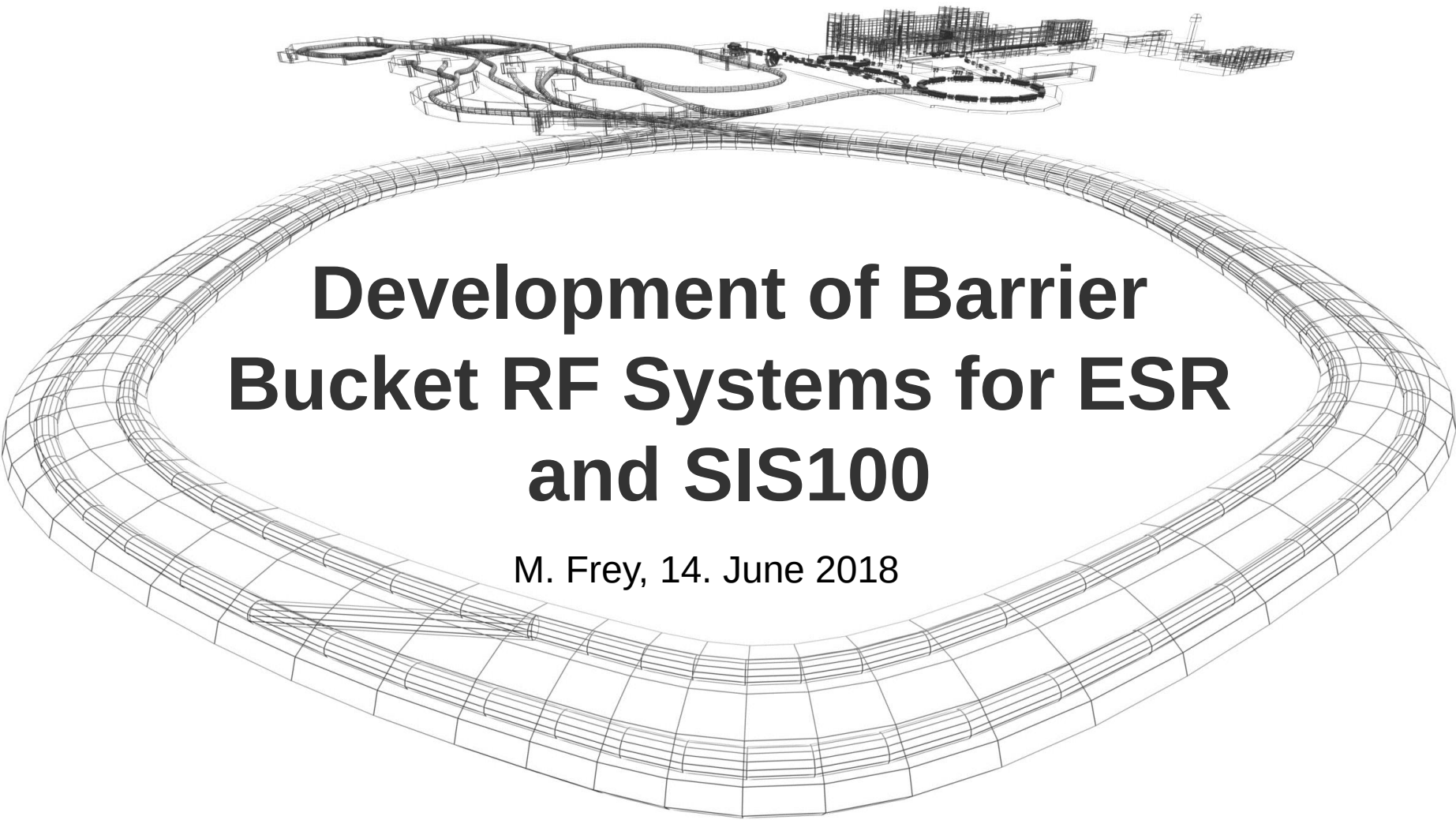


A large, detailed wireframe model of a particle accelerator is shown in the background. It features a large, oval-shaped ring structure with multiple internal components and a complex network of pipes and structural elements. The model is rendered in a black and white wireframe style, highlighting the intricate geometry of the facility.

