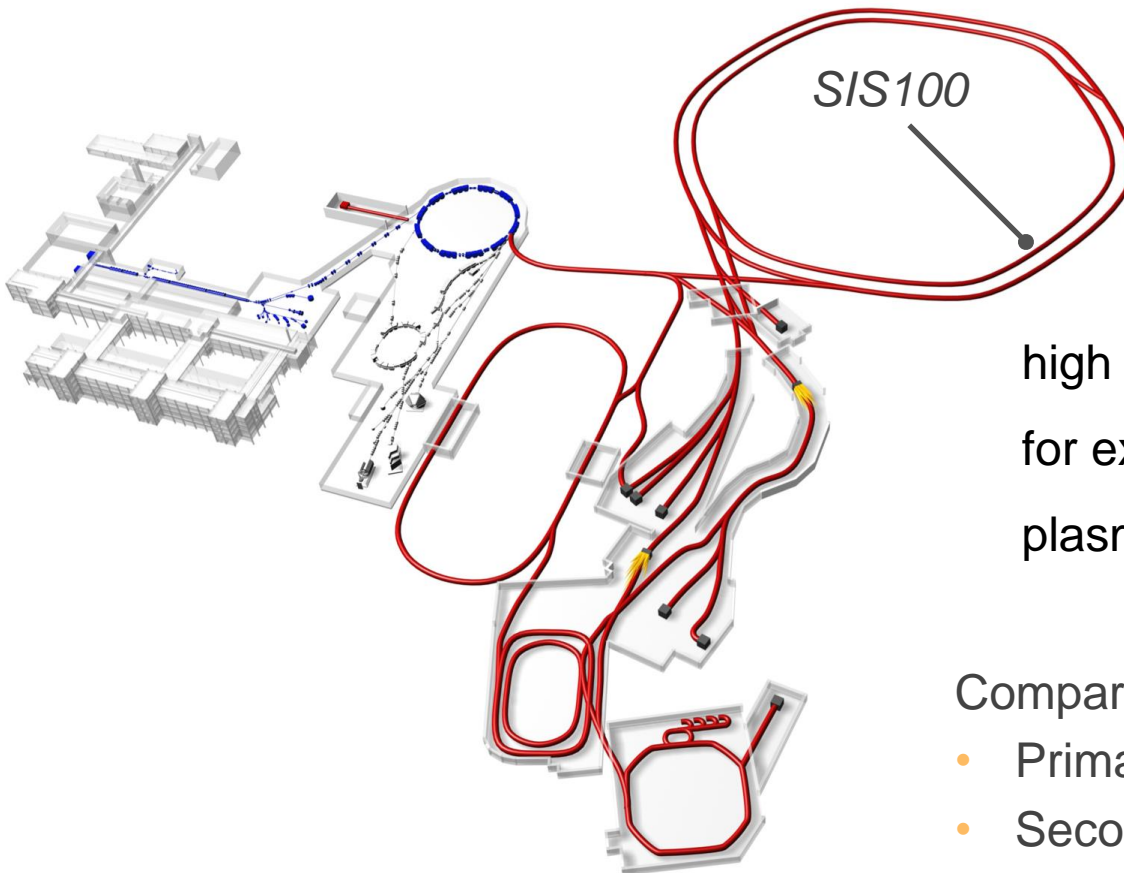
# Facility for Antiproton and Ion Research



*Existing GSI facility*

*FAIR facility*

*International project*



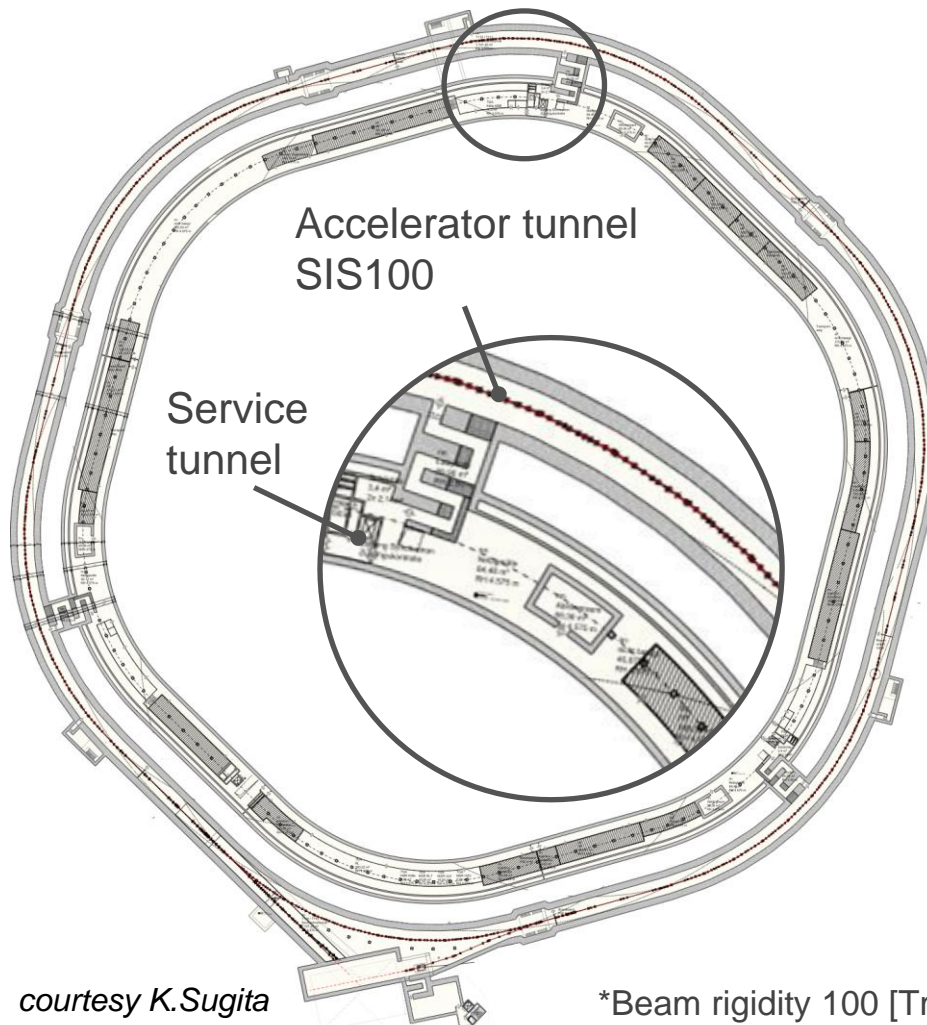
high intensity ion and antiproton beams  
for experiments in nuclear, atomic,  
plasma physics and material science

Compare to the existing GSI facility

- Primary beam intensities: **×100**
- Secondary beam intensities: **×10000**
- Primary beam energies: **×10**
- Antiproton production

# Heavy Ion Synchrotron SIS100

SIS100 = **S**chwerionensynchrotron 100 [Tm] = Heavy ion synchrotron (beam rigidity\*) 100 [Tm]



Hexagonal, circumference 1083.60 m

Superconducting (magnet)  
accelerator

Fast-ramp Machine  
~0.5 sec. to maximum field.

*courtesy K.Sugita*

\*Beam rigidity 100 [Tm] = Bending dipole field 1.9 [T] × Bending radius 52.632 [m]

# SC Magnets for SIS100 – Why SC Technology?

## Radioactive beam program:

$5 \cdot 10^{11}$   $U^{28+}$  ions per pulse,  
acceleration to 2.7 GeV/u

## Antiproton production:

$2.5 \cdot 10^{13}$  protons per pulse,  
acceleration to 29 GeV



$B_{max} = 1.9$  T, field err.  $B_n/B_m$   $6 \cdot 10^{-4}$   
 $dB/dt = 4$  T/s , cycle frequency  $\sim 1$  Hz

## operation with $U^{28+}$

vacuum pressure  $\sim 10^{-12}$  mbar

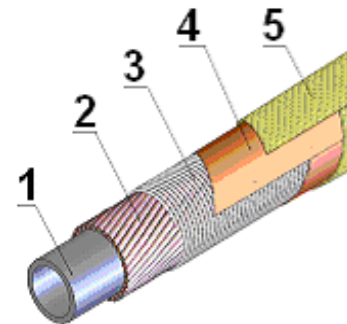


cold vacuum chamber @ 15 K  
for the cryo pumping

## Principles of the magnet design

- iron dominated (super-ferric) magnets
  - superconducting (sc) coil
  - Nuclotron cable
  - cooling by two phase Helium @ 4.5 K
  - low AC losses magnets
- (to remove 1W @ 4.5K 300W @ 300K are needed)

## Nuclotron cable:



- 1 - Cooling tube CuNi
- 2 - SC wire NbTi
- 3 - CrNi wire
- 4 - Kapton tape
- 5 - Glasfiber tape

# SC Magnets for SIS100 – Why SC Technology?

## Normal Conducting (NC)

- $B_{\text{dipole}}$  only 1.9 T... typical regime for NC magnets
- AC operation (1 Hz) → AC losses in the magnetic yoke and in Cu windings
- Lower construction cost but higher operation cost
- Ultra high vacuum (UHV)  $10^{-7} \dots 10^{-12}$  mbar  
→ Cryo adsorption pumping → beam chamber at 10-15 K →  
**sophisticated cryostat and cryoplant required for the beam chamber**
- Access to the magnet parts and instrumentation → easy maintenance
- **Large cross-section → large machine size**

## Superconducting (SC)

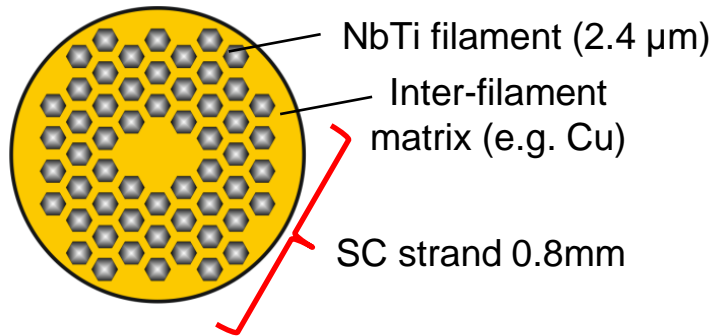
- No DC losses but we aim for AC operation anyway...
- Higher construction cost but lower operation cost
- **Ultra high vacuum  $10^{-7} \dots 10^{-12}$  mbar**  
→ **Cryo adsorption pumping → beam chamber at 10-15 K → no problem since we anyway need LHe for SC coils**
- Required cooling and quench detection/magnet protection systems
- Difficult access to the magnet parts → magnet is immersed into a cryostat
- **Low cross-section → compact machine size**

SIS100 is SC because of UHV requirements



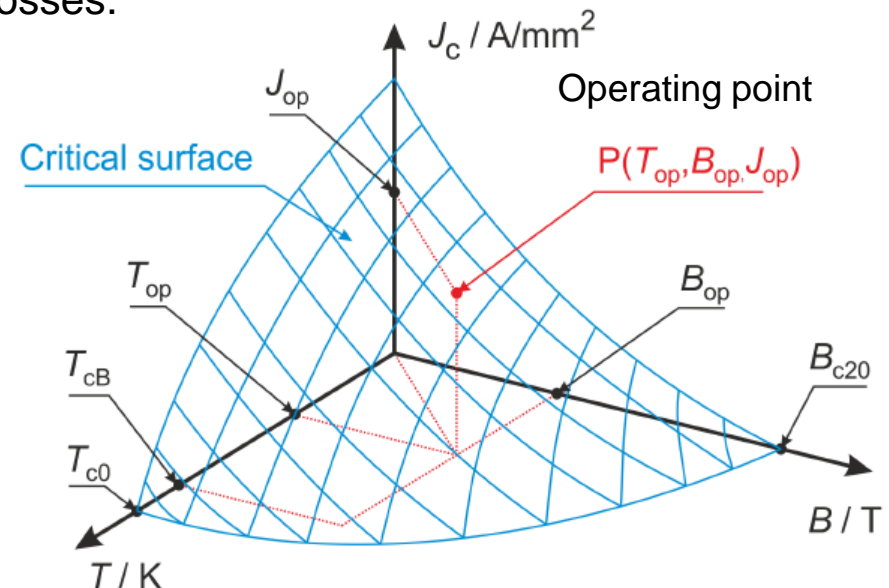
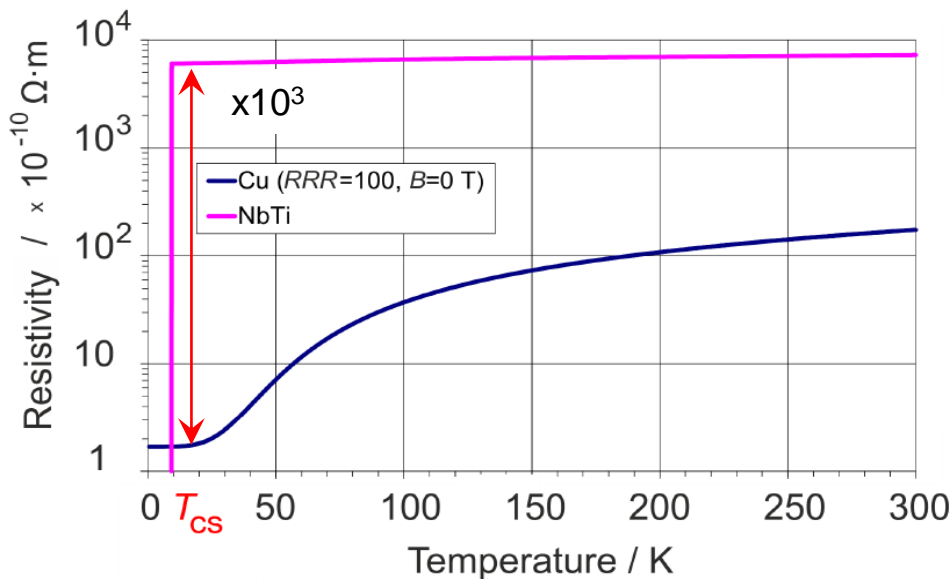
# Superconducting Magnets and Quench

Conductor: **NbTi** – “work horse” for superconductivity (LTS type II, alloy);  $T_{c0}=9.2$  K,  $B_{c20}=14.5$  T.



**Quench** – sudden transition from the superconducting state to normal conducting (resistive) state.

Origin: conductor movement (friction), poor cooling, beam losses.



“P” below the critical surface → **SC**

“P” beyond the critical surface → **NC**



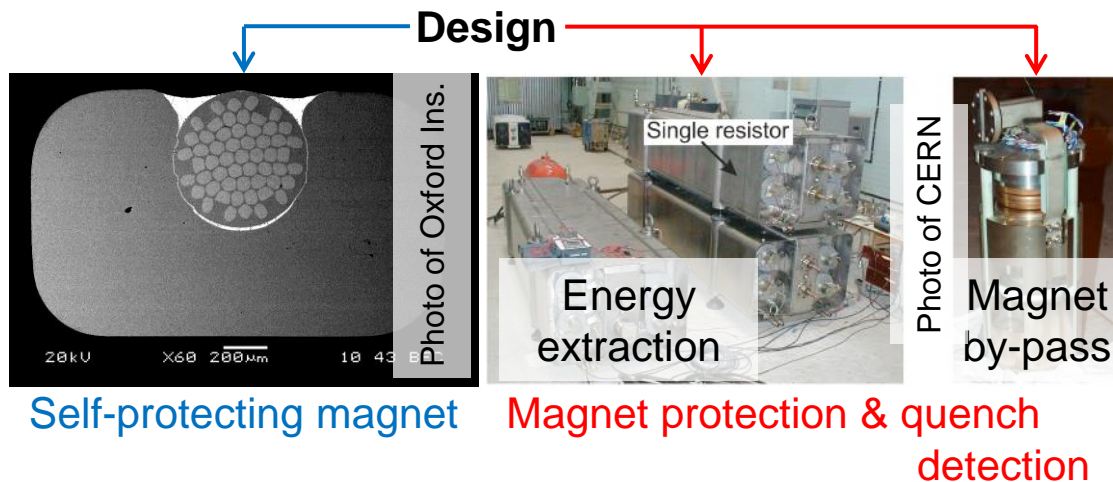
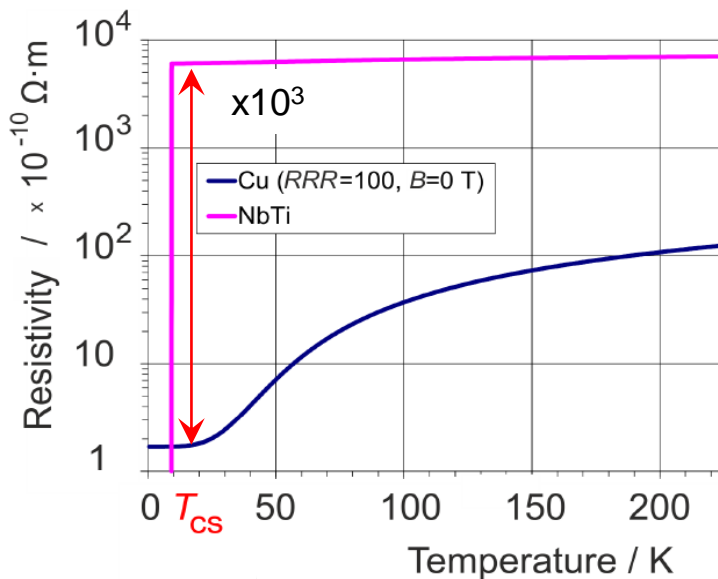
# Superconducting Magnets and Quench

A quench is a natural phenomenon! Therefore it shall be taken into account in the machine design as a **normal operating** condition.

Is a **quench** dangerous?

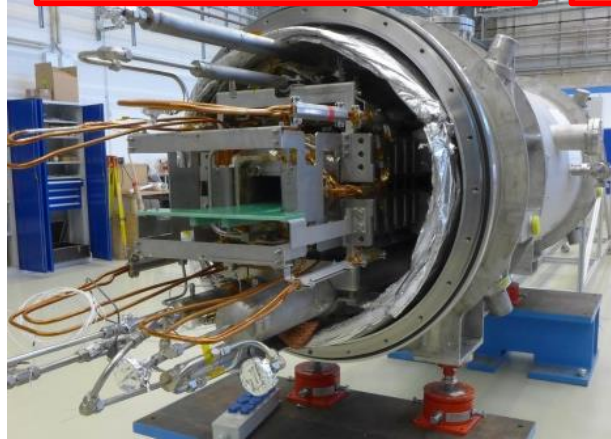
SC NbTi  $\rightarrow$  1000–3000 [A /mm<sup>2</sup>] at 4 K and 5 T

Cu  $\rightarrow$  2 (el. installations) – 20 (extreme cooling) [A /mm<sup>2</sup>]

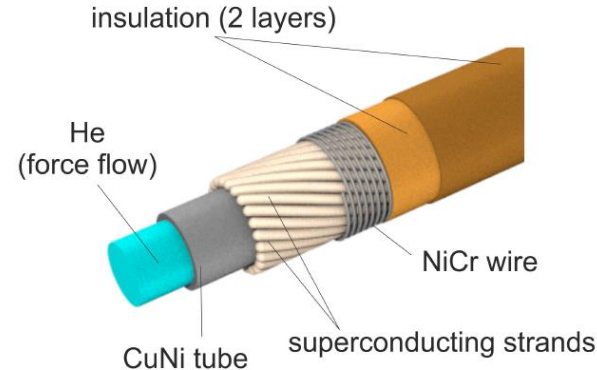


# SIS100 Dipole Magnet: Low AC Loss SC Cable

SIS100 dipole prototype



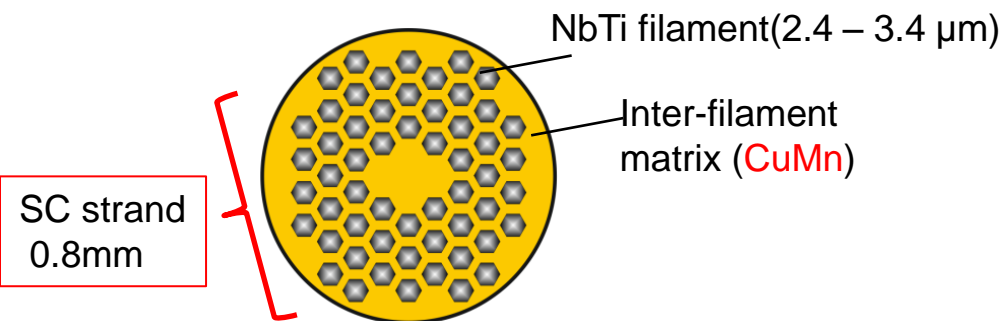
Low AC-loss cable (CuMn matrix)



hysteresis loss in NbTi

$$P_h \propto d_f, \quad P_{ifc} \propto \frac{t_{pf}^2}{\rho_{IF}}$$

inter-filament loss:  
eddy currents through  
the matrix

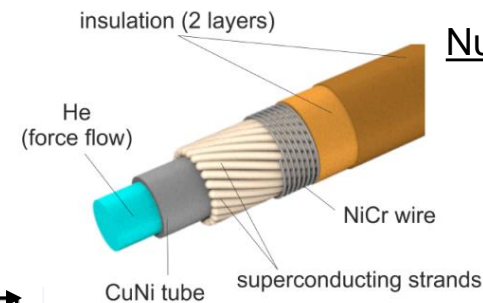
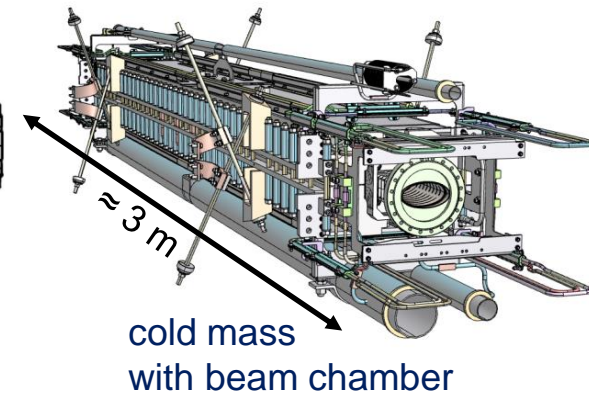
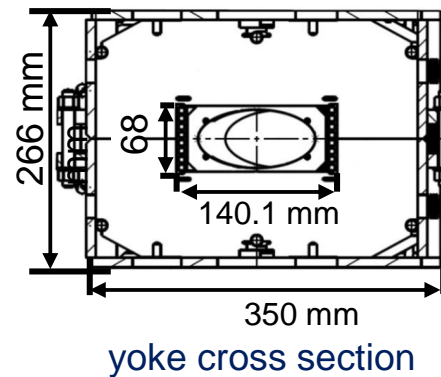


Quench back effect is not expected!  
If a single magnet quenches, other  
magnets will not quench due to high  
 $di/dt$  at current extraction  
(very low probability).