Development of Barrier Bucket RF Systems for ESR and SIS100

M. Frey, 14. June 2018

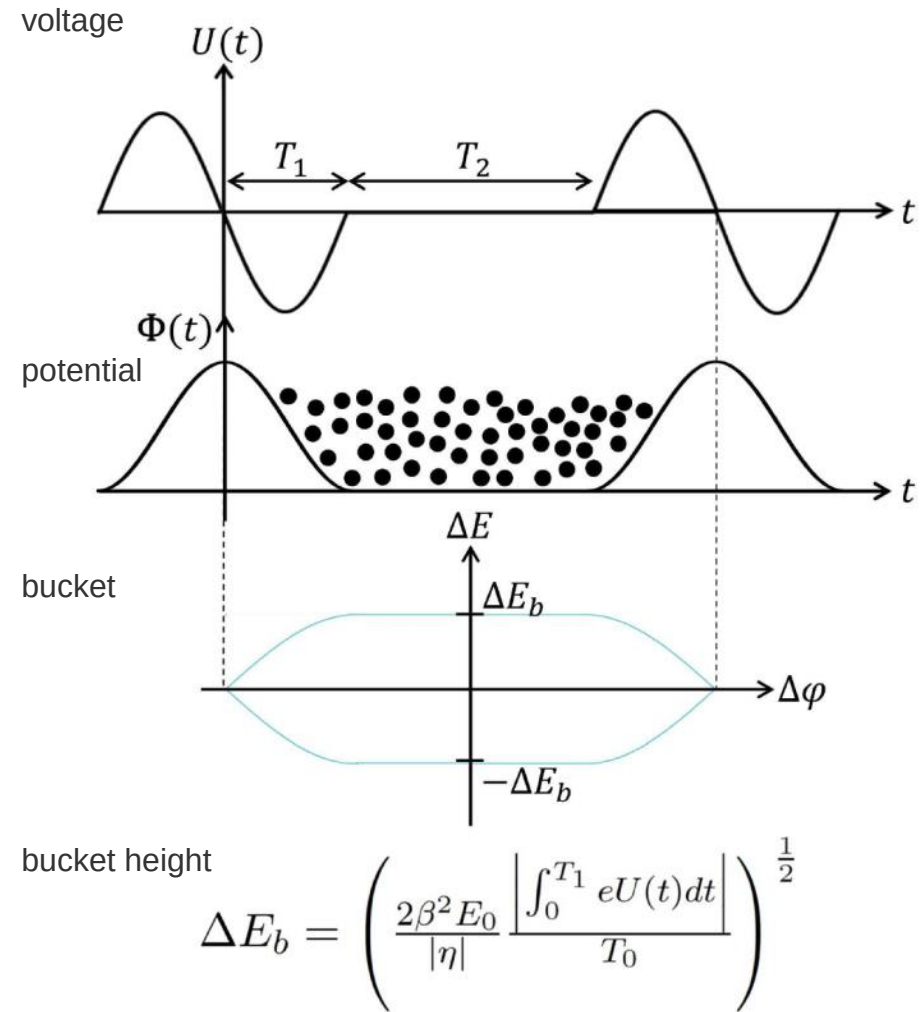
outline

- motivation/history at ESR
- ESR BB system
 - requirements
 - theory of operation
 - choice of ring core material
- ESR BB cavity design
 - prototype ring core impedance measurement+modeling
 - PSpice simulation of full cavity
- ESR BB cavity properties
- ESR BB pre-distortion
- ESR BB signal generation
- ESR BB full system results
- ESR BB outlook

- SIS100 BB system

motivation

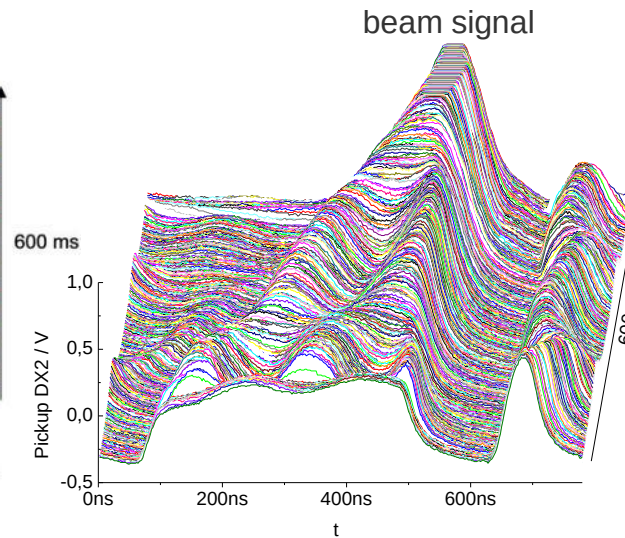
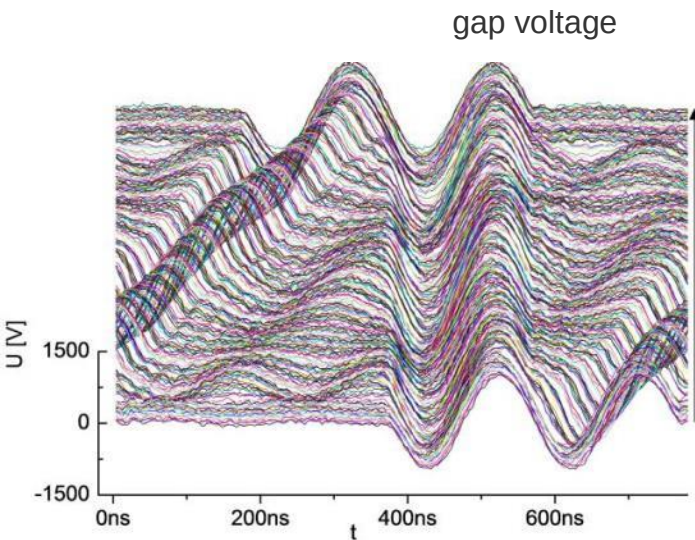
- RF pulses create potential barriers
- barrier creation allows longitudinal beam manipulation, e.g. confinement of a bunch
- when barriers are moved, beams can be compressed -> intensity increases
- multiple injections between compression operations lead to further intensity increase („longitudinal stacking“)