# Superconducting Magnets for SIS100

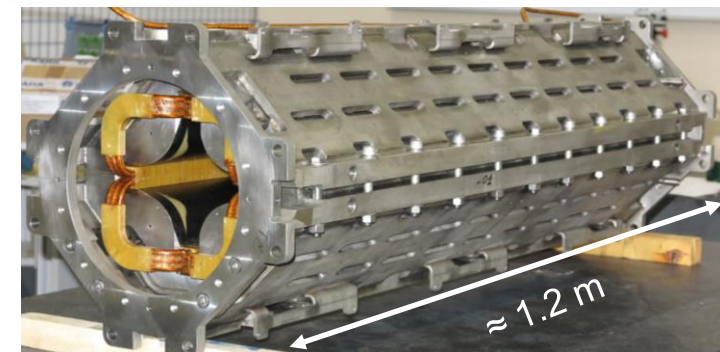
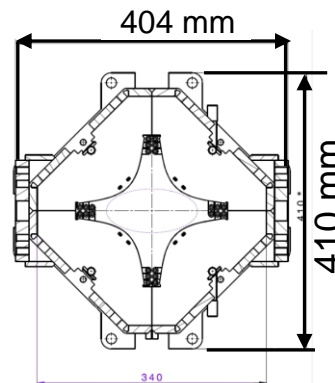
## Main Dipole Magnets

- super-ferric 1.9T
- window frame, curved magnet R 52.632 m
- Nuclotron-type cable
- fast ramped 4T/s
- cooling with 2 phase He
- 108 Magnets



## Main Quadrupole Magnets

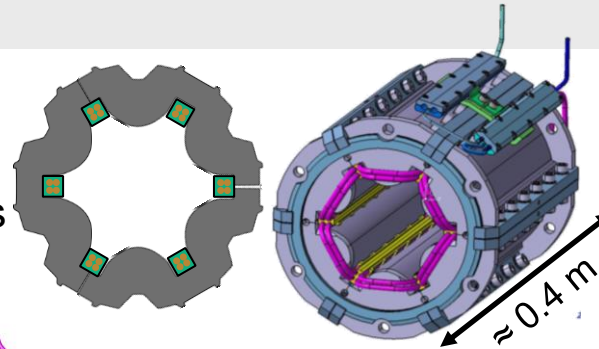
- super-ferric, 27.7 T/m
- Nuclotron cable
- cooling with 2 phase He
- 166 Magnets



# Superconducting Magnets for SIS100

## Chromaticity sextupole:

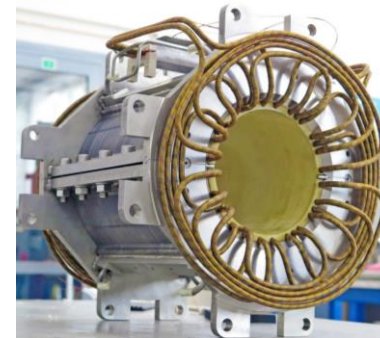
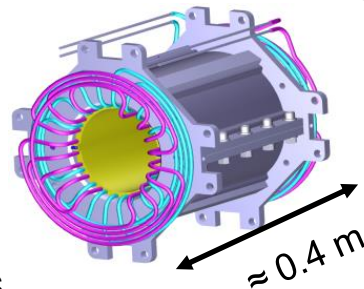
- Super-Ferric 232 T/m<sup>2</sup>
- Nuclotron cable with insulated strands
- 42 Magnets



*photos courtesy JINR*

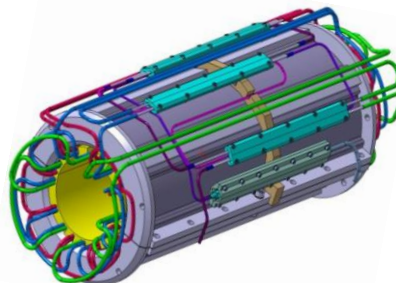
## Steering magnet:

- Cos- $\Theta$
- Nuclotron cable with insulated strands
- Nested (horizontal and vertical correction)
- 83 Magnets

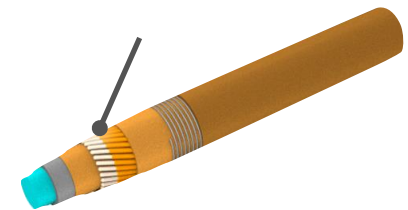


## Multipole corrector magnet:

- Cos- $\Theta$
- Nuclotron cable with insulated strands
- Nested (B2, A3, B4) correction
- 12 Magnets



Insulated Sc. strands connected in series



$$250\text{A} \times 27 \text{ Strands} = 6.75\text{kA}$$



# Superconducting Magnets for SIS100

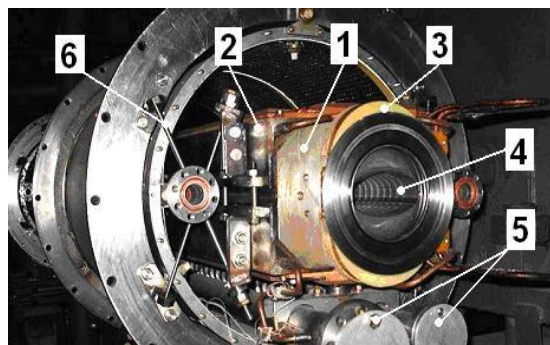


	Unit	Main Dipole	Main Quadrupole	Chromaticity sextupole	Steerer (nested h/v)		Multipole correctors (nested)		
							Quadrupole b2	Sext. (skew) a3	Octupole b4
Design		super-ferric	super-ferric	super-ferric	$\cos\theta$		$\cos\theta$	$\cos\theta$	$\cos\theta$
Number of Magnets		108	166	42	83		12	12	12
<u>Magnetic field strength</u>	T/m <sup>n-1</sup>	1.9	27.77	232	0.372	0.366	0.91	31.8	446
Effective length	m	3.062	1.264	0.383	0.403	0.410	0.62	0.59	0.56
Usable aperture	mm	133x65	133x65	135x65	135x65		133x65		
Ramp time to Max.	sec.	0.5	0.5	0.175	0.2		0.175		

415 sc magnets of different type are needed for the magnetic system of SIS100  
411 + 4 ( inj. / extr. quadrupoles)

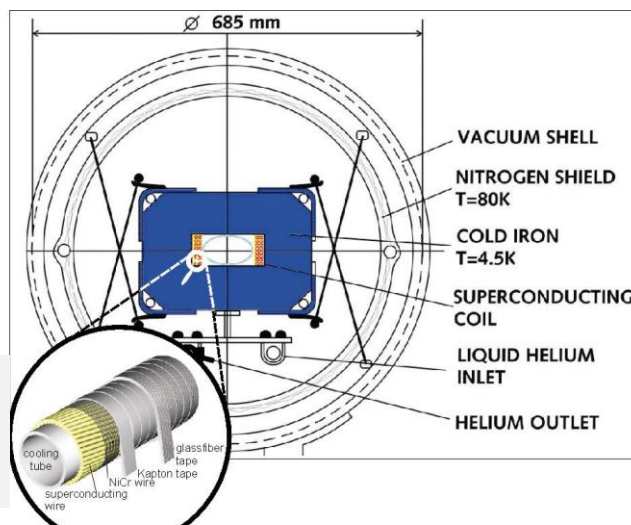
# SIS100 Dipole Magnets: Development

SC magnets for Nuclotron synchrotron - starting point for SIS100 magnets



Nuclotron dipole inside cryostat:

1 - yoke end plate, 2 – brackets, 3 - coil end loop, 4 - beam pipe, 5 - helium headers 6 - suspension



Nuclotron quadrupole inside cryostat

- Nominal gradient: 34 T/m
- Ramp rate: 68 T/m·s

## Main parameters

		Super ferric, window-frame, 2 layer coil with 8 turns per pole
Effective length $L_{\text{eff}}$	m	1.426
Usable aperture	mm x mm	55 x 110
Bending angle	deg.	3.75
Bending radius	m	22.5
Nominal Field	T	1.9 @ 6kA
Ramp rate	T/s	4

**Nuclotron-Synchrotron 160 SC magnets (dipoles and quadrupoles) for magnetic system**

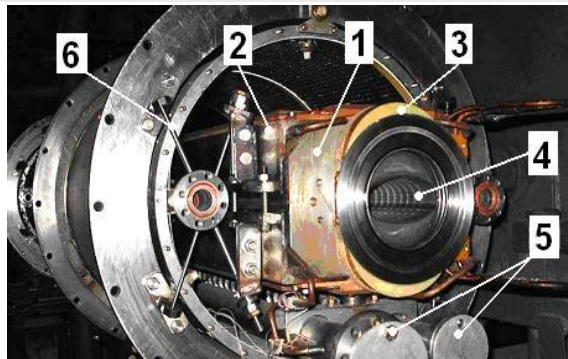
# SIS100 Dipole Magnets: Development

2001 - start of the R&D program

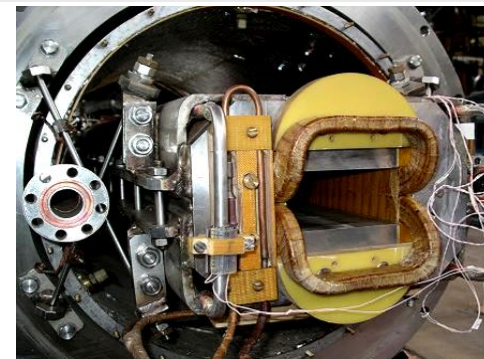
2001 – 2005 multiphysics FEM simulations (2D, 3D) and tests on the short models ( > 20 different short magnet models were constructed and tested)

Goals of the design optimizations on short models and FEM:

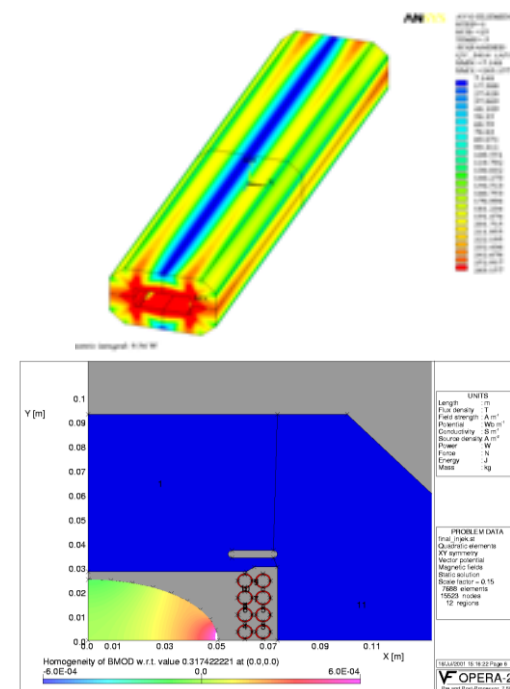
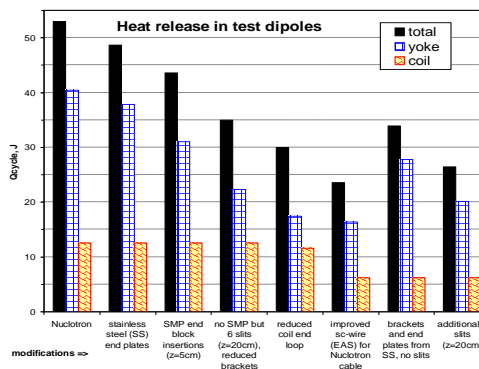
- reduction of the AC losses,
- improvement of the field homogeneity by optimizing the lamination geometry
- precise positioning of the sc-cable
- mechanical stability of the coil ( $\geq 2 \cdot 10^8$  cycles)



Nuclotron dipole

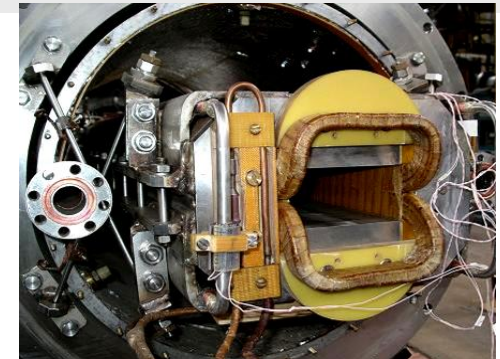
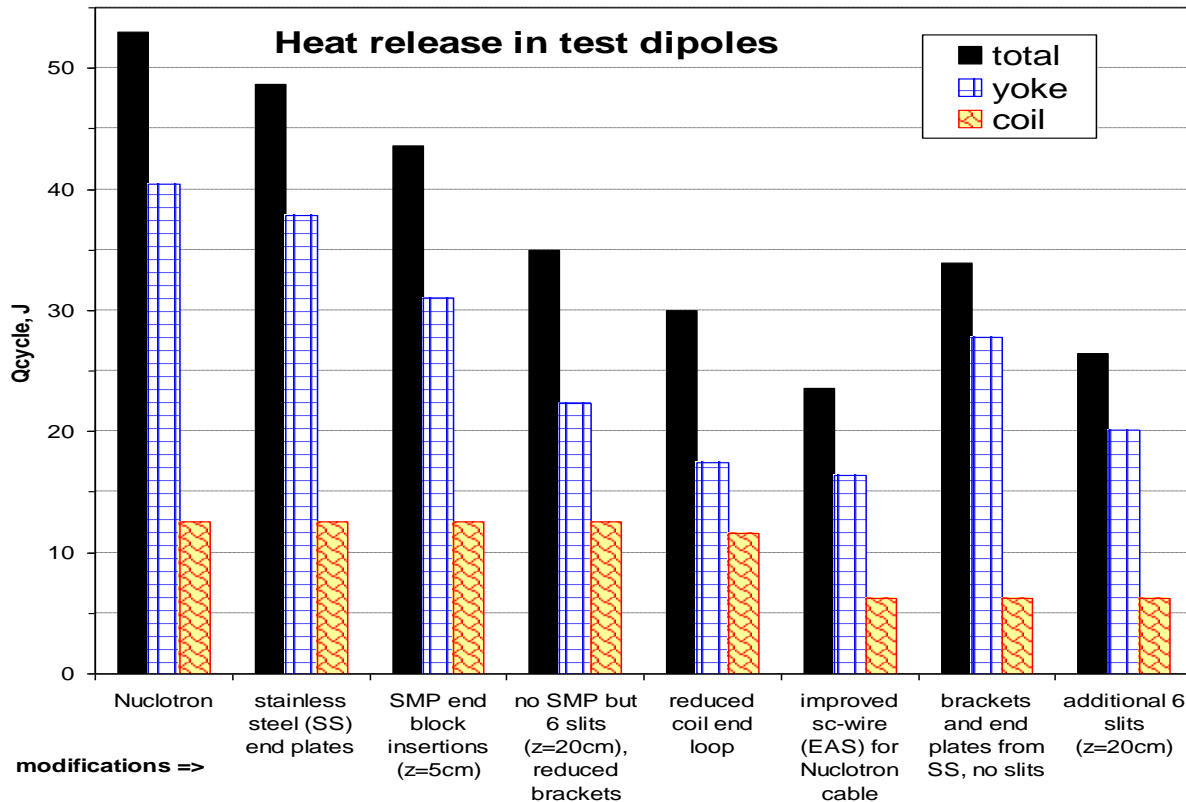


short model - 4KDP6a





# SIS100 Dipole Magnets: Development

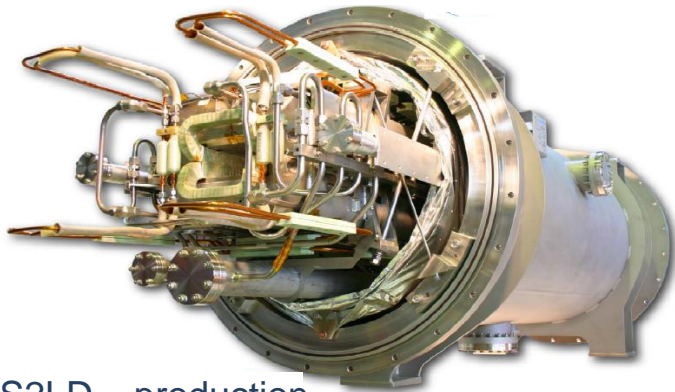


## Optimised design for SIS100 magnets:

- brackets, end plates made from SS
- laser cut lamination slits
- optimized lamination geometry
- minimized coil ends
- new coil package structure
- new sc wire with higher current density and lower losses

*courtesy E.Fischer*

## Full size models

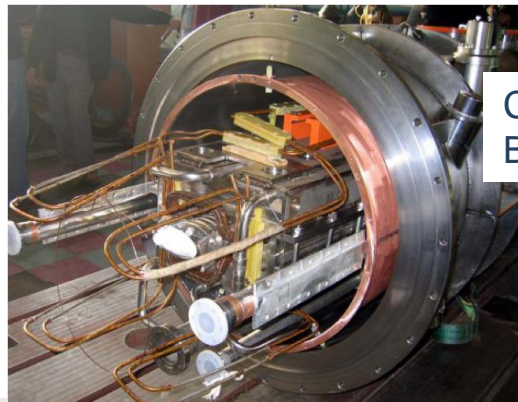


S2LD – production  
Babcock Noell GmbH

### Objectives:

- practical evaluation of the magnetic, cryogenic, mechanical properties of the magnets
- evaluation of the different manufacturing technologies:
  - cable production (dry/wet)
  - coil winding,
  - precise positioning of the cable
  - long term mechanical stabilisation of the coil
- impact of the steel properties AC losses and field properties

S2LD – production JINR Dubna



C2LD – production  
BINP, Nowosibirsk

*Photos courtesy BNG, JINR, BINP*

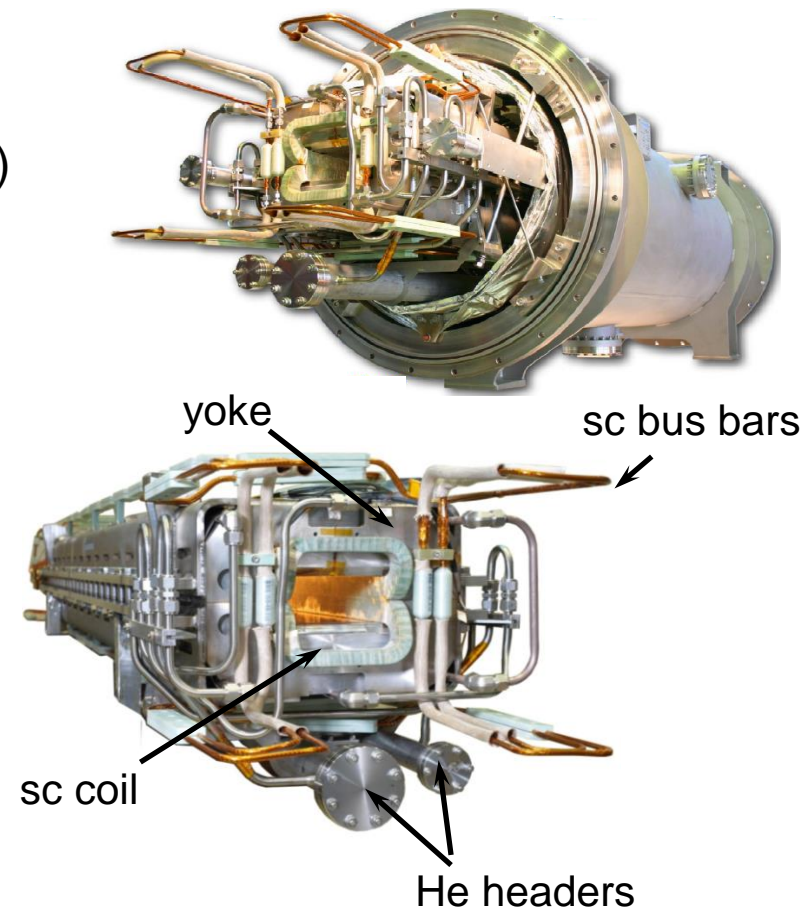
# SIS100 Dipole Magnets: Development

First full size prototype for SIS100 dipole – S2LD

produced by Babcock Noell GmbH

tested @ GSI Dec. 2008 – Nov.2009 (6 test runs)

Design		Window-frame, straight laminated cold iron yoke, lamination thickness 1mm, two layer coil with 16 turns, <b>steel M700-100</b>
Effective magnetic length L	m	2.76
Useable aperture	mm	130 * 60
Bending angle	deg	3 1/3
Bending radius	m	47.36
Bmin	T	0.253
Bmax	T	2.1
Current at max. field	A	7500
Ramp rate	T/s	4



*Photos courtesy: Babcock Noell GmbH.*

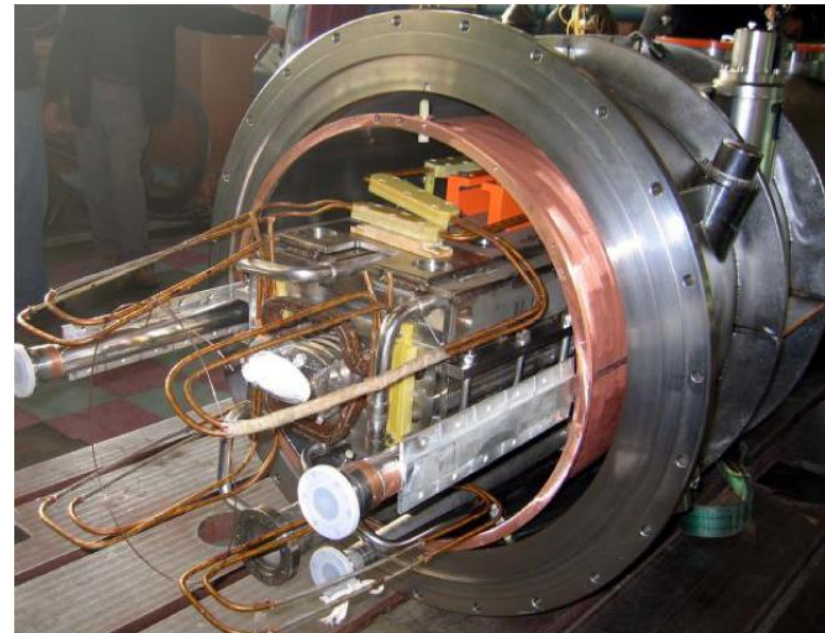
# SIS100 Dipole Magnets: Development

Second full size prototype for SIS100 dipole – C2LD

produced by BINP (Nowosibirsk)

tested @ Dez.2009 – Nov 2011 (11 test runs)

Design		Window-frame, curved laminated cold iron yoke, lamination thickness 1mm, two layer coil with 16 turns, <b>steel ET3414 (anisotr.)</b>
Effective magnetic length L	m	3.062
Useable aperture	mm	113 * 58
Bending angle	deg	3 1/3
Bending radius	m	52.632
Bmin	T	0.253
Bmax	T	1.9
Current at max. field	A	6500
Ramp rate	T/s	4