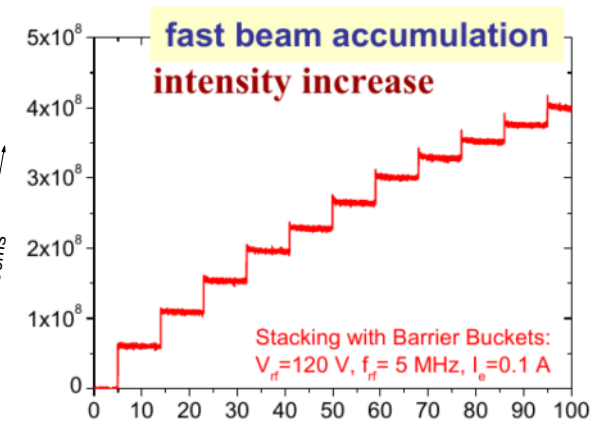
J. Harzheim, Temf, TU Darmstadt

demonstration at ESR

- ferrite acceleration cavities were used with single sine + offset pulses



G. Schreiber, LRF department, GSI



C. Dimopoulou, BCO department, GSI

- hardly feasible due to extreme sensitivity concerning pulse parameters



development of a specialized BB cavity

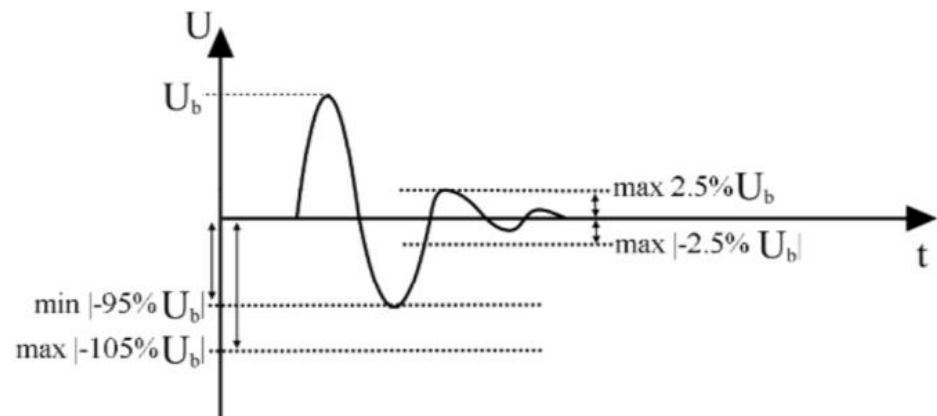
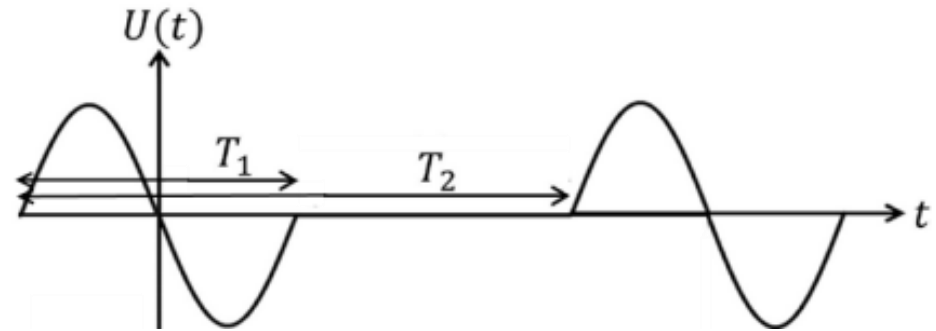
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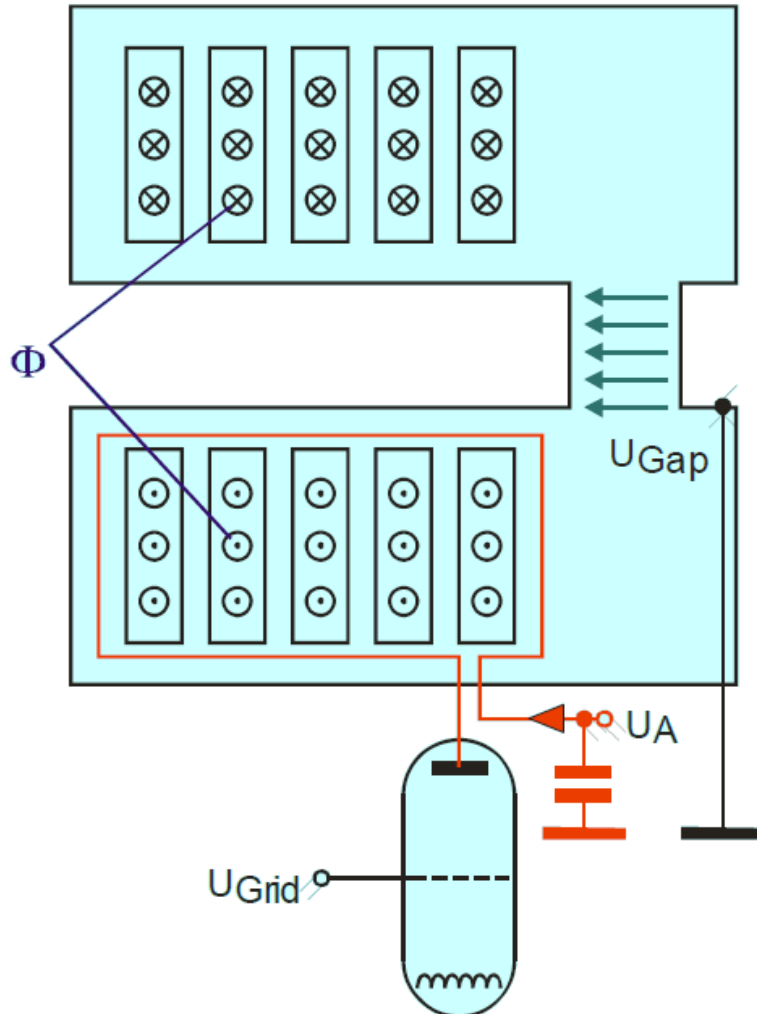
- SIS100 BB system

ESR requirements

- single sine pulses of $T_1=200$ ns ($f_{BB}=5$ MHz)
- pulse amplitude $\hat{U} = 1$ kV
- flexible control of amplitude and repetition period T_2 at injection energy: 4-400 MeV (between $f_{rep}=250$ kHz and $f_{rep}=2$ MHz)
- symmetry and low ringing