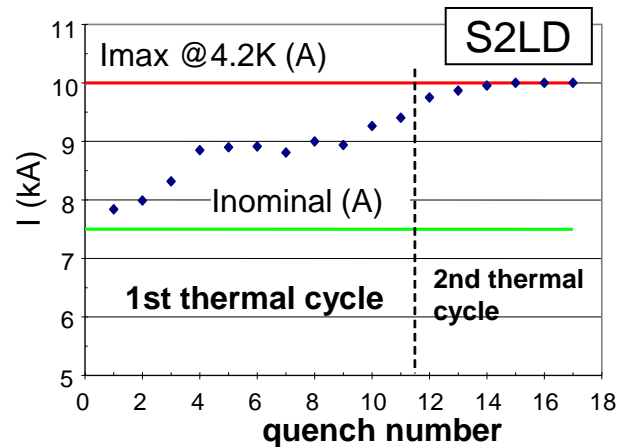
curved magnet:

- reduces the magnet aperture width

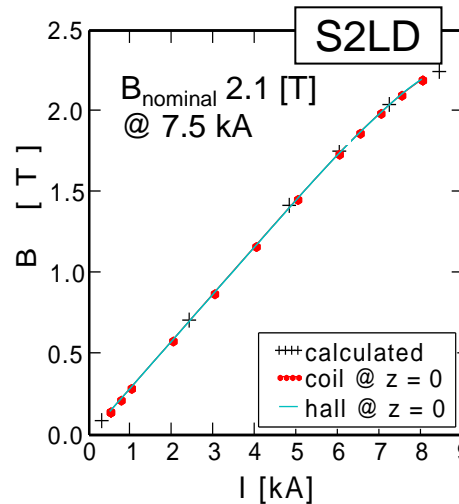


# Test Results for Full Size Dipole Models

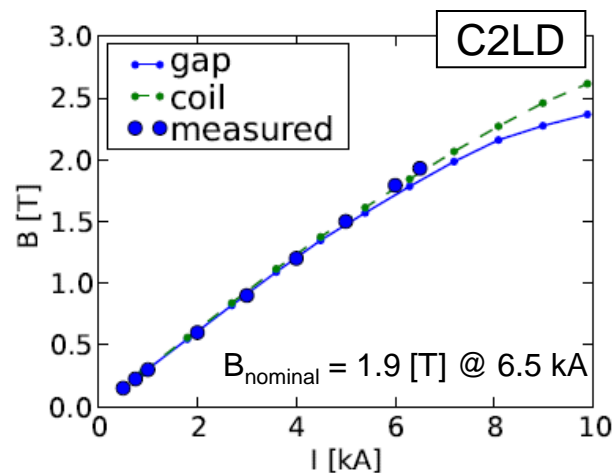
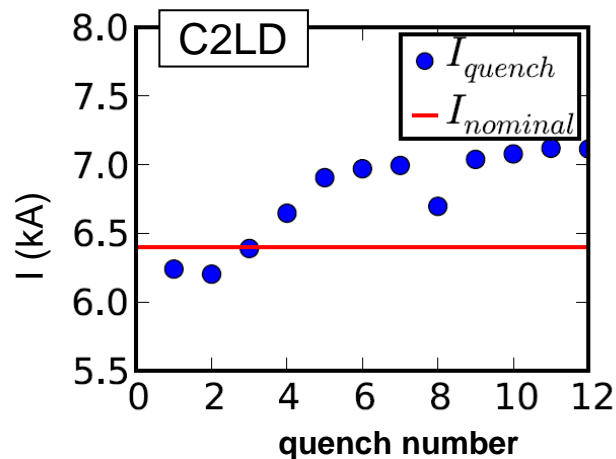
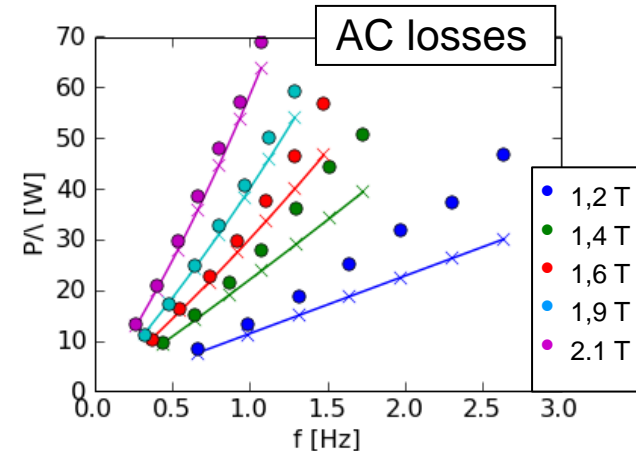
## Magnet training



## Load line

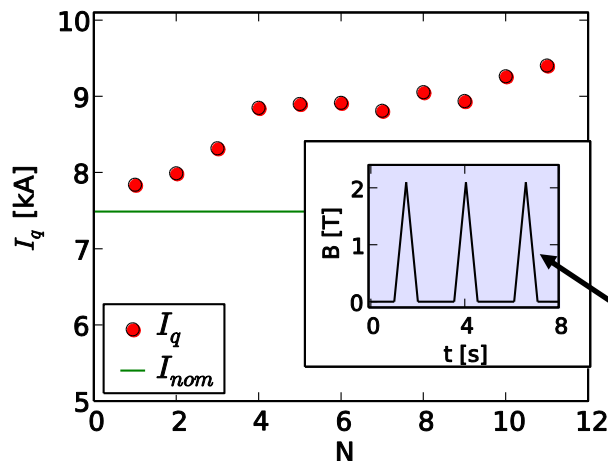
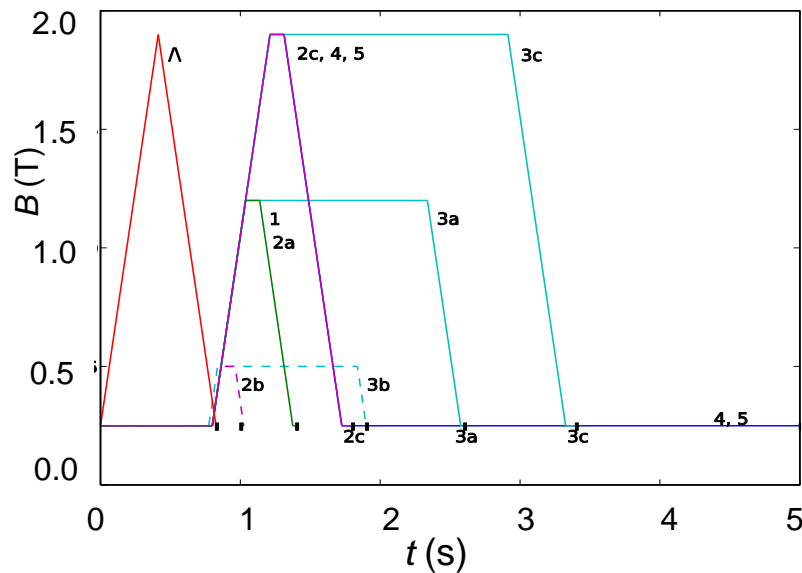


AC loss as measured for the C2LD (circle) versus the loss obtained for the S2LD magnet (x)

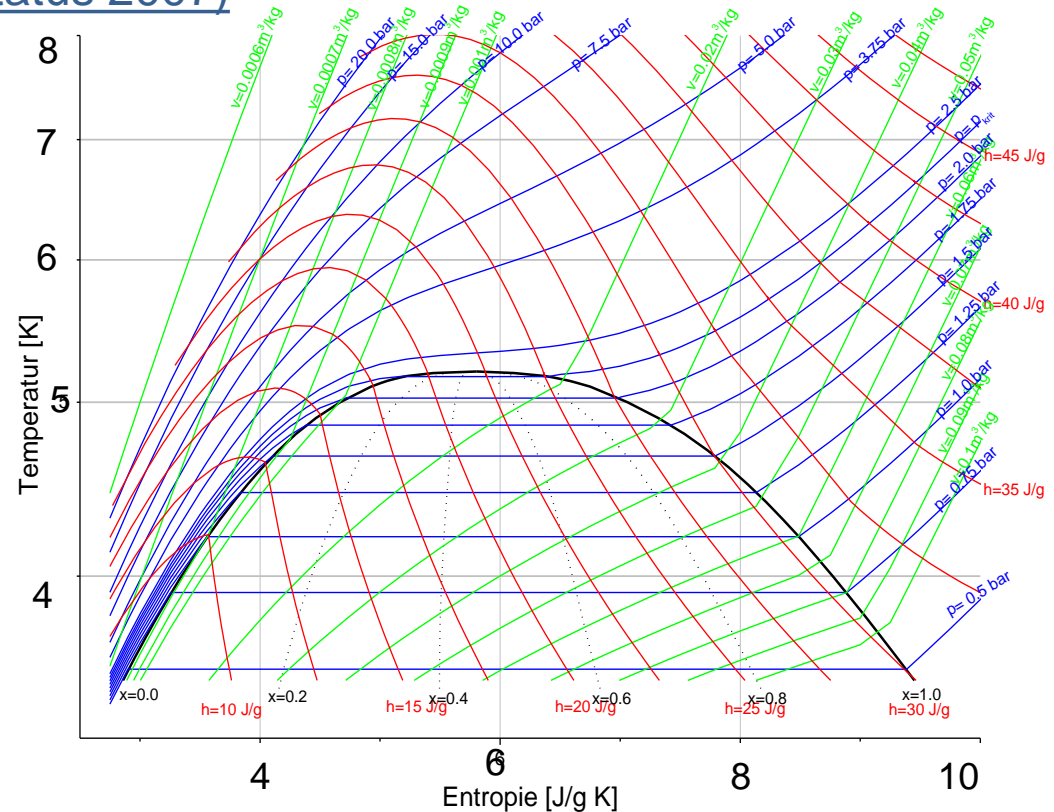


# Test Results for Full Size Dipole Models

## Main operation cycles for SIS100 (status 2007)

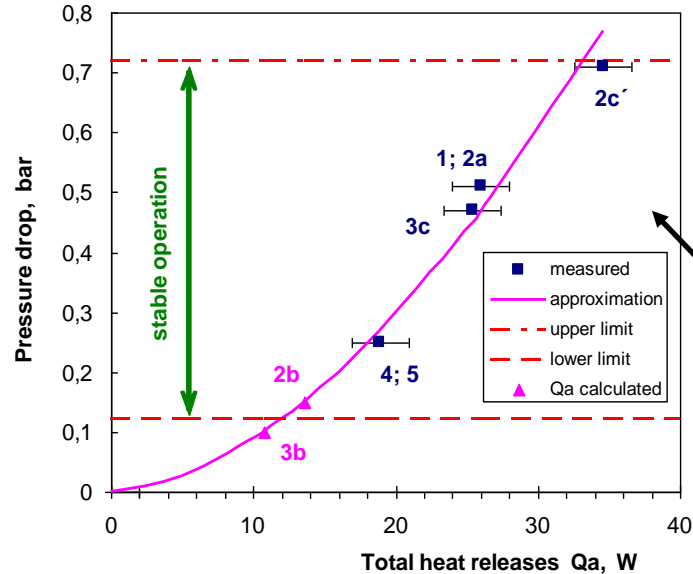
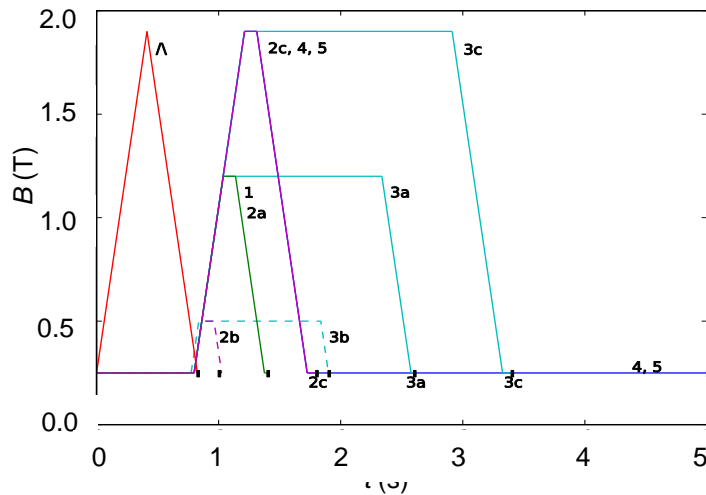


the strongest cycle mode of the magnet continuously tested at S2LD during one week and up to now for  $2 \cdot 10^6$  cycles.

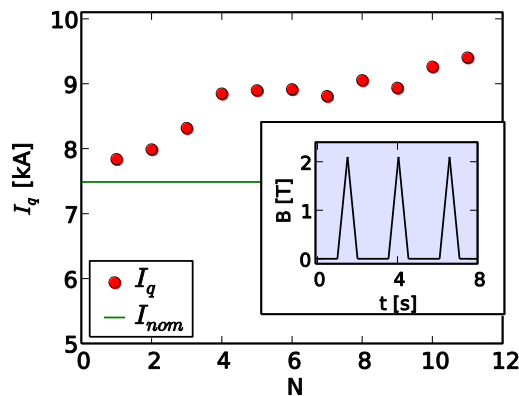


T – S phase diagrams for  $^4\text{He}$

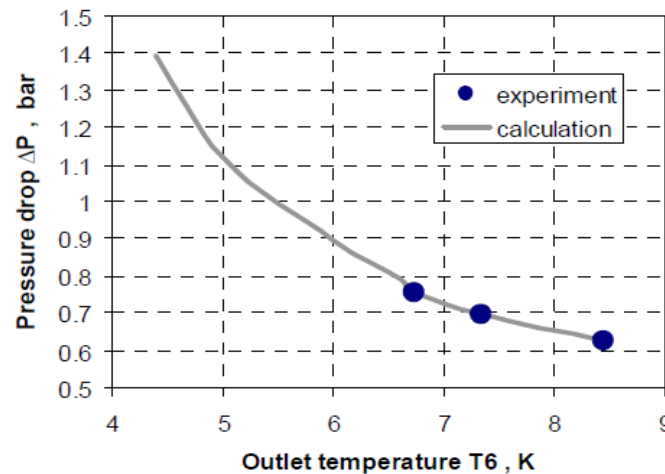
# Test Results for Full Size Dipole Models



Straight dipole: Cryogenic stability range evaluation from an analytical model dipole for double layer coil



strongest cycle mode achieved for S2LD



Dependence of the cooling circuit pressure drop from the yoke outlet temperature calculated for equivalent dipole model for a stable triangular cycle

& measured for S2LD, C2LD



# Conclusions for the Final Dipole Design

- The test results achieved at S2LD and C2LD confirm R&D results and calculations for AC loss and magnetic field quality
- Both the calculation (analytical) and measurements of the hydraulic resistance showed that with the 2 layer coil design the new SIS100 cycles are not feasible
- The hydraulic resistance of the double layer coil limits the cycling rate of SIS100!
- The comprehensive test of these models gave important information required to optimize the final design and to specify the pre-series magnets.
- The redesign of an optimized curved dipole with a single layer coil can fulfill the updated operation requirements of the FAIR SIS100 accelerator.

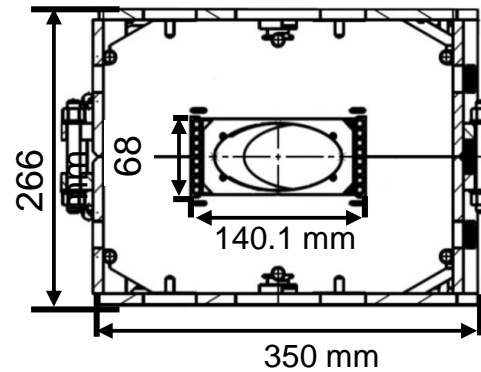
## Redesign of the coil to satisfy the operation parameters:

- ✓ new cable design (with lower hydraulic resistance)
- ✓ shorter coil length - 4 turns per pole instead of 8
  - 13.1 kA higher nominal current instead of 7.5 kA
- ✓ CSLD (curved single layer dipole)

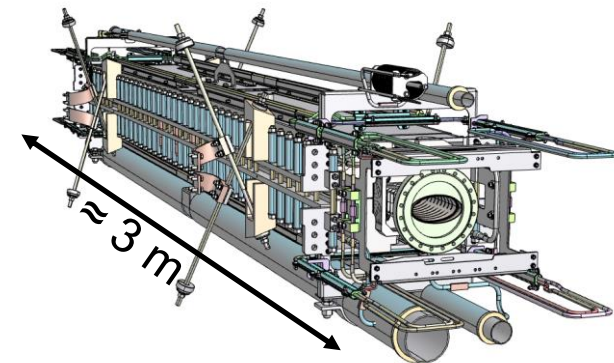
# First of Series (FoS) Dipole for SIS100

## Final design

- super ferric
- window frame
- sc coil - 4 turns per pole
- low AC loss Nuclotron-type cable (CuMn inter-filament matrix)
- cooling with 2-phase He



magnet cross section

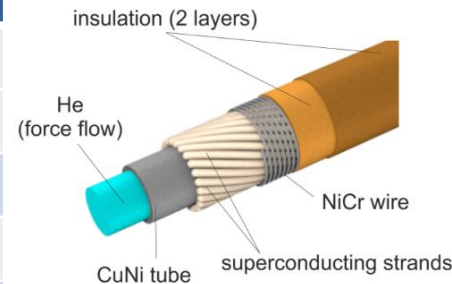


cold mass  
with beam chamber

## Main design parameter

Number of magnets in SIS100		108 + 1
Effective length $L_{\text{eff}}$	m	3.062
Usable aperture	mm x mm	60 x 120
Bending angle	deg.	1 1/3
Bending radius	m	52.632
Nominal Field	T	1.9
Field homogeneity $\Delta B/B_{\text{main}} \times 10^4$	units	$< \pm 6$
Ramp rate	T/s	4 @ 1Hz

## Nuclotron cable:

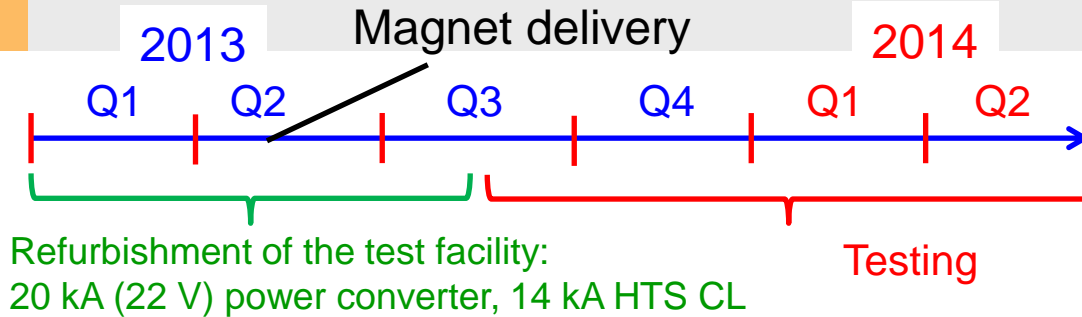


- 1 – CuNi Cooling tube
- 2 – NbTi SC wire
- 3 - CrNi wire
- 4 - Kapton tape
- 5 - Glasfiber tape



cryo-dipole module

# First of Series (FoS) Dipole for SIS100



## Testing program:

- Alignment
- Pressure drop and flow rate tests for all He-lines  
→ hydraulic adjustment
- Leak- and vacuum tests for a vacuum vessel
- Electrical tests for HV and LV circuits  
(HV-, capacitor discharge, continuity tests)
- Magnet training
- Field measurement
  - new curve - to obtain better accuracy for the field simulations
  - load line and field homogeneity (DC& AC-operation - for beam dynamic requirements)
  - end profile optimization – to improve the integral field quality ( $b_3$ )
- AC-losses – to estimate dissipated heat load  
→ required cooling power for the SIS100

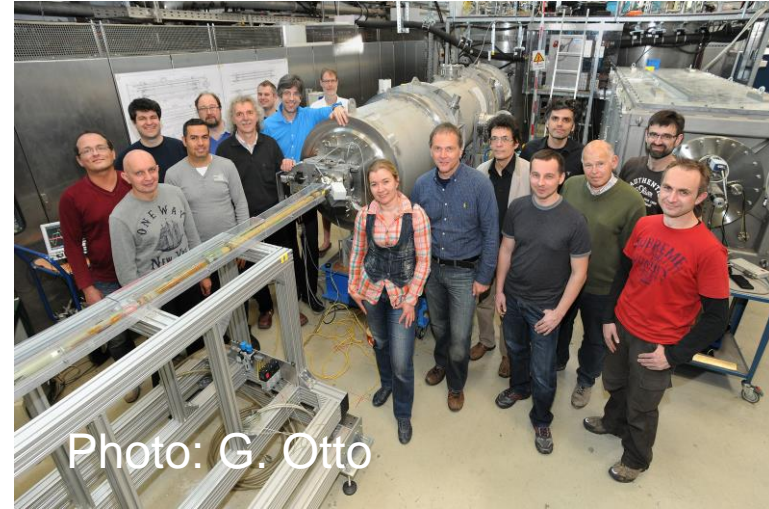


Photo: G. Otto

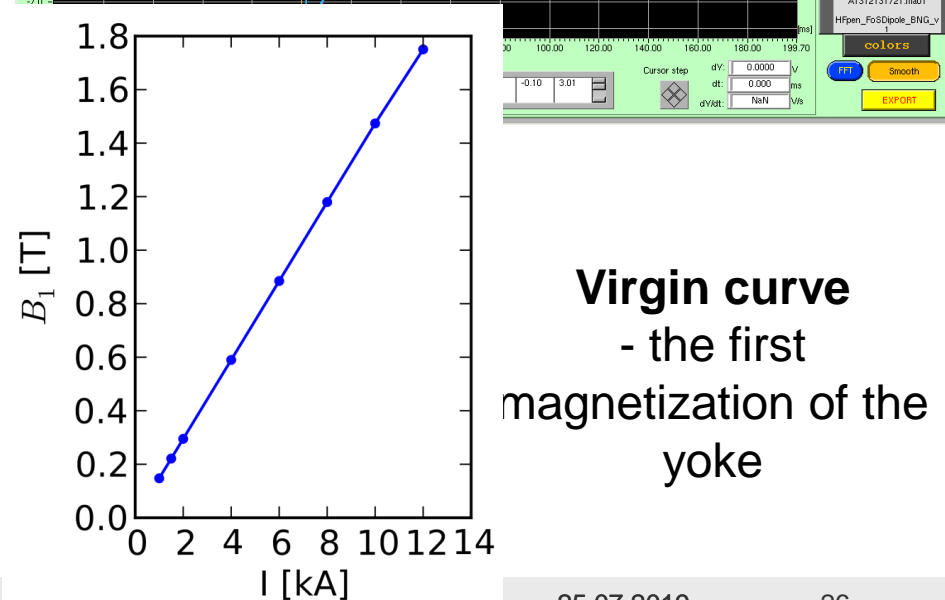
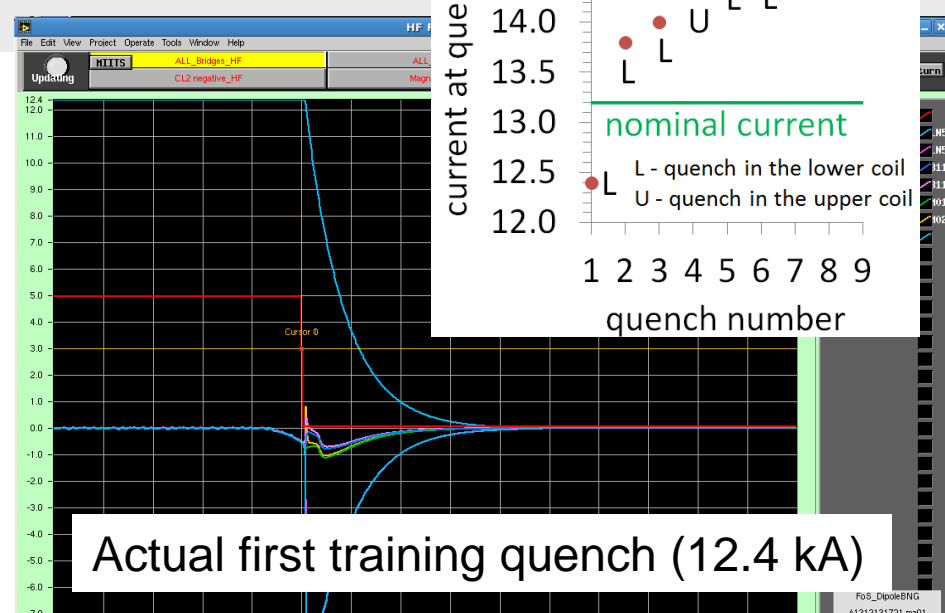




# Testing of the SIS100 FoS Dipole

Lucky Friday the 13<sup>th</sup> (Dec. 2013)

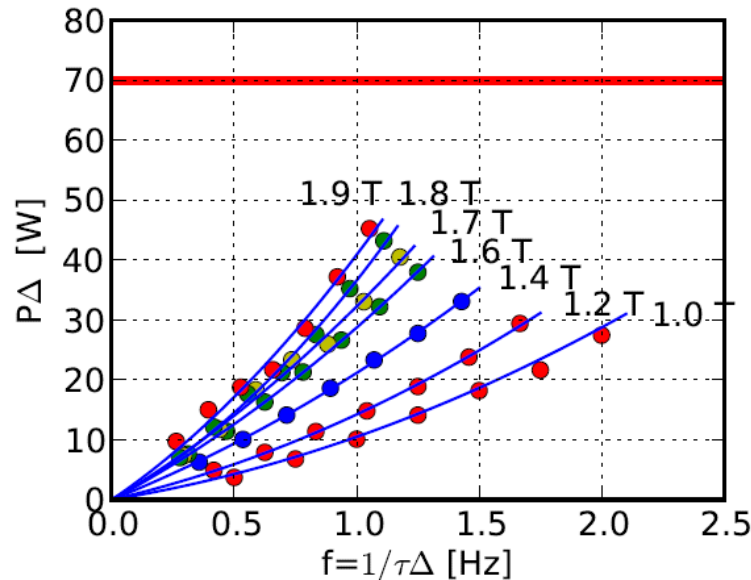
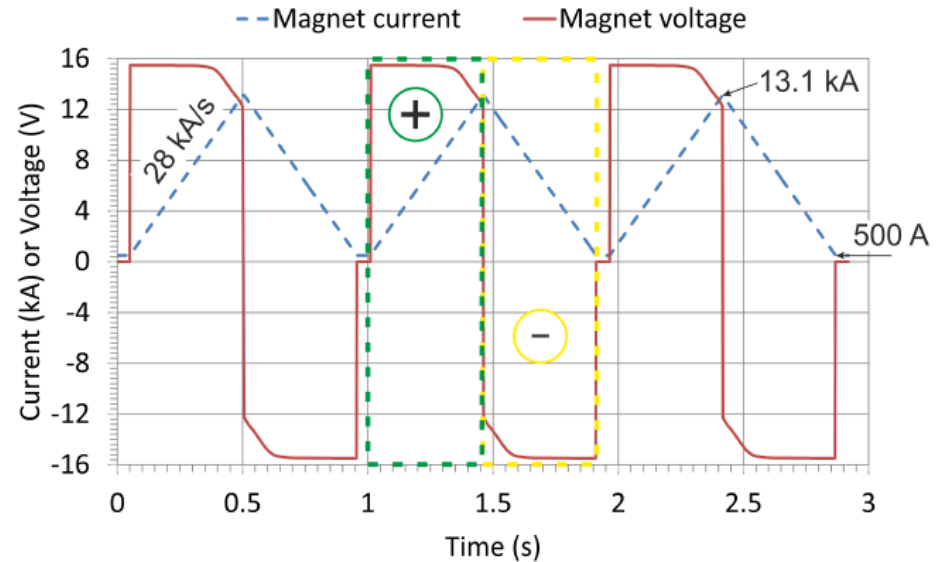
- the first powering at cold
- virgin curve measured
- 2<sup>nd</sup> quench above nominal current
- magnet trained up to 15 kA (CL limit)



# FoS Dipoles: AC Loss Measurement

## V-I Method:

- we measure the energy absorbed by the magnet and returned to the power converter over a single powering cycle
- the tiny difference in the energy is associated with AC losses
- the measurement requires a high precision DVM for the voltage acquisition which also gives the trigger for the synchronized current acquisition



$$E = \underbrace{\int V(t) \cdot I(t) \cdot dt}_{\text{cycle}}$$

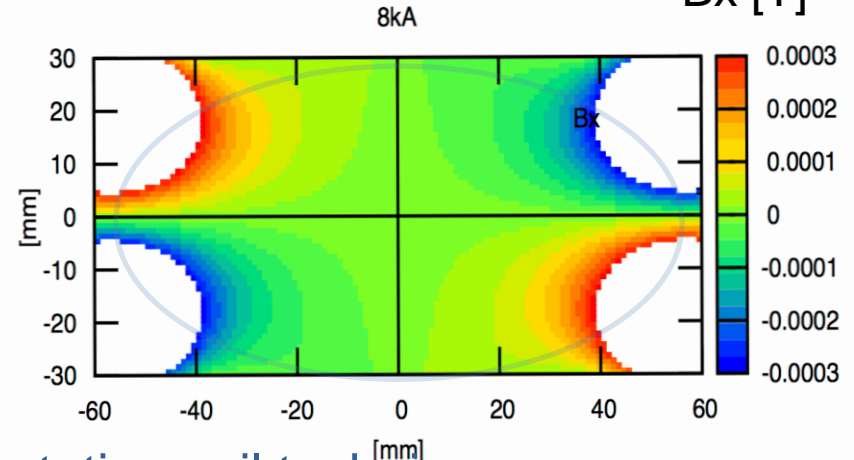
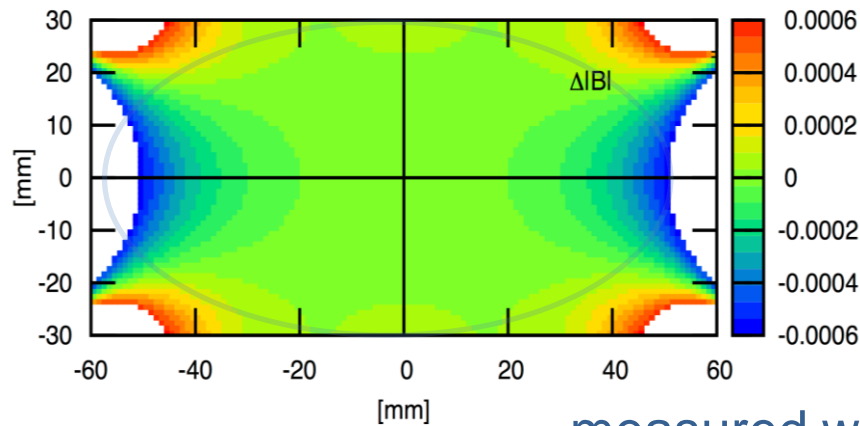
The AC loss for various operation cycles (various cycling rates). The maximum field is given at the end of the line.

# FoS Dipole: Magnetic Field Issues

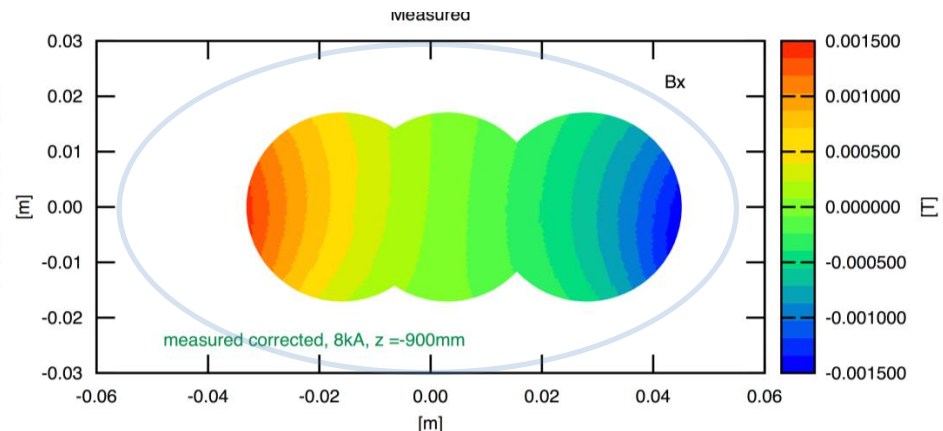
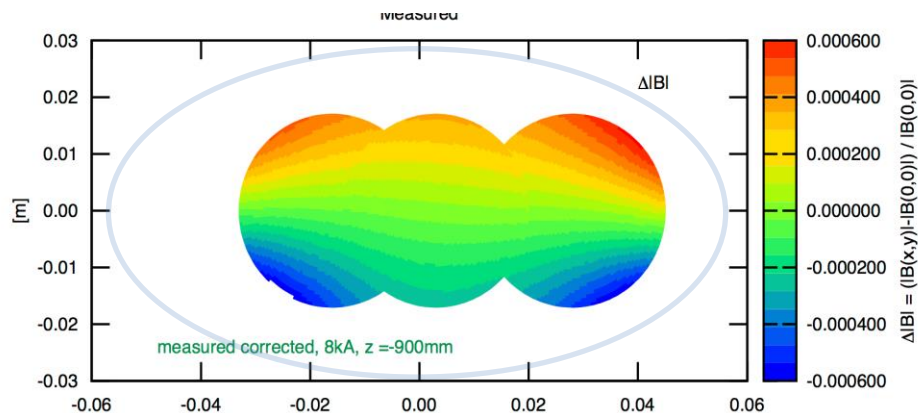
$\Delta|B|$  w.r.t  $|B(0,0)|$  [units]  
8kA

expected field distribution

$B_x$  [T]



measured with rotating coil technic



$\Delta|B|$  colored  $\pm 6$ unit = 0.0006 w.r.t  $|B(0,0)|$

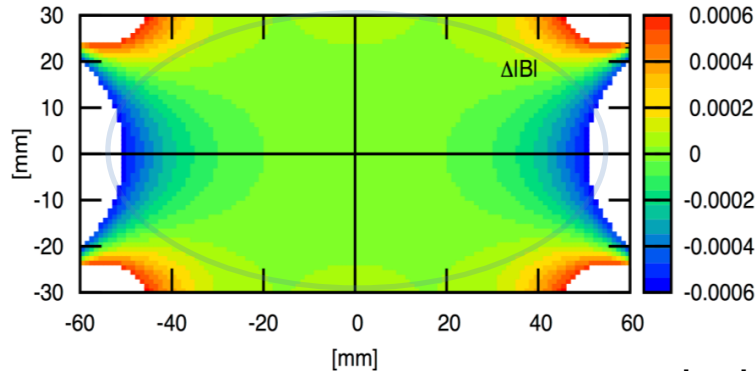
$B_x$  colored  $\pm 0.0003$  T (top),  $\pm 0.0015$  T (bottom)

courtesy K.Sugita

# FoS Dipole: Magnetic Field Issues

$\Delta|B|$  w.r.t  $|B(0,0)|$  [units]

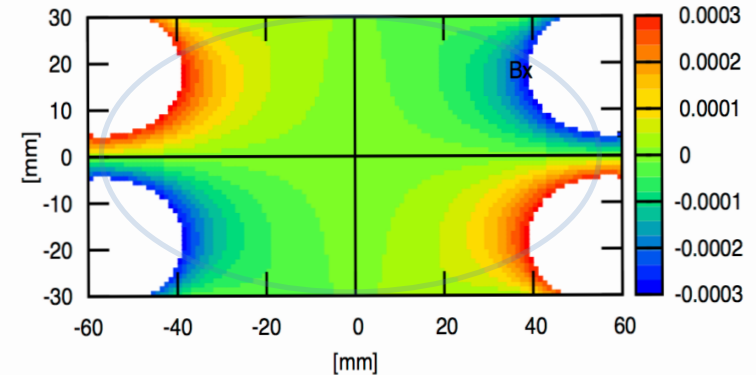
8kA



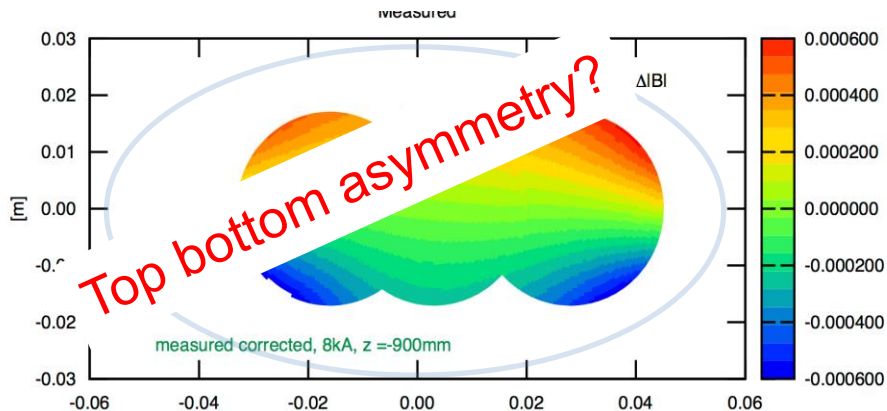
expected field distribution

8kA

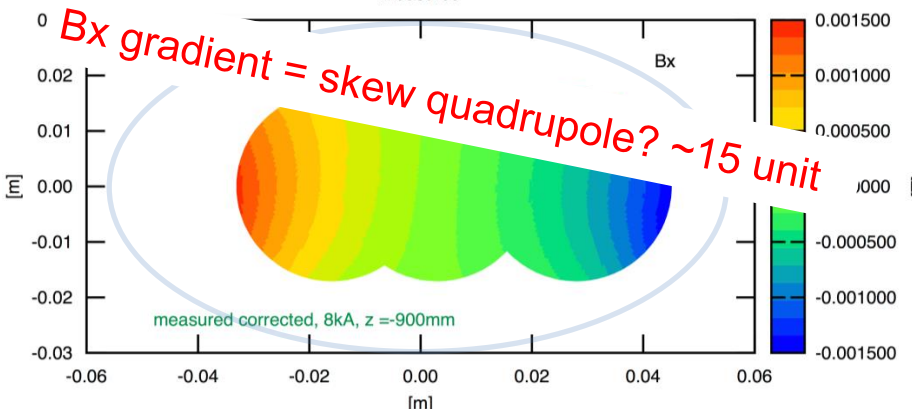
$B_x$  [T]



measured with rotating coil technic



$\Delta|B| = (|B(x,y)| - |B(0,0)|) / |B(0,0)|$



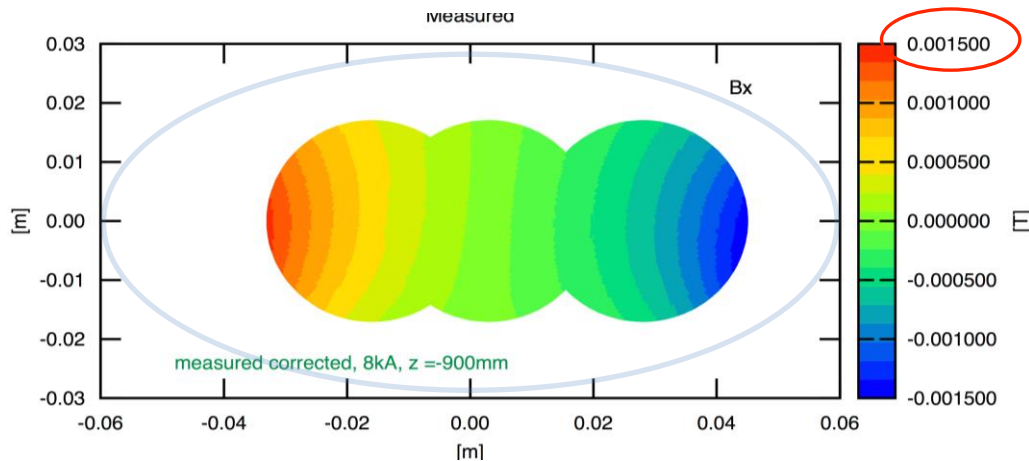
What could be the reason? Measurement error?

Not really easy to produce such an error but let us crosscheck with another technique



# FoS Dipole: Magnetic Field Issues

measured with rotating coil technic



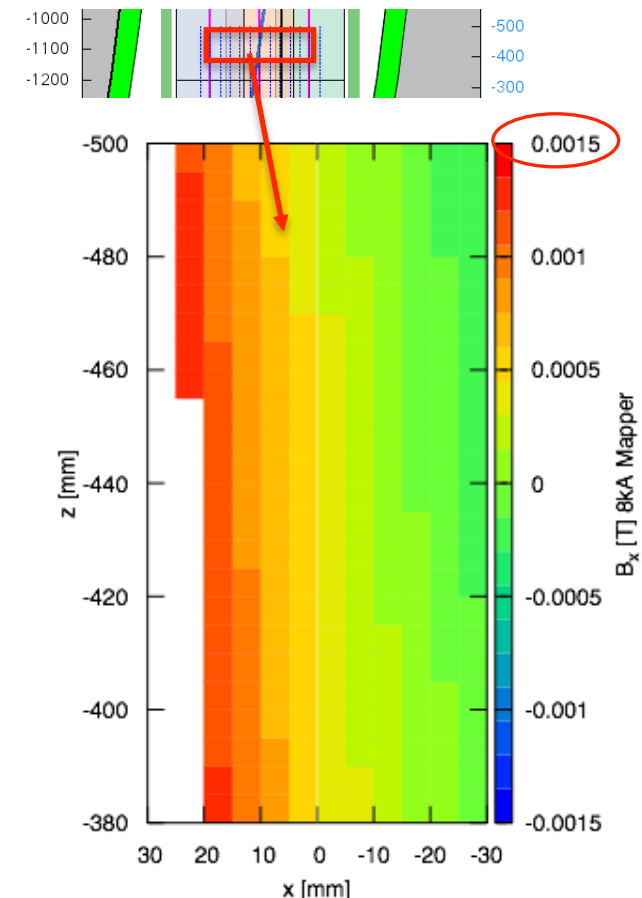
Bx gradient = skew quadrupole ~15 units proved by Hall probe measurement

How can we explain unexpected field error?

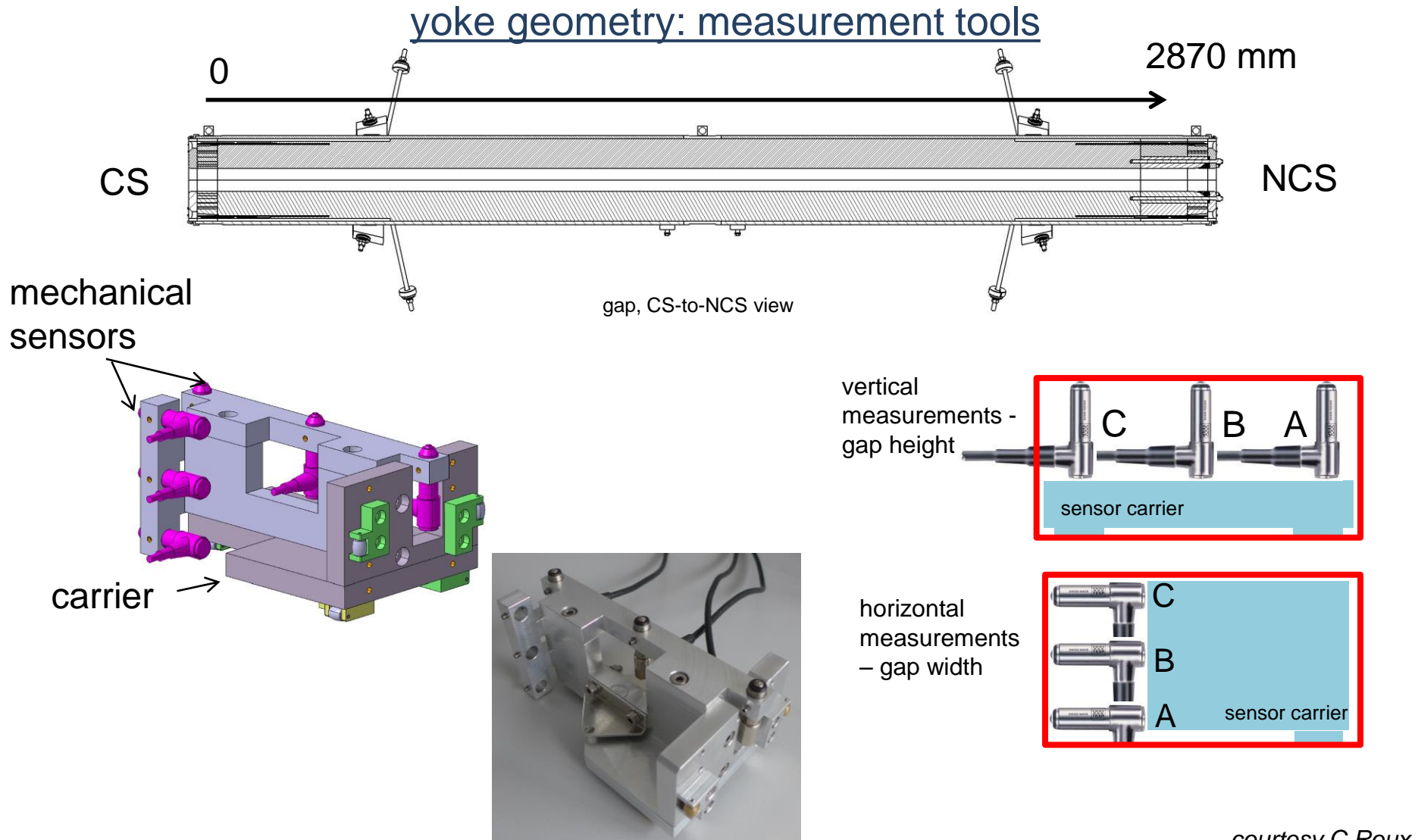
Is it a manufacturing error? Which one?