ESR cavity design – theory of operation



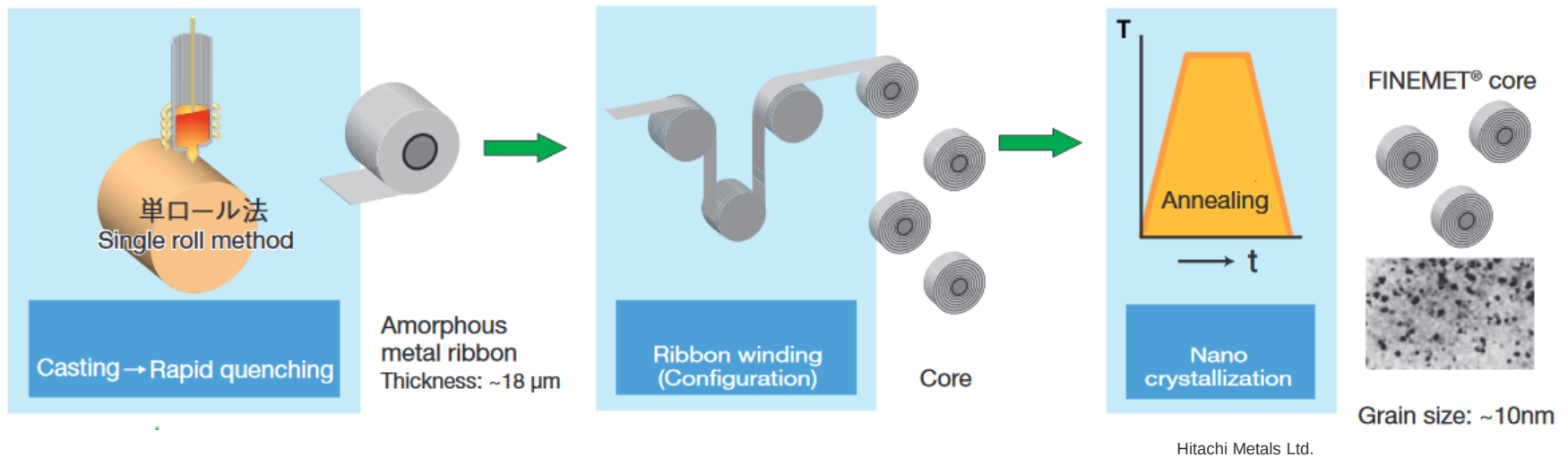
- cavities with ring cores are transformers: ring core = iron core, housing = secondary winding, gap capacity = load
- ring cores are a lossy inductance defined by geometry and complex $\underline{\mu}_r$

$$L_0 = l \frac{\mu_0}{2\pi} \ln\left(\frac{d_o}{d_i}\right) \quad L = L_0 \mu_r' \quad R = \omega L_0 \mu_r''$$

- ring core inductance L, resistance R and gap capacity C form RLC circuit
- loss effects in ring cores described by μ_r'' ($\sim R$) -> define oscillation damping -> bandwidth

ESR cavity design – ring core material

- ferrites: high Q-value -> narrowband cavities ☹️
- iron-based nanocrystalline Magnetic Alloy (MA) ring cores: very low Q-value -> broadband cavities 😊



- cores are wound from thin ribbon: side surfaces are roughly textured because layers tend to misalign (important for cooling)

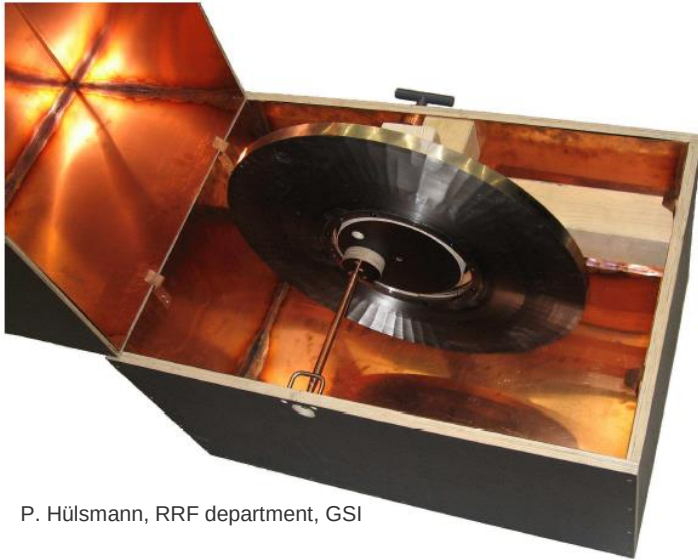
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strategy: ring cores dominate cavity
 → analyse prototype core to enable
 simulation of full cavity → obtain
 amplifiers load impedance

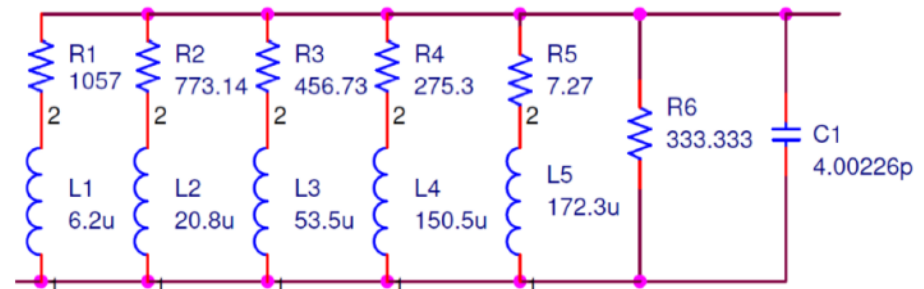
ESR cavity design – impedance measurement and PSpice modeling



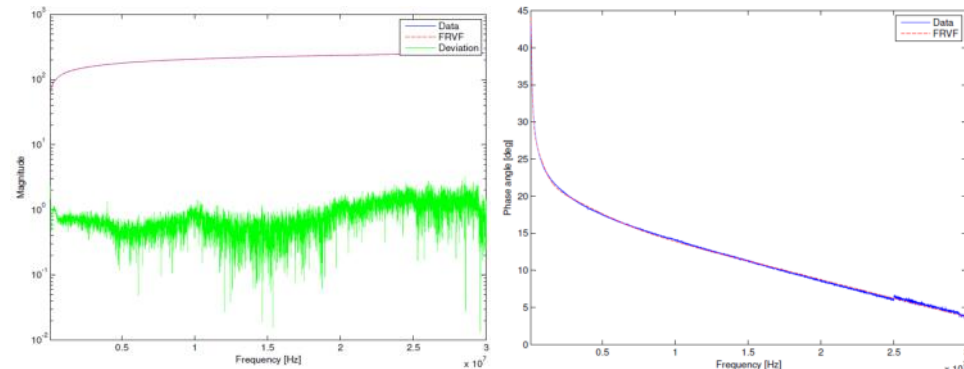
P. Hülsmann, RRF department, GSI

- impedance measurement of prototype core in test box
- subtraction of test box influence (estimated with CST simulation)

- identification of lumped-element equivalent circuit using „vector-fitting“ algorithm