The contractor built the magnet according to the drawings.  
To demonstrate, that the observed field distortion is caused by the production, one needs to precisely measure the geometrical parameters (gap height, width)

Hall probe measurement Bx in the 2D field region



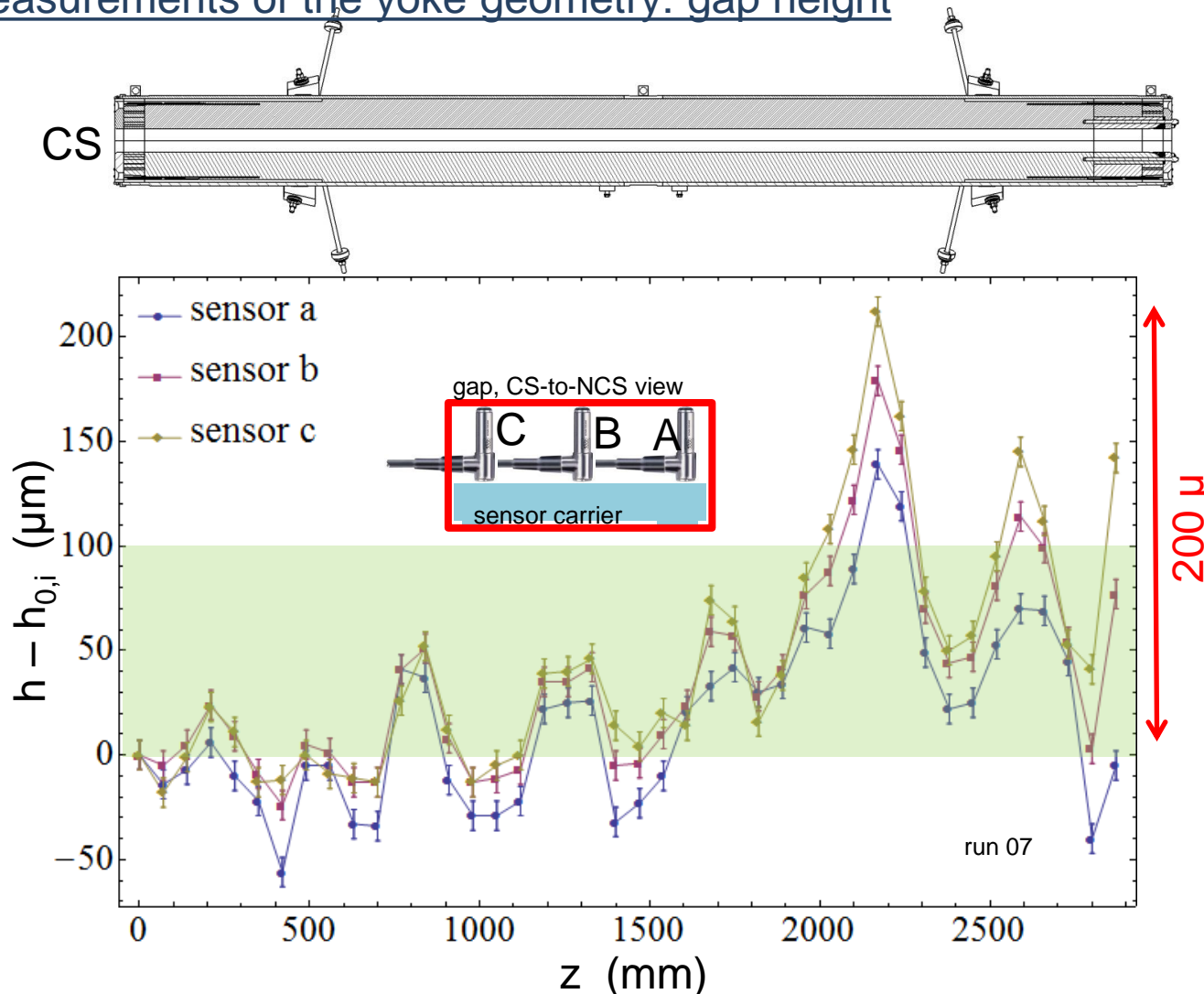
# FoS Dipole: Magnetic Field Issues



courtesy C.Roux

# FoS Dipole: Magnetic Field Issues

## Measurements of the yoke geometry: gap height

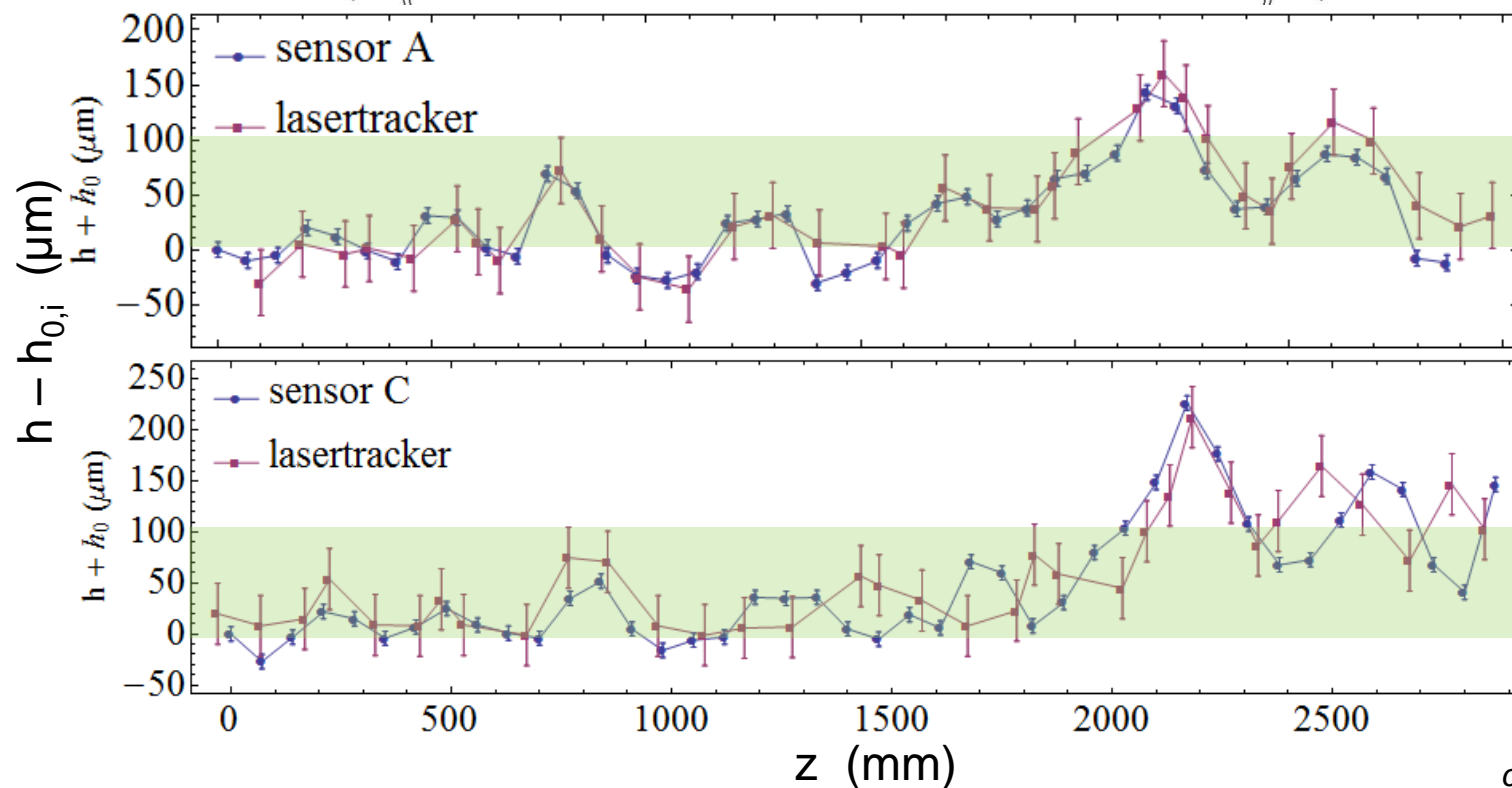
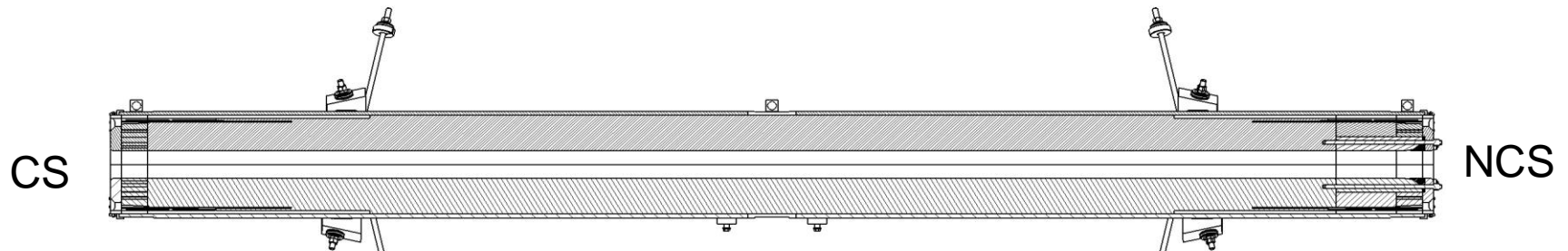


Spec.  
2.2.11:  
gap  
tolerance  
(+100/- 0) $\mu$

specified  
tolerance

courtesy C.Roux

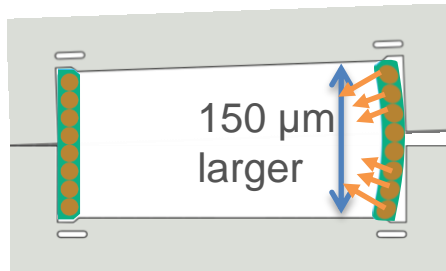
## yoke geometry: comparison of measurement techniques



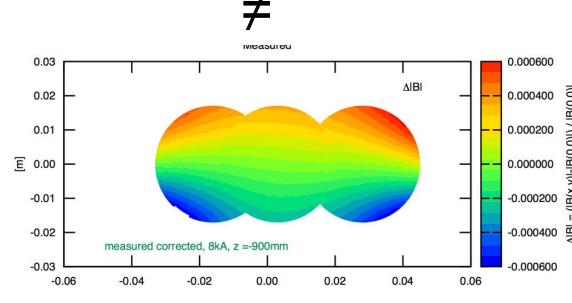
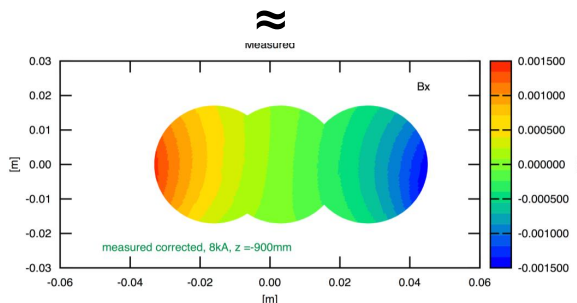
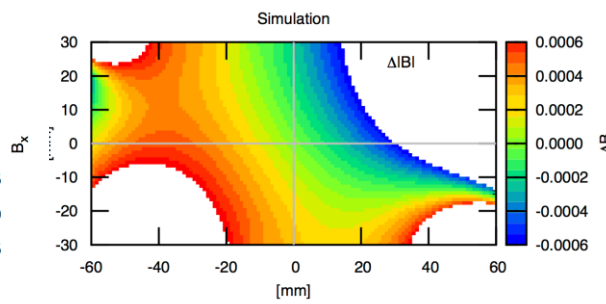
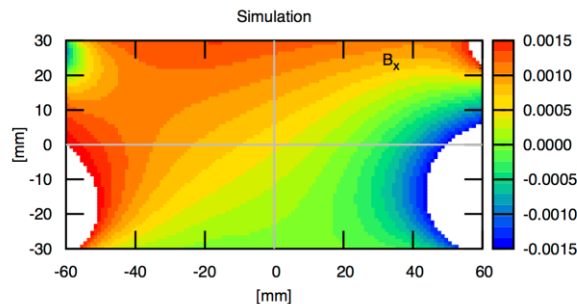
courtesy C.Roux

# FoS Dipole: Magnetic Field Issues

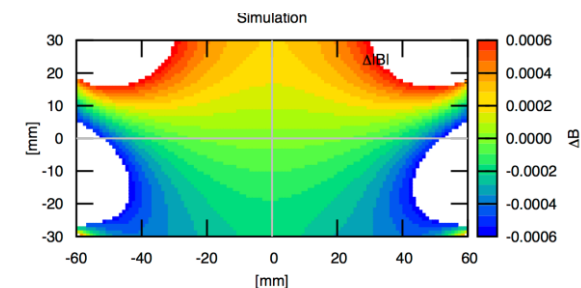
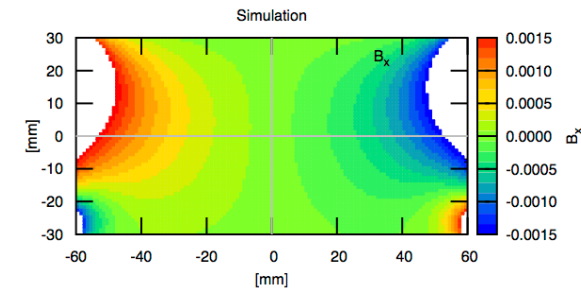
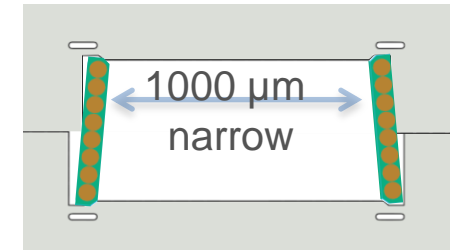
FEM studies - model based on the geometrical measurements



This can explain  $B_x$ ,  
but not  $|B|$  top-bottom asymmetry



cf.



Such huge deviation was not observed  
→ Combination of manufacturing errors

courtesy K.Sugita

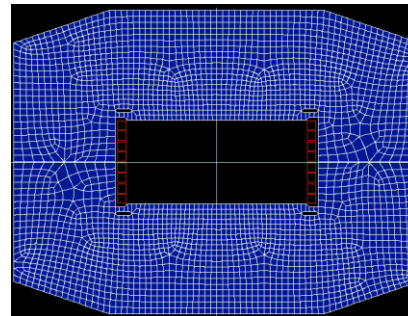
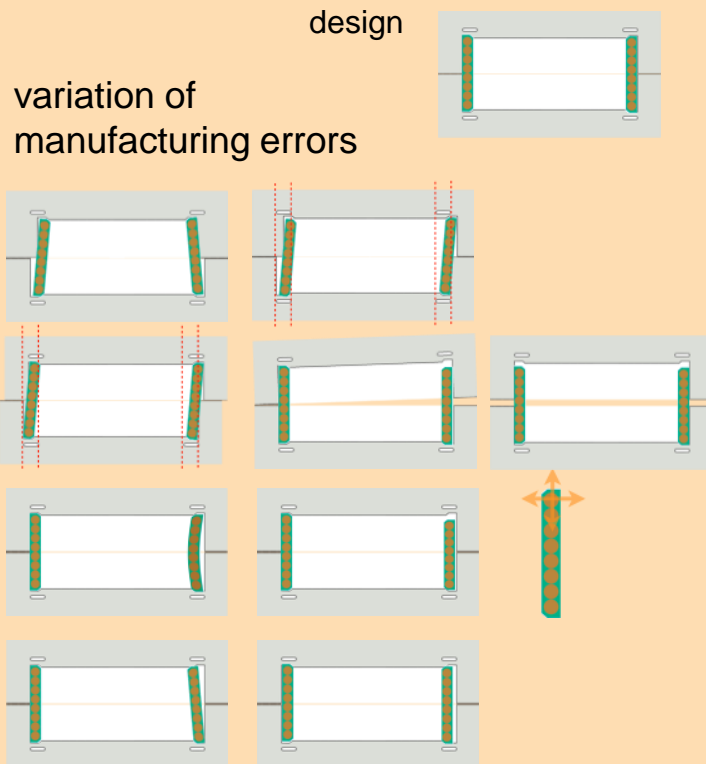
## field-error simulations: starting point

*courtesy K.Sugita*

Input:

analysis of production drawing/procedure

analysis of magnetic field measurement results



Simulations  
Roxie2D

We have simulated a number of possible magnet assembly errors. However we couldn't reproduce the observed field distortion completely.



# SIS100 Dipole Magnets: Production

Q/2 2014 – Q1/ 2015 - survey on alternative manufacturing technics  
analysis of possible manufacturing errors

Q2- Q3/2015 – manufacturing of the new yoke and magnet reassembly

## lamination stamped to final geometry

- no further machining

## laser welding

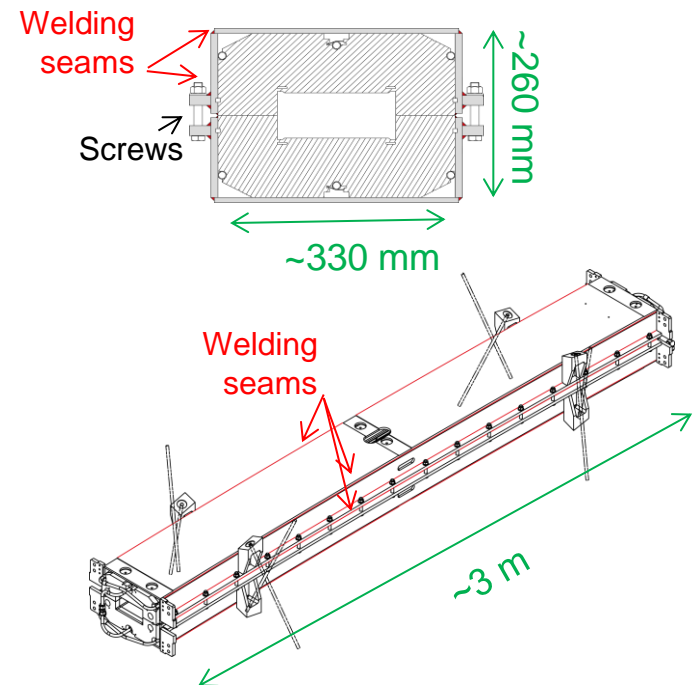
- low heat input
- low tension
- automated



## removal of gap between yoke halves

- coil clamped in elastic range

**+ > 130 further changes in fabrication  
and quality issues for series dipoles**



*courtesy C.Roux*

October/2015 – reassembled magnet delivered to GSI for testing



# SIS100 Dipole Magnets: Production

FoS 2 – FoS dipole assembled with a new yoke and reused coil

Testing at GSI - October/2015 – Q1/2016

lamination stamped to final geometry

- no further machining

laser welding

- low heat input
- low tension
- automated

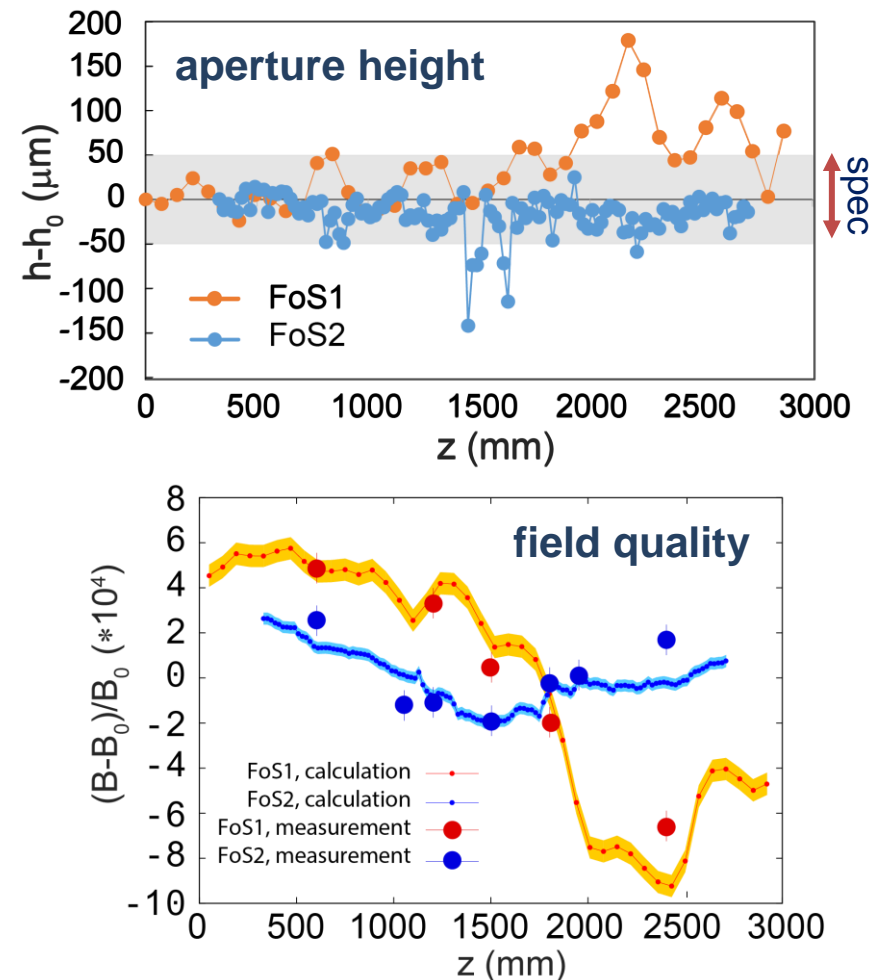


removal of gap between yoke halves

- coil clamped in elastic range

successful

08/2016 Release of series production



## At the contractor site:

- Quality inspections at different production steps

(e.g. yoke geometry for half yokes before and after welding, after assembly with the coil)

- Functionality tests @ 300K
  - ✓ components of assembly
  - ✓ assembled magnet
- Factory Acceptance Test (FAT)
  - ✓ measurement protocols
  - ✓ quality certificate (summary of single tests)

## At the GSI site:

- Standard Test Program for 100% of magnets:
  - ✓ documents control
  - ✓ quality controls
  - ✓ functionality tests @ 300K (after delivery, after cold tests)
  - ✓ functionality tests @ 4.5K  
including magnetic field measurements (DC, AC mode)
- Advanced Test Program for 10% of magnets
  - ✓ magnetic field measurements in the enlarged area

# Site Acceptance Test (SAT): Scope



## quality assurance (including safety)

- yoke geometry
  - ✓ aperture height (precise)
  - ✓ sag and twist
  - ✓ positioning
- process lines
  - ✓ pressure and leak,
  - ✓ massflow rate
  - ✓ positioning
- instrumentation check
- electrical integrity
  - ✓ HV
  - ✓ continuity
  - ✓ turn-to-turn isolation
- quench performance
- static heat load and AC losses