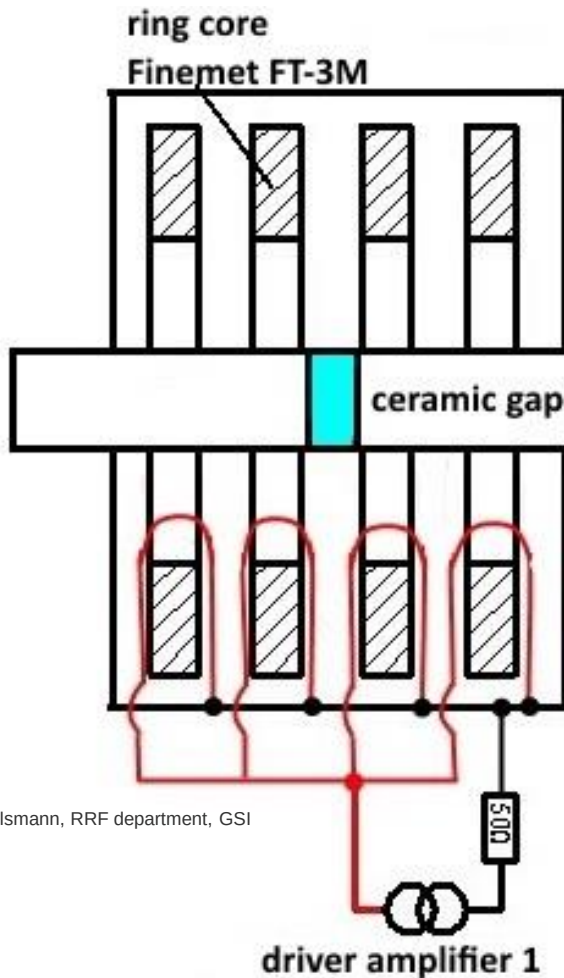


J. Harzheim, H. Klingbeil, Temf, TU Darmstadt



- 1 ring core at 5 MHz: $|Z| \approx 200 \Omega$

ESR cavity idea

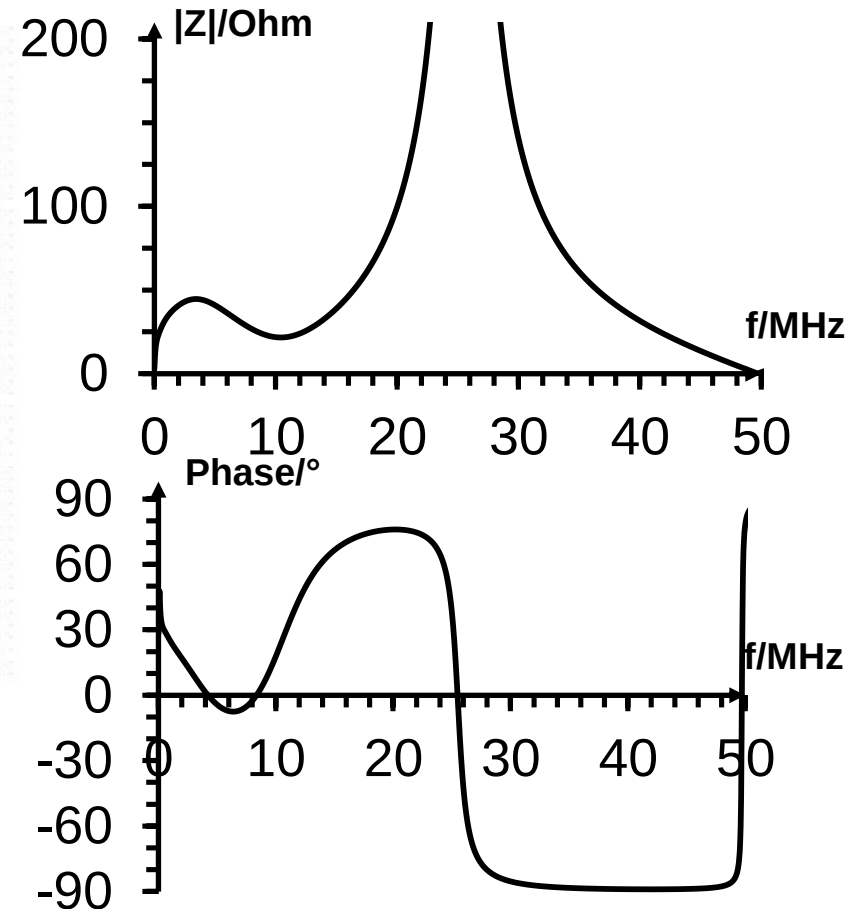


- 4 ring cores connected in parallel
-> gap voltage
= 4 x voltage at load
- one cavity per pulse
(2 in same housing)

P. Hülsmann, RRF department, GSI



- sufficient matching between amplifier and cavity at 5 MHz
- at 5 MHz and $|Z|=25\ \Omega$,
 $U=4 \times 225\ \text{V} = 900\ \text{V}$
 possible with 1 kW



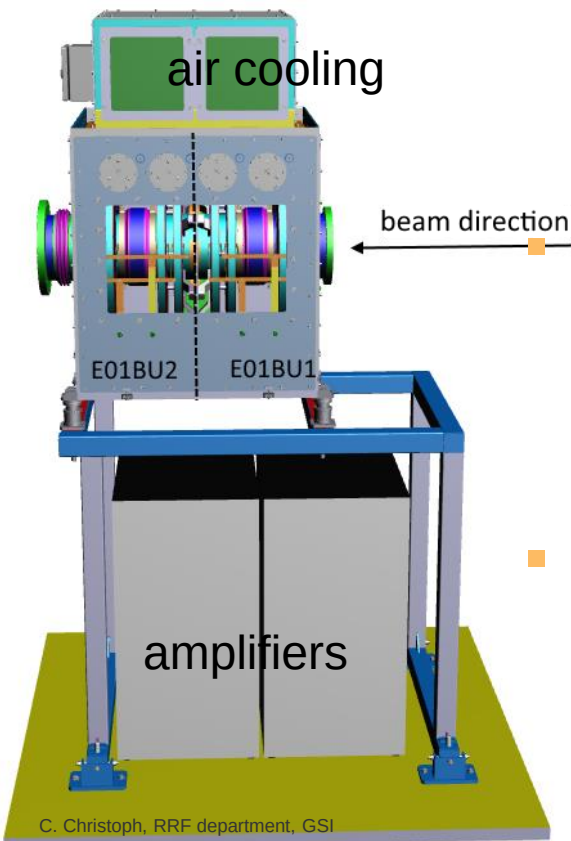
satisfying results



production approval

ESR cavity design – CAD and production

- based on extensive testing with ARD broadband test cavity



- very short beam pipe requested (for Schottky pick-up on same base-frame)
- large ESR beam pipe diameter -> little space for ring core material
- power range of amplifiers 1 kW -> air cooling necessary