## machine control

- integral B-field
- harmonics
- load line

about 30 parameters

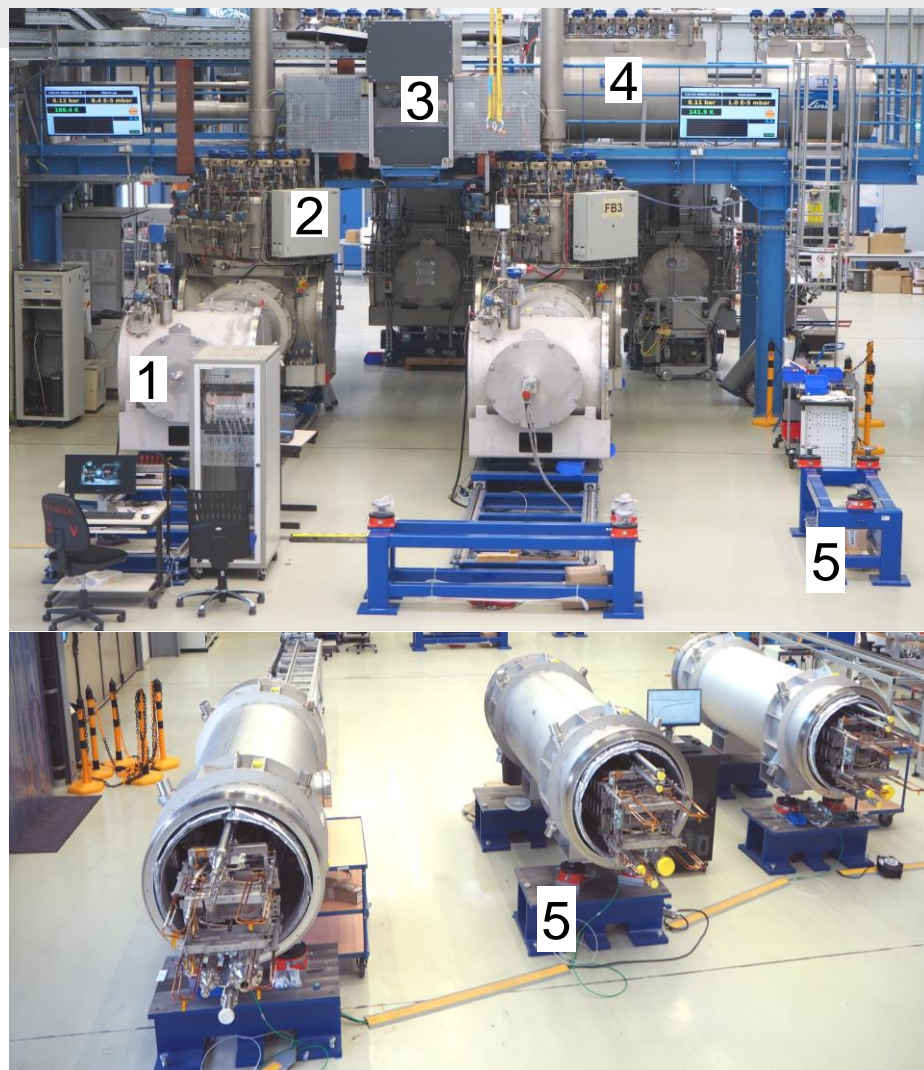
about 110 steps

Duration ~ 3 weeks per magnet

# GSI Test Facilities for SIS100 Magnets

## Series Test Facility (STF)

- ✓ Refurbishment of the SH2-SH3, installation of the test benches – 2013 - 2015
- ✓ Cryo-plant 1.5 kW – commissioned Q2/2015
- ✓ power converters 2 x 20 kA (66 V) – commissioned Q1 & Q3/2016
- ✓ 14 kA DC HTS Current Leads (CL) – commissioning Q3/2015 – Q1/2017
- ✓ QD / Magnet protection system
- ✓ 687m<sup>2</sup> total area
- ✓ 4 test benches for cold tests
- ✓ 6 preparation benches
- ✓ calibration chain for MF-probe



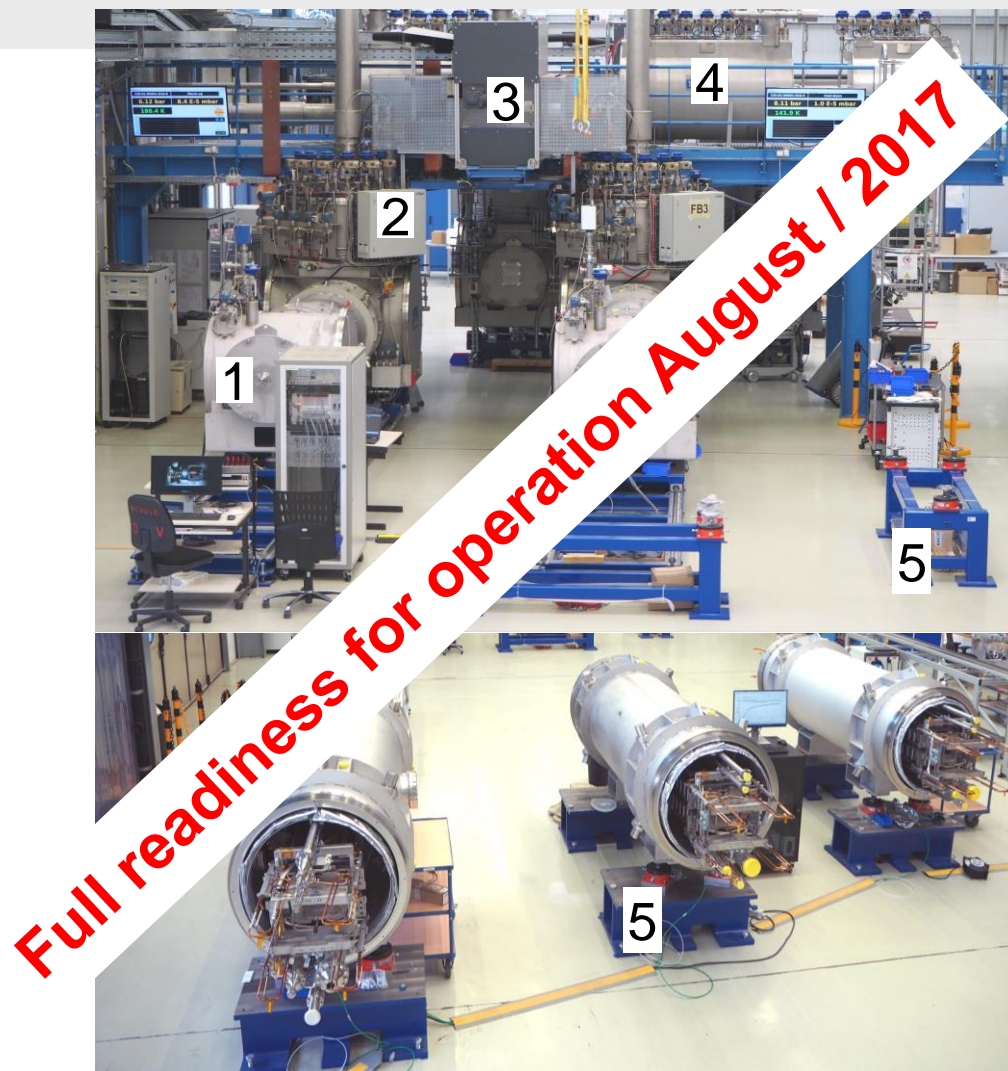
Test benches for superconducting magnets: 1-end box, 2 - feed box, 3 - distribution box, 4 - power switch, 5 - preparation bench



# GSI Test Facilities for SIS100 Magnets

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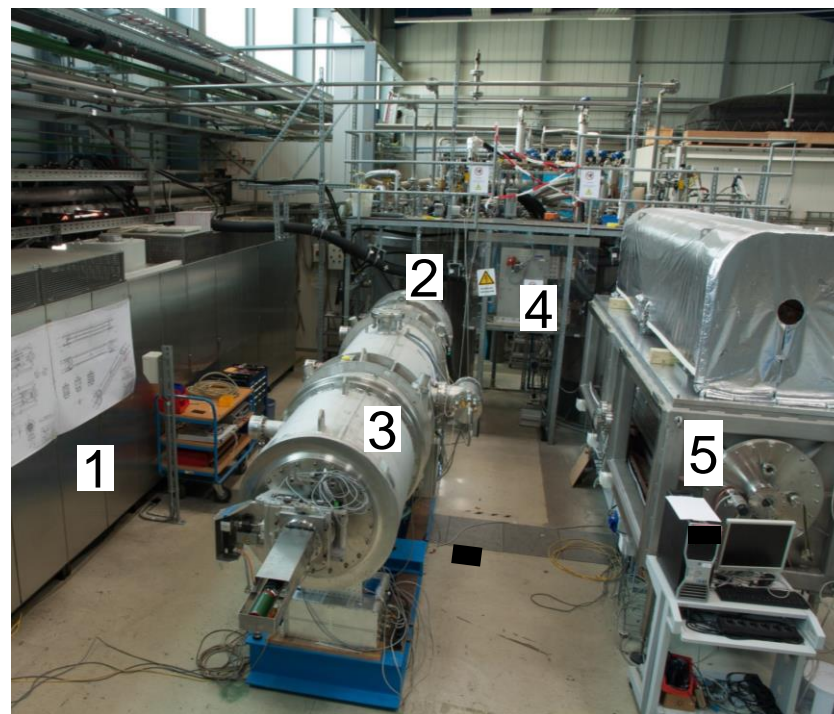


Test benches for superconducting magnets: 1-end box, 2 - feed box,  
3 - distribution box, 4 - power switch, 5 - preparation bench



## Prototype Test Facility

- ✓ Cryo-plant 0,6 kW – commissioned 2007
- ✓ power converters 20 kA (66 V) – commissioned Q3/2013
- ✓ 14 kA DC HTS Current Leads (CL) – commissioning Q3/2013, Q4/2014
- ✓ QD / Magnet protection system
- ✓ 150 m<sup>2</sup> total area
- ✓ 1 test benches for cold tests SIS100 dipole
- ✓ 1 universal cryostat



1 - power converter, 2 - feed box for testing of SIS100 magnets, 3 - First of series dipole for SIS100, 4 – power switch, 5 Universal cryostat for cryogenic tests of small components.

## Series Test Facility

- ✓ SIS100 series dipole -100%
- ✓ SIS100 string test
- ✓ 14kA HTS CL for SIS100 (11 pairs)
- ✓ Cryo Components for SIS100 (Bypass Line, FoS Current Lead and Feed Box)
- ✓ UHV components (FoS vacuum chamber for SIS100 dipole, FoS cryosorption pumps)

## Prototype Test Facility

- ✓ Local current leads (250A HTS) for SIS100 corrector magnets
- ✓ small cryo components (cryo-catcher)  
14kA HTS CL for SIS100 (11 pairs)

# Magnetic Field Measurements: Used Methods

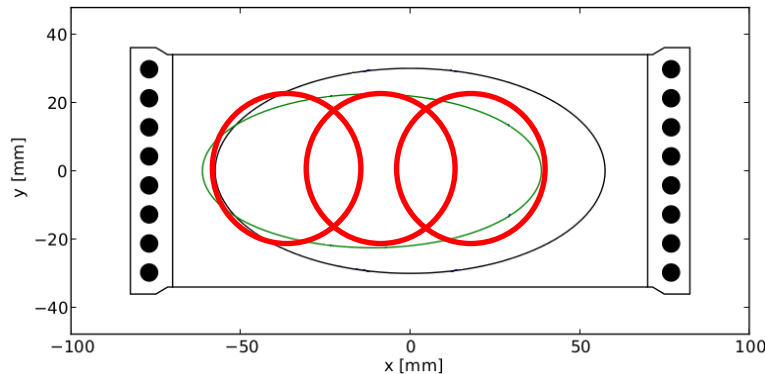
## Combining rotating coil probe measurements:

### Warm rotating coil probe – the „Mole“

- rotating coil probe with dipole compensation

$$R_{ref} = 17\text{mm}, L = 600\text{mm},$$

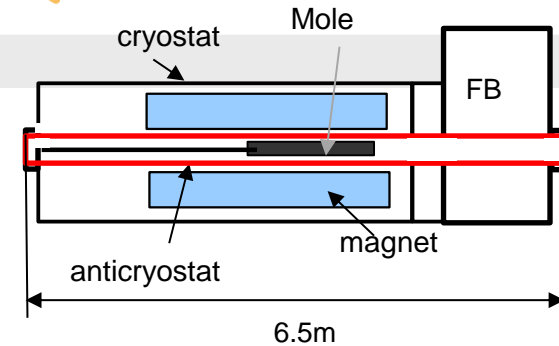
- operate in anticryostat  $R_{out} = 32\text{mm}$ ,  $R_{in} = 23.45\text{mm}$ ,  $L = 6.5\text{m}$
- measurements at 3 lateral positions
- measurements for 5 longitudinal positions



solid black: usable beam aperture

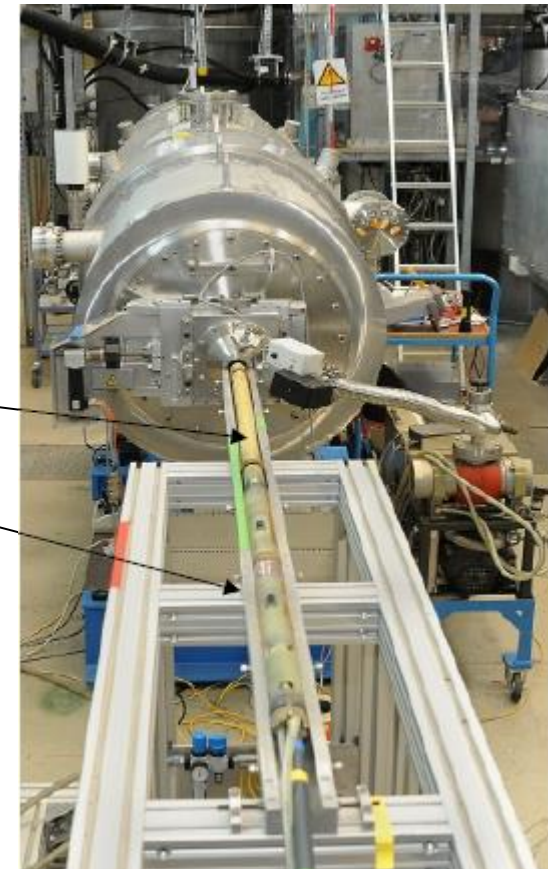
red area covered by Mole for a single lateral position

green area covered by measurements with the Mole in the anticryostat



coil probe

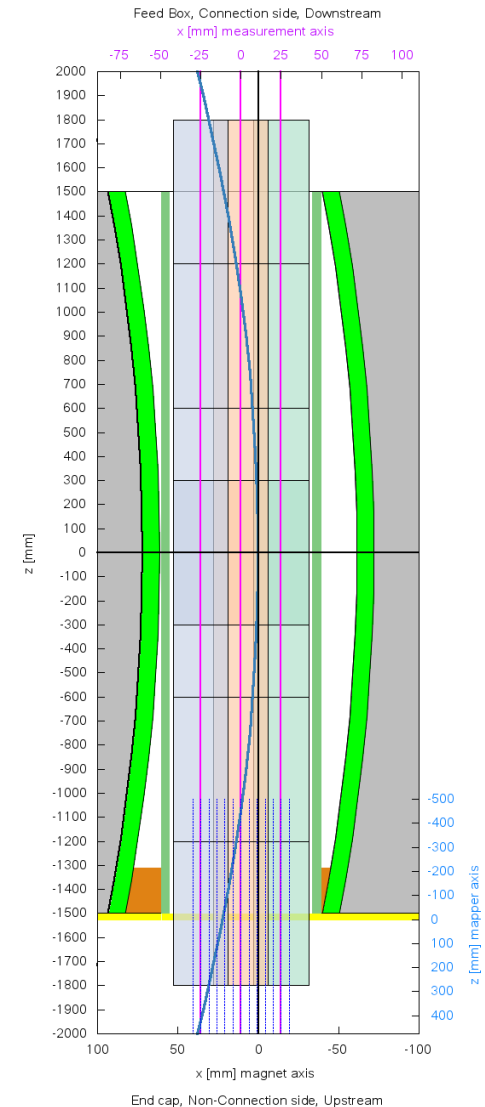
motor unit



## Challenges of the Mole system:

- Precise positioning of the anticryostat in the magnet with respect to XY plain
- Precise positioning of the coil probe respect to the beam axis
- The field can not be measured directly on the beam axis with the existing probe. Recalculation of the field on the beam axis is difficult since the real position of the probe with respect to the x-axis is not known -> not systematic error -> not clear error propagation for reconstructed field
- only small area inside the magnet gap can be covered
- complicated installation and alignment procedure for anticryostat

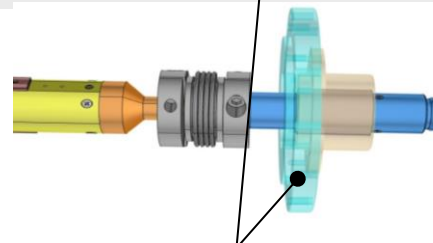
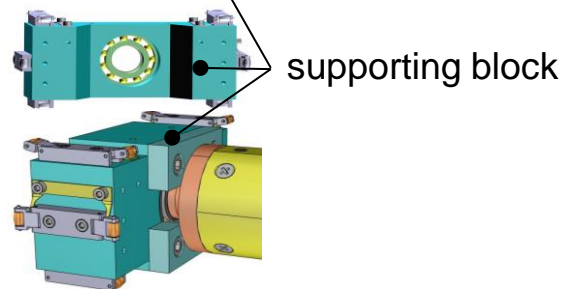
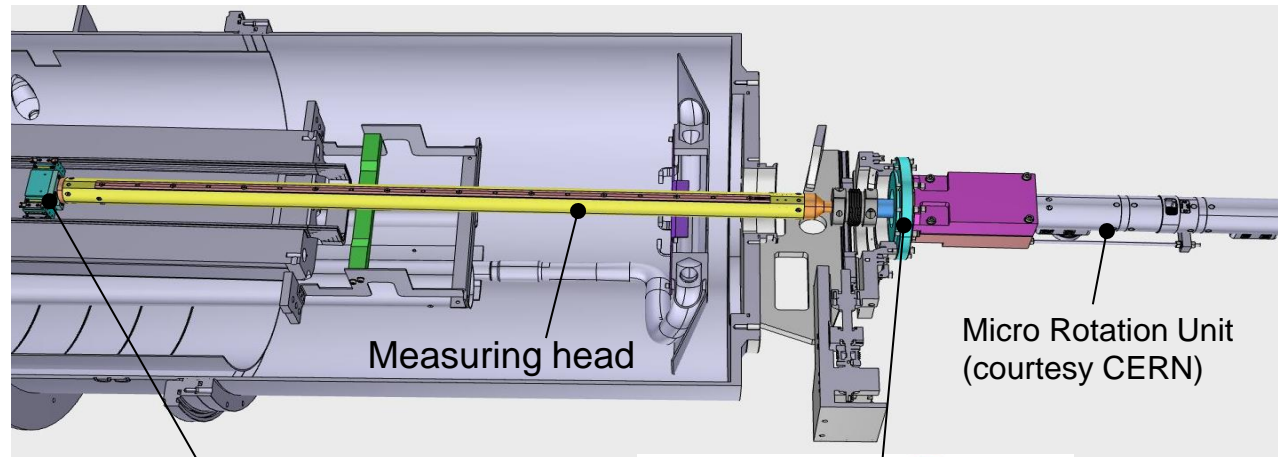
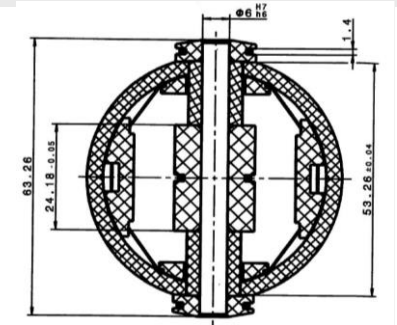
Therefore a new system with appropriate measurement precision, larger coverage (xy plane) and simpler handling is needed for qualifying the series dipole magnets!



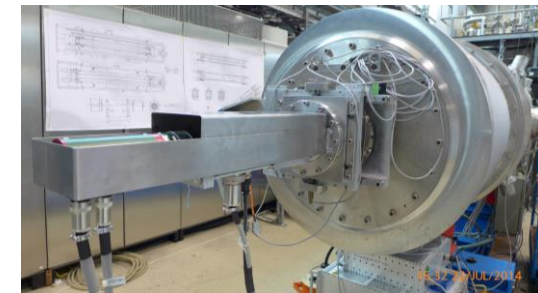
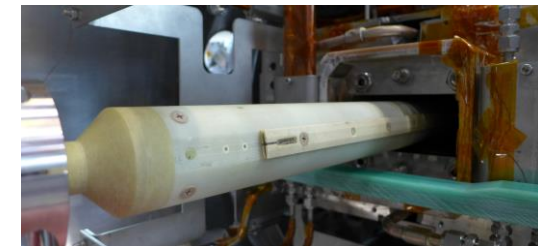
# New Measurement Systems for Qualifying SIS100 Series Dipoles

## Field measurements @ 4.5K in vacuum

Mechanical adaptation of the CERN rotating coil probe R30/L1200mm (tangential coils) for the field measurements in vacuum @ 4.5K



ferrofluidic rotary feedthrough



Start of development - Oct. 2013  
First measurements in FoSD Jul. 2014

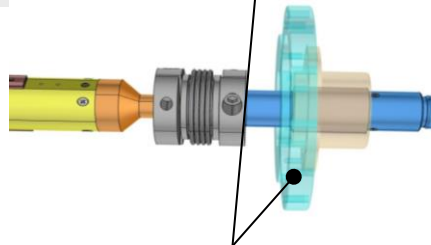
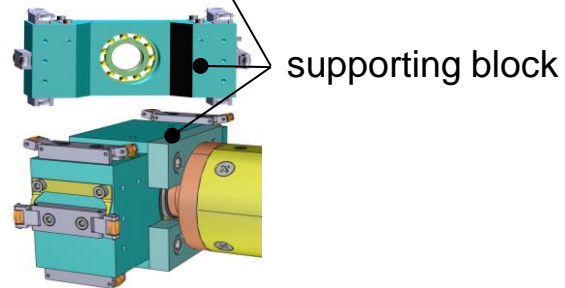
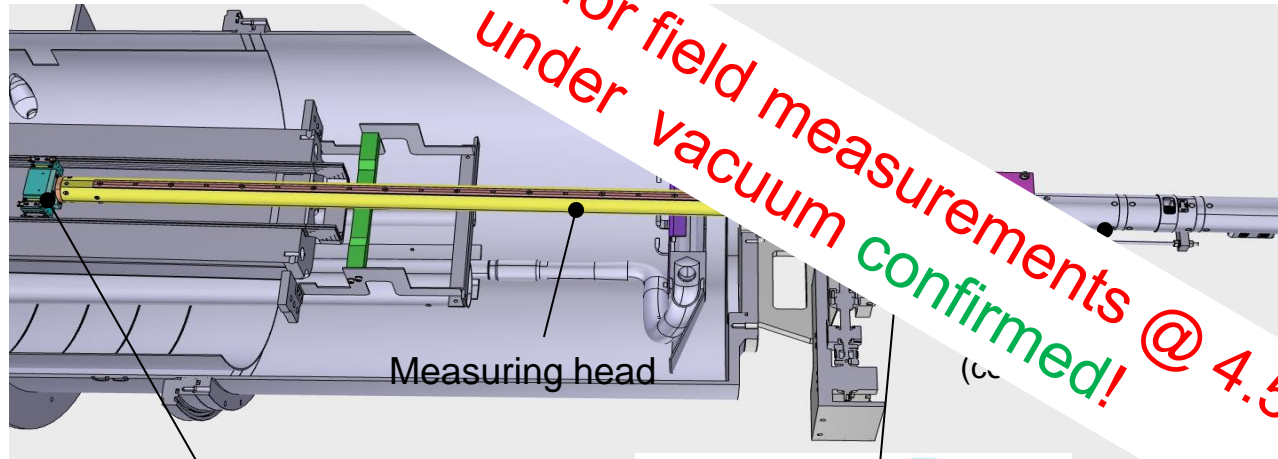
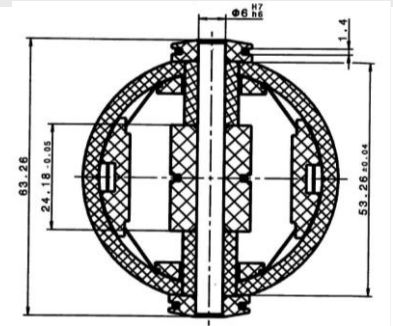


# New Measurement Systems for Qualifying SIS100 Series Dipoles

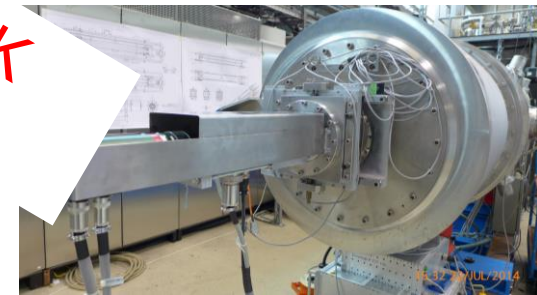
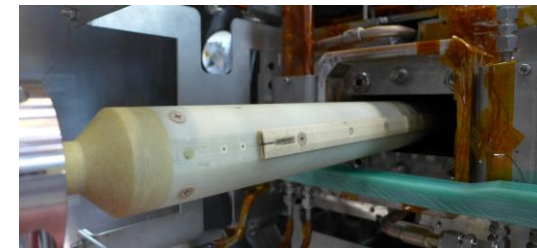
## Field measurements @ 4.5K in vacuum

Mechanical  
(tangential)

of the CERN rotating coil probe R30/L1200mm  
field measurements in vacuum @ 4.5K



ferrofluidic rotary  
feedthrough

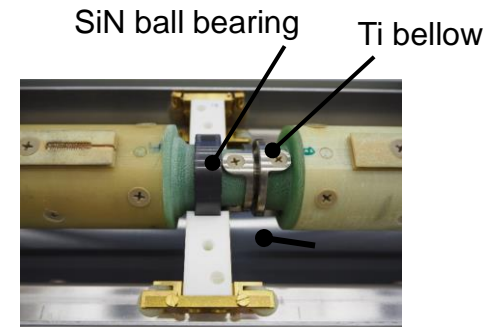
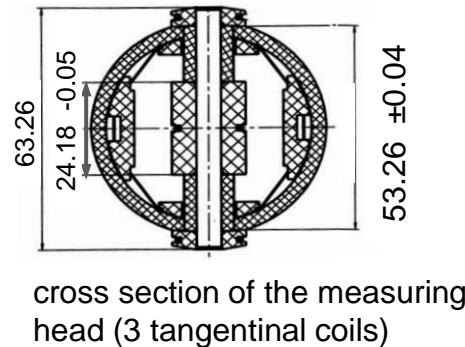
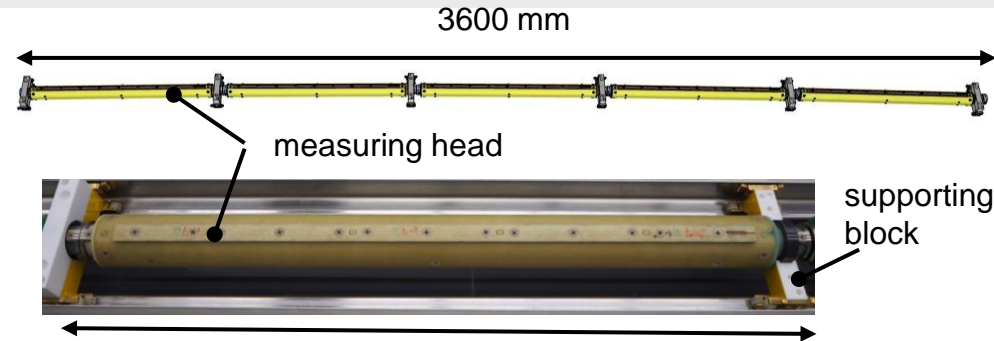


Start of development - Oct. 2013  
First measurements in FoSD Jul. 2014

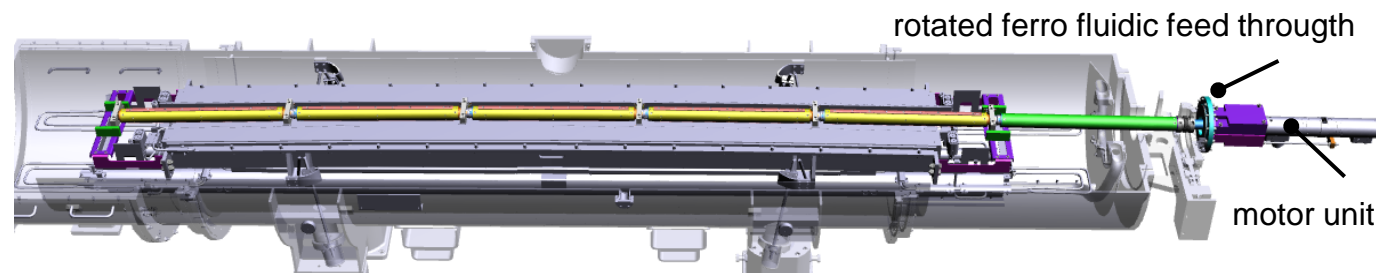
# New System for Magnetic Field Measurements

## System for magnetic field measurements

- ✓ 5 measuring heads – tangential coils
- ✓ 3 pick up coils per head, 600 mm length
- ✓ effective surface  $1.67 \text{ m}^2$
- ✓ Ti-alloy bellows – interconnection between segments and to align the heads along the beam axis
- ✓ SiN ball bearings for rotation motion
- ✓ ceramic supporting blocks for transverse positioning in the gap



Field measurements  
in vacuum @ 4.5K



The measuring probe is designed and built in collaboration with CERN

# New System for Magnetic Field Measurements

## Mechanical challenges

- all material should be non-magnetic
- thermal expansion
- Ceramic  $\text{Si}_3\text{N}_4$  ball bearings
  - moving at 4.5 K (no grease or oil)
  - many different types tested
- Ti-alloy bellows
  - shaped for eddy-current reduction
- Ceramic holder with small wheels for installation
  - two parts for easier maintenance
- Peek screws (nylon didn't work)



courtesy F. Kaether (SCM)

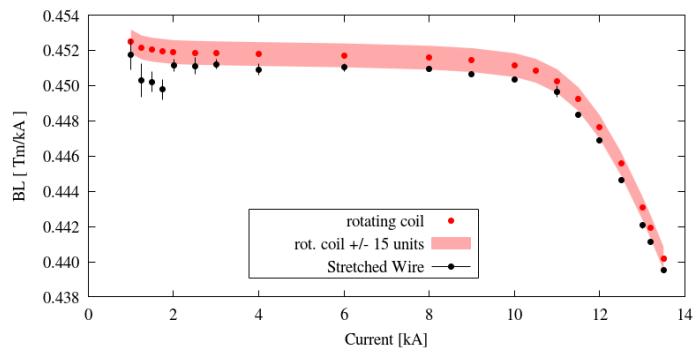


# New Measurement Systems for Qualifying SIS100 Series Dipoles

## Calibration of the magnetic field measuring probe

- ✓ calibration @ 300K in NC dipole
- ✓ surface calibration → precise measurement  $B_1, \int B dl$
- ✓ angular displacement of the head relative to the reference one, i.e., the middle segment → direction  $B_1$ , higher order harmonics
- ✓ lengths of the interconnection areas between the segments → precise measurement  $\int B dl$

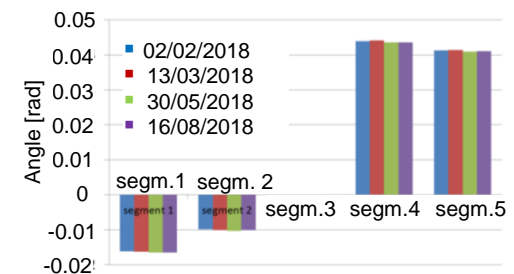
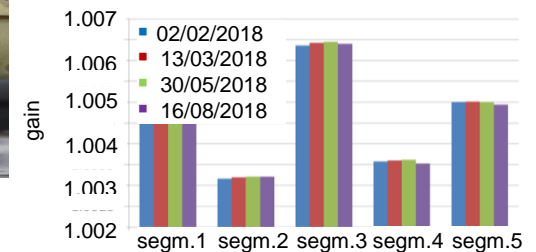
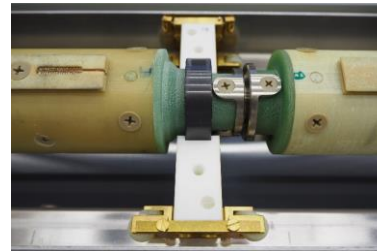
does the warm calibration work for the cold measurements?



yes, it works and is precise enough for qualifying of the SIS100 dipoles.

Required precision  $< 4 \times 10^{-3}$

mechanic of the MF-probe is not affected by thermal cycles.  
The calibration stays stable





# New Measurement Systems for Qualifying SIS100 Series Dipoles

## System for high precision gap height measurement V2

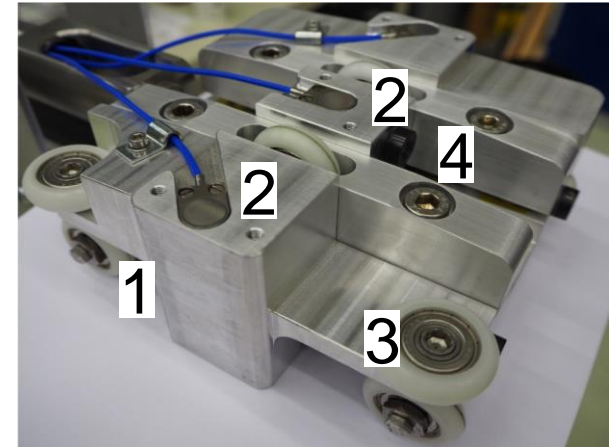
- ✓ 6 capacitive sensors CSH1,2FL(20)-CRm 4,0 from Micro - Epsilon GmbH & Co.KG
- ✓ linear encoder WDS-100-P 115-CR from Micro-Epsilon GmbH & Co for reproducible positioning of the carriage along the magnet

absolute precision  $15\mu\text{m}$

relative precision  $< \pm 3\mu\text{m}$

} @ 300K

In combination with a laser tracker, the system provides data regarding the yoke's sag and twist.



1 carriage, 2 capacitive sensors, 3 wheels, 4 holder for spherically mounted retroreflectors.





# The Team for SIS100 Dipole Testing



design,  
physics,  
evaluation,  
et al.

+ W. Freisleben, M. Al Ghanem, A. Zaghloul, H. Bouillot, V. Velonas, K. Knappmeier, A. Junge, T. Ziglasch

- survey & alignment
- electrical integrity
- field measurement
- quench detection
- cryo operators
- DAQ, control and analysis
- transport & installation
- quality assurance
- Communication with production
- test coordinators

## GSI departments

SCM, QA, TRI, CRY, EN-  
MG, EPS, VAC, BB, RHV  
Support on demand –  
MEWE, KB, ENG

# Site Acceptance Test (SAT): Sequence

## ■ Reception

- ✓ visual inspection
- ✓ document check

## ■ SAT @300 K (incoming) 5 days to 4 weeks if non-conformities

- ✓ geometry
- ✓ instrumentation
- ✓ electrical insulation
- ✓ pressure and leaks, massflow rate

## ■ Mounting on the test bench

2 - 3 days

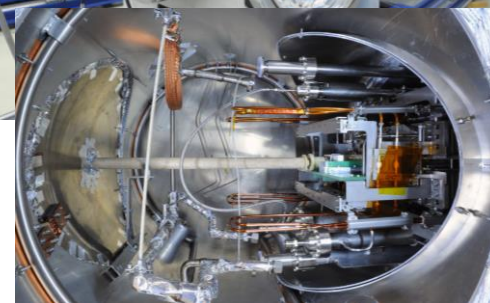
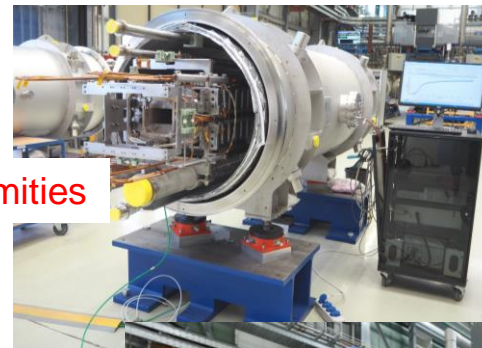
- ✓ Installation of the MF-probe
- ✓ electrical integrity magnet+current leads
- ✓ pumping - 24 h
- ✓ cool down – 76 - 90h

## ■ SAT @ 4.5K 3 - 4 days

- ✓ electrical integrity and insulation
- ✓ magnet training
- ✓ inductance
- ✓ magnetic field
- ✓ static and AC losses

## ■ warming up and dismounting 4 - 5 days

## ■ SAT @ 300K (outgoing) - 2 days





# Site Acceptance Test (SAT): Sequence

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- ✓ visual inspection
- ✓ document check

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- ✓ pressure and leaks, massflow rate

## ■ Mounting on the test bench 2 - 2

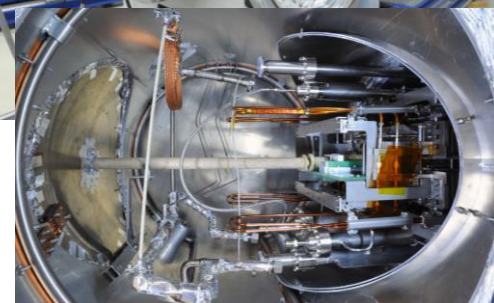
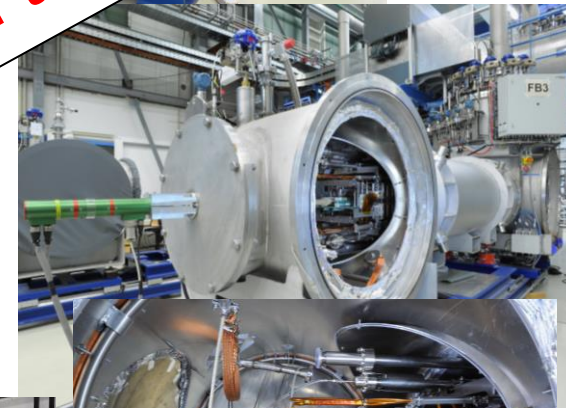
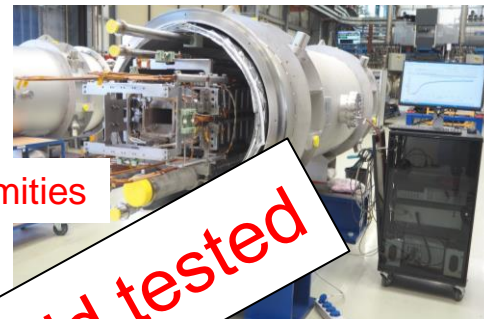
- ✓ Installation of the MF-probe
- ✓ electrical integrity magnet+cable
- ✓ pumping - 24 h
- ✓ cool down - 76 - 0

## ■ SAT @ 4.5K

- ✓ electrical insulation
- ✓ magnetic field
- ✓ static and AC losses

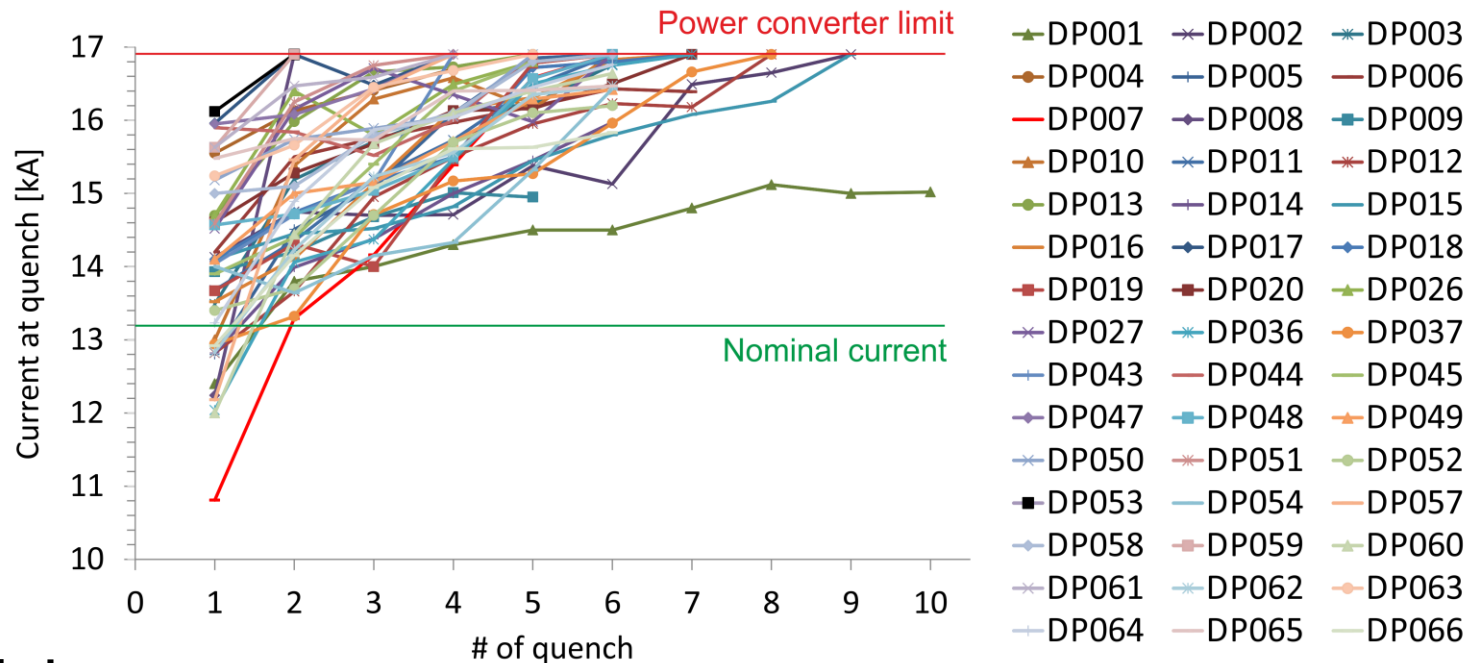
## ■ warming up and dismounting 4 - 5 days

## ■ SAT @ 300K (outgoing) - 2 days



47 out of 110 magnets have been cold tested

# SIS100 Series Dipole Magnets: Training



45 magnets tested @ cold

## Specified:

- nominal current (nc) to be reached:
  - at 3rd quench in first cycle
  - at 1st quench in further
- de-training limited to 5 % of nc (compared to previous quench)
- quench current has to stabilize at 110 % of nc at least (14.5 kA)

Outstanding quench performance!

- ✓ nom. current reached at 2nd quench at least
- ✓ no significant de-training observed

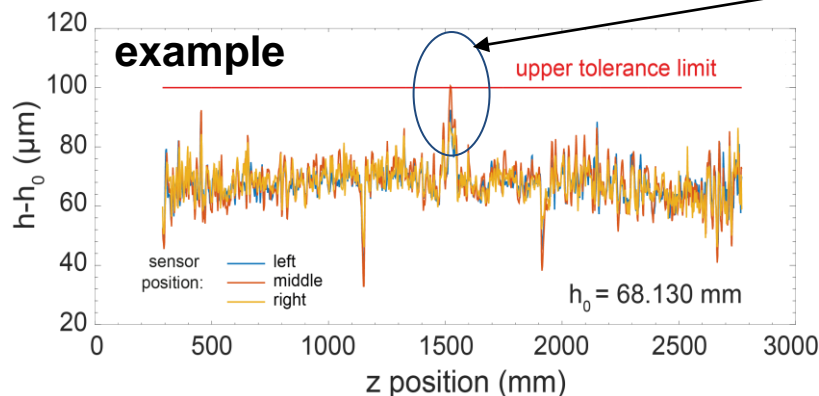
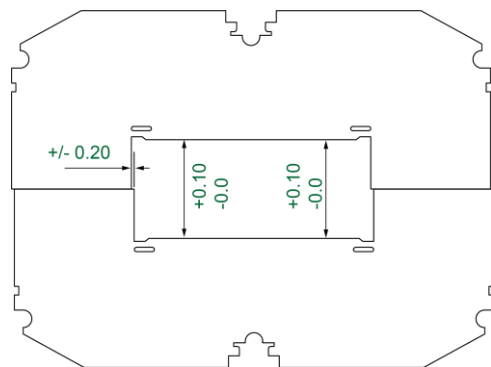
Training close to the short sample limit of the cable (17.8 kA)

→ high stability of the coil structure in the yoke.

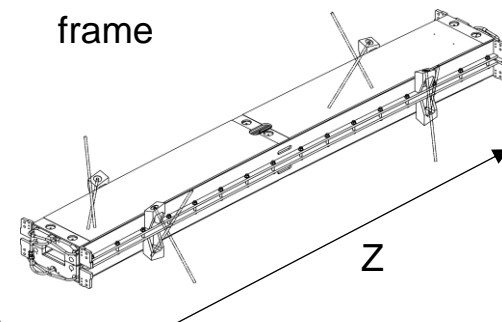
# Test Results for SIS100 Series Dipoles

## Gap geometry

required:



spot welding of lamination to outer frame

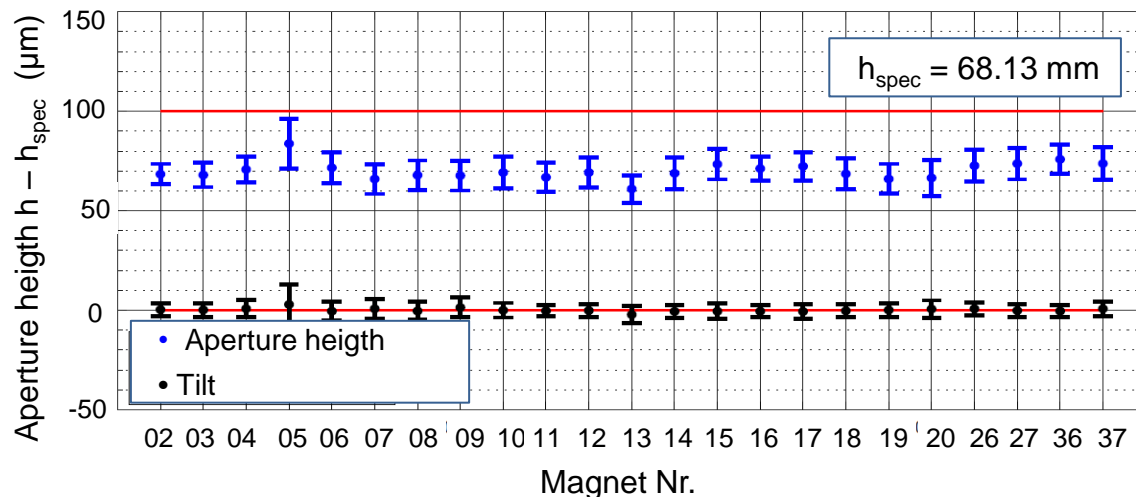


## aperture height ( $\rightarrow$ BL)

- well within specification on average for each magnet
- **very good reproducibility**

## tilt ( $\rightarrow a_n, b_n$ )

- **negligible**





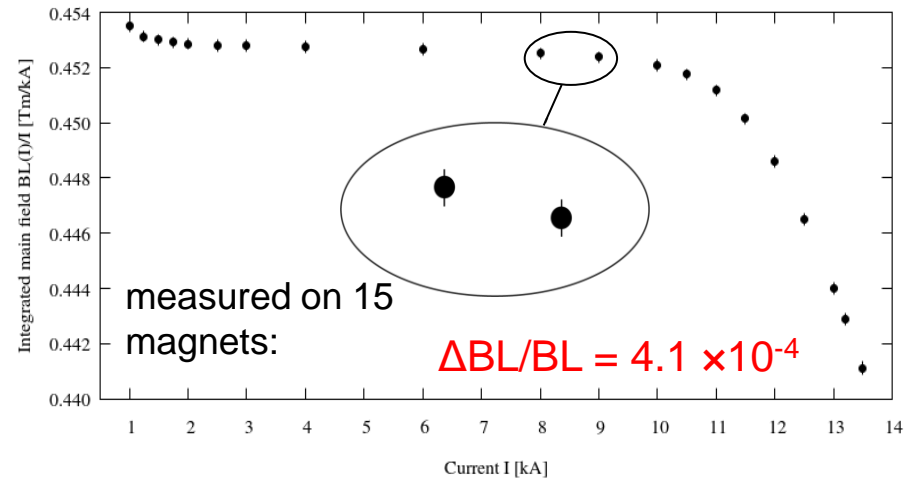
# Test Results for SIS100 Series Dipoles

## Integral Field

acceptance criteria for SIS100:

$$\Delta BL / BL \leq 4 \times 10^{-3} \quad \text{with } BL = \int B(l) dl$$

measured on 15 magnets:  $\Delta BL / BL = 4.1 \times 10^{-4}$



## Field homogeneity

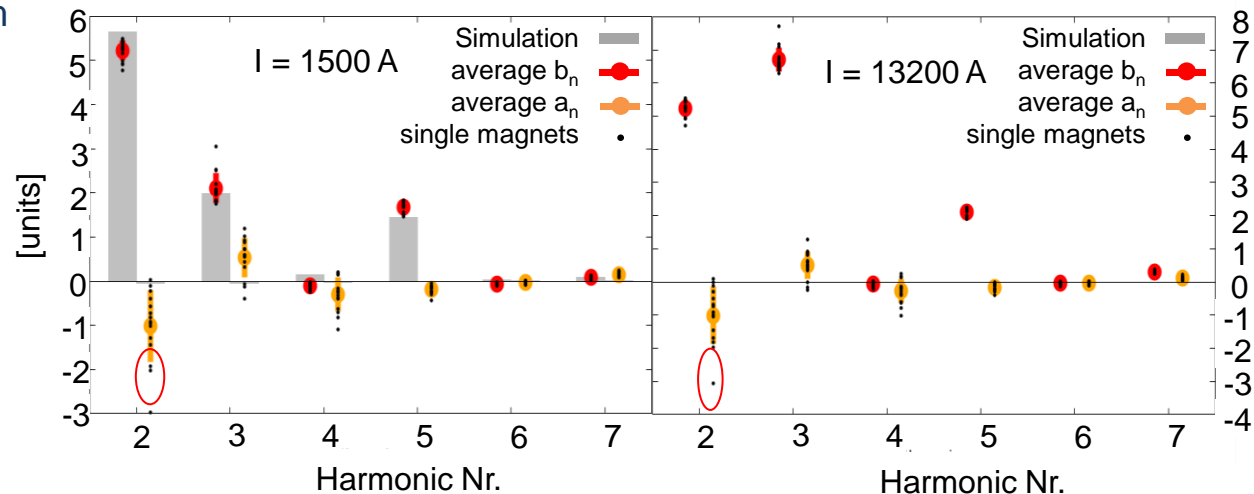
acceptance criteria:

$$\sum_n C_n / B_1 < \pm 6 \text{ units} \quad @ R_{ref} = 30 \text{ mm}$$

measured on 15 magnets:

- ✓ magnet data acceptable for synchrotron operation
- ✓ good agreement with expectation except:
  - $b_3$  systematic → correctable
  - $a_2$  under investigation
- ✓ high reproducibility ( except ... )

$$B(z = x + iy) = \sum_n C_n \left( \frac{z}{R_{ref}} \right)^{n-1} \quad \text{with } C_n = B_n + iA_n$$



# Next Activities at Test Facilities for SC Magnets

**SAT for SIS100 Dipole** ~29th Sept. 2017 – Mai. 2020

delivery rate - 1 magnet per week starting from the 5th one (approximately. from Dec.2017).

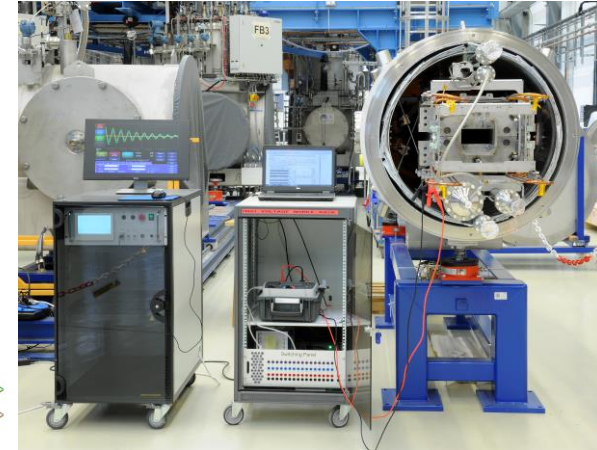
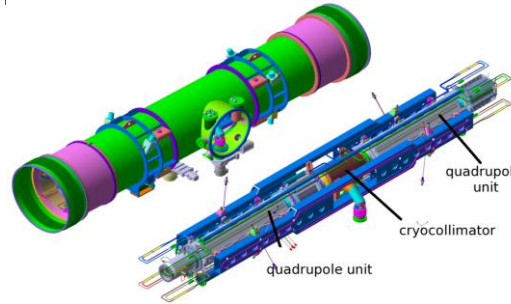
**SAT for FoS Quadrupole Module (Typ 2.5) for SIS100** ~ Q3/2019

## String Test

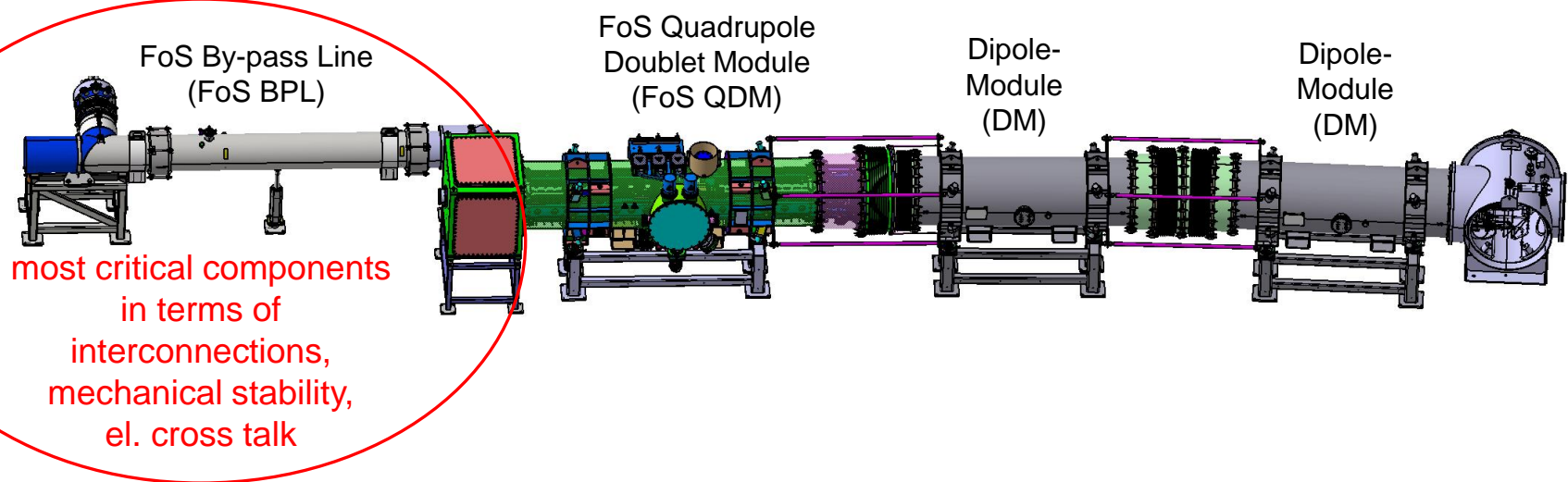
- from Q1 2020 to Q4 2020

## Other testing activities

- 13 pairs of the Main Current Leads (14kA DC HTS ) for SIS100 ~ March 2016 – Sept. 2019
- FoS BPL (long unit)
- Feed-, End- and Current Lead Boxes for SIS100 of one type
- FoS VC for the SIS100 dipole
- LCL for SIS 100
- Cryocatcher
- CL (FoS) for Super-FRS

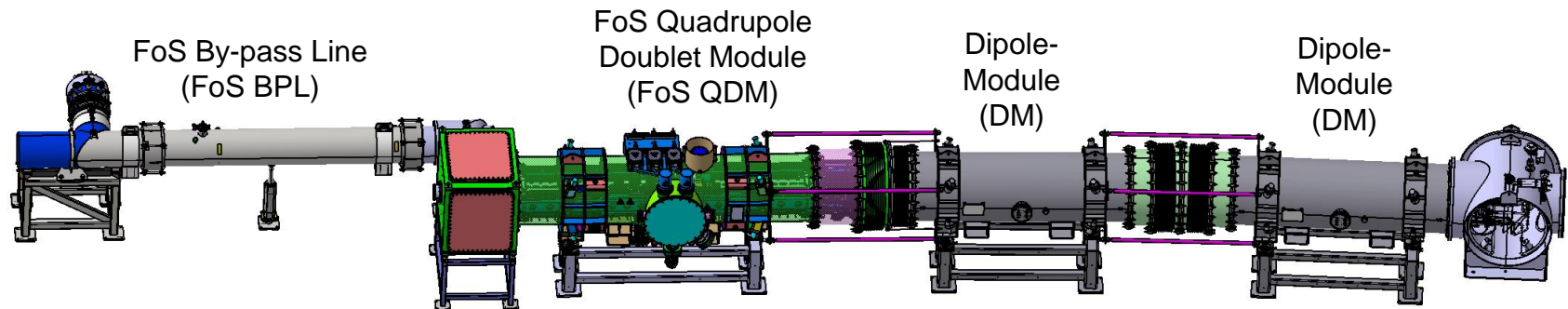


# SIS100 String Test



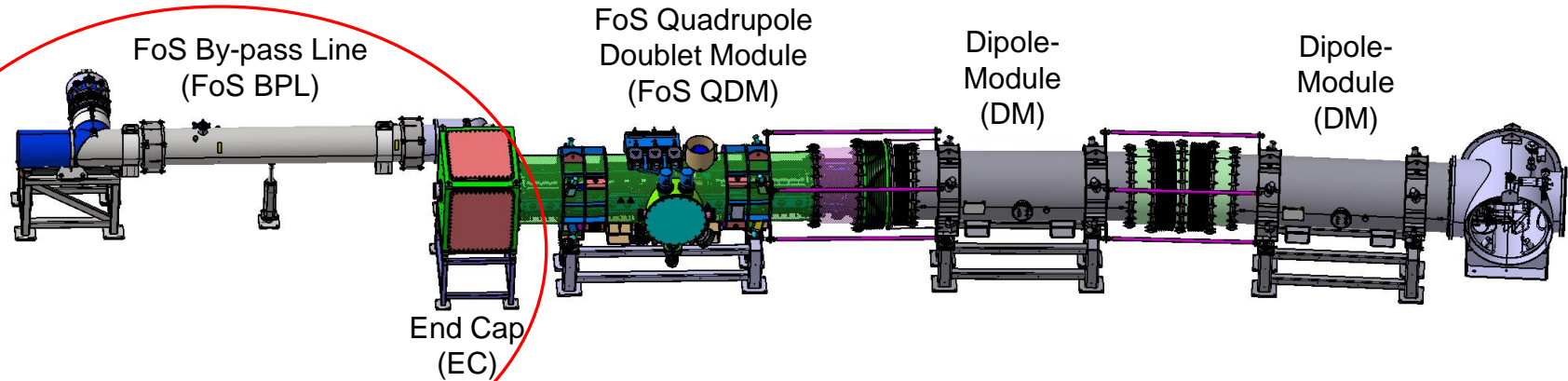
- a short section of SIS100 built of main cryo-magnetic and local-cryo components of the SIS100
- verification of different interfaces and interconnections regarding fitting and mountability
- preparation for installation, commissioning and operation of SIS100

# SIS100 String Test: Objectives

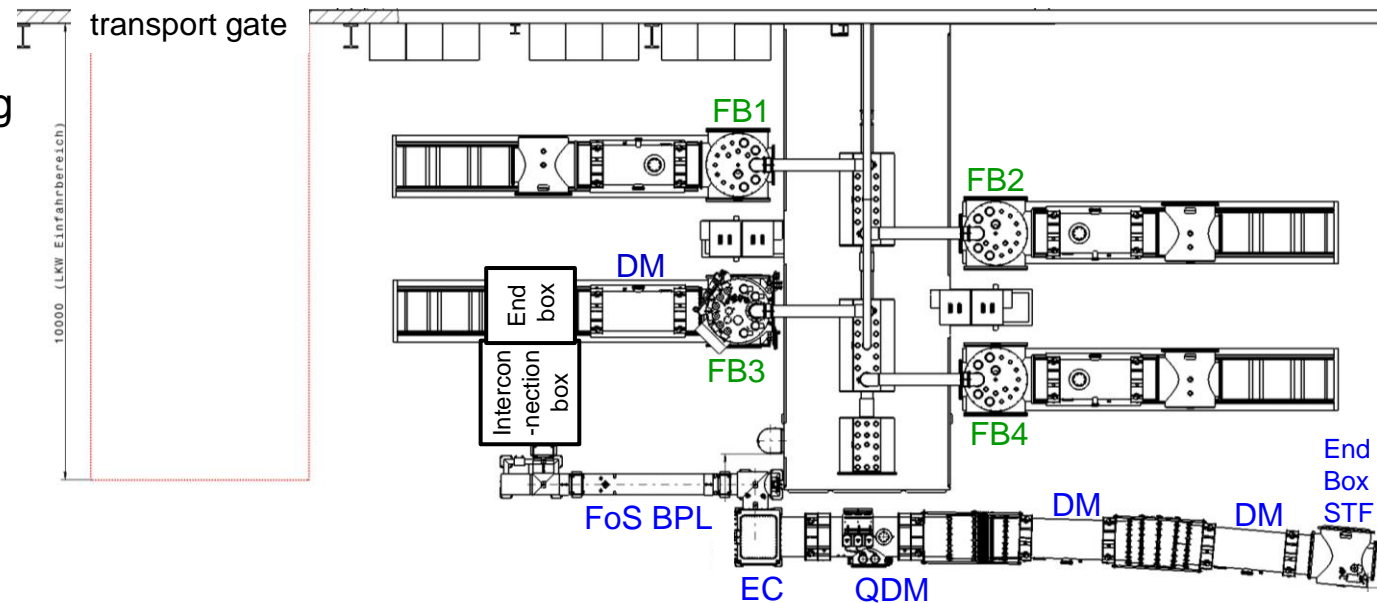


- preparation of work instructions for the machine installation (cooperation of SCM, CRY, UHV, TRI, ENG, TEL, FSB, approval through WPLs, SPL SIS100)
- choosing appropriate tools for installation in the tunnel
- mechanical stability of interconnections
- insulation vacuum stability and performance of the UHV components
- cooling down behaviour, functionality of parallel cooling channels and local cryo-components
- electrical issues – cross-talk between live circuits, degradation of insulation resistance
- testing of new quench detectors and cabling
- testing of the slow control system

# Configuration of the SIS100 String

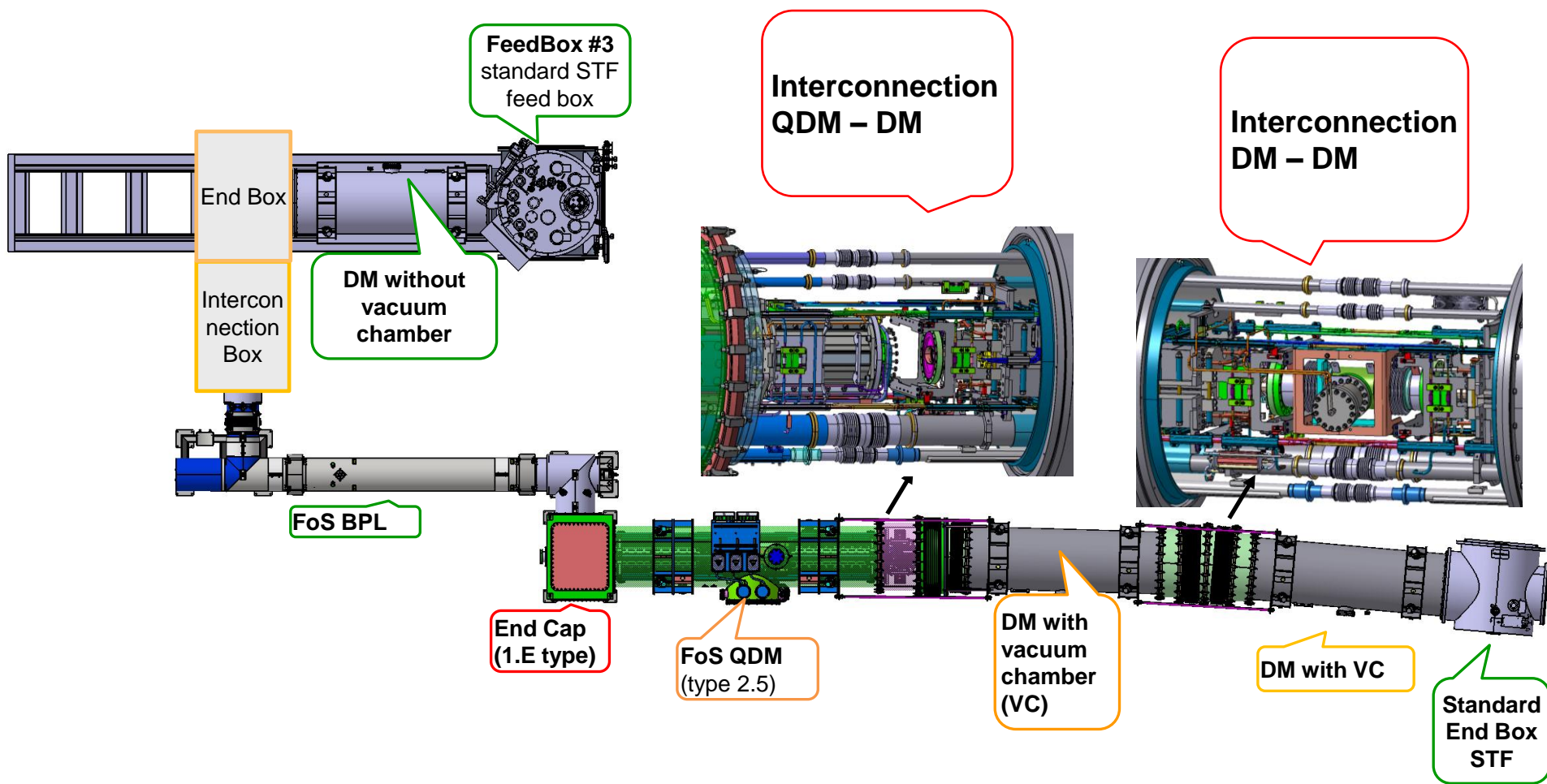


Arrangement of the string at STF





# SIS 100 String Layout and Single Components



# Time Line & Required Resources

## Milestones for realisation of the string test

definition of the useful configurations	DMU for installation at STF	final decision for the string configuration	design of the auxiliary constructions	procurement of the auxiliary constructions	assembly of the string	testing phase
28.09.2018	23.10.- 31.10.2018	18.01.2019	02.- 06.2019	06.2019 - 01.2020 availability of the end cap and interconnection bellows 01.2020	02.-03. 2020	03. – 08.2020

## Requirements:

- upgrade of the infrastructure at STF (e.g. warm cables to the 20kA PC, additional electronics for QuD, DAQ)
- design and production of auxiliary constructions
- human resources: SCM, CRY, EPS, ACO,UHV, TRI, DMU, ENG, MEWE, EKM

- The sc magnets for SIS100 have been developed at GSI based on the Nuclotron magnets
- Magnet development: FEM and CAT models → short magnet models → full size prototypes -> FoS magnet; dipole: 2001 to 2013, quadrupole module: 2001-2017
- The series production of the SIS 100 dipole magnets started in August 2016 and the series production of quadrupole and corrector magnets started in Q2 2019
- The infrastructure required for the qualification of magnets was constructed/set up at GSI by close collaboration of colleagues from CAM, GAT, CRY, EPS, SCM and TRI departments
- Quality control and functionality tests at contractor and GSI site were defined
- High precision measurement systems for magnet evaluation were developed
- The measurement results obtained on the series dipole magnets reveal an excellent performance of the chosen design and high production quality (outstanding magnet training performance, coil stability, etc.)
- Since the geometrical properties of the aperture define the magnetic field quality, they are tracked for all series magnets
- The magnetic field shows very low variation in terms of the field integral and the low harmonic content is satisfactory for beam physics requirements.
- The magnet series production is ongoing: some „childhood diseases“ still to be overcome
- Currently the FoS quadrupole module is expected to be delivered in the end of August.
- The next challenges for magnet testing are the FoS quadrupole module and magnet string tests

Thank you for your attention