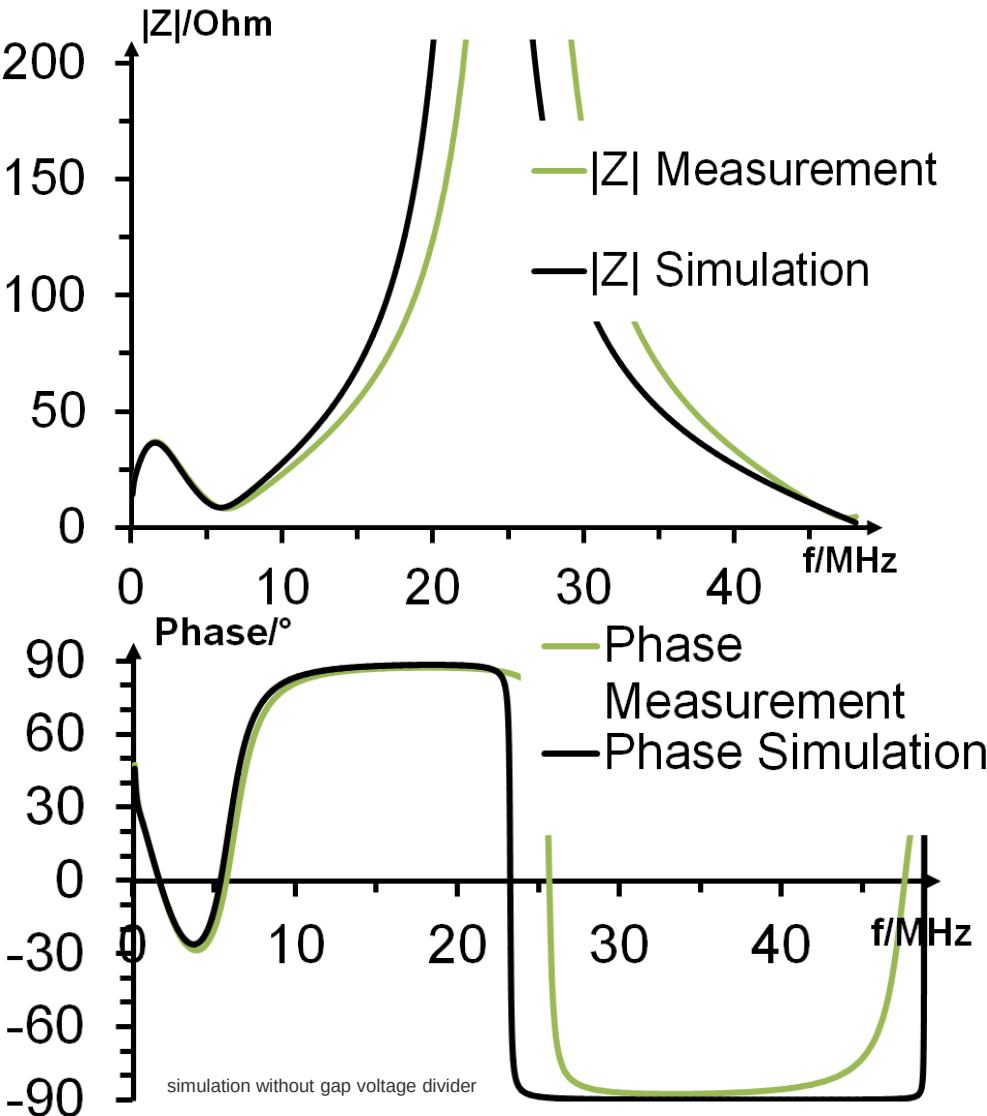


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- **ESR BB cavity properties**
- **ESR BB pre-distortion**
- ESR BB signal generation
- ESR BB full system results
- ESR BB outlook

- SIS100 BB system

ESR cavity properties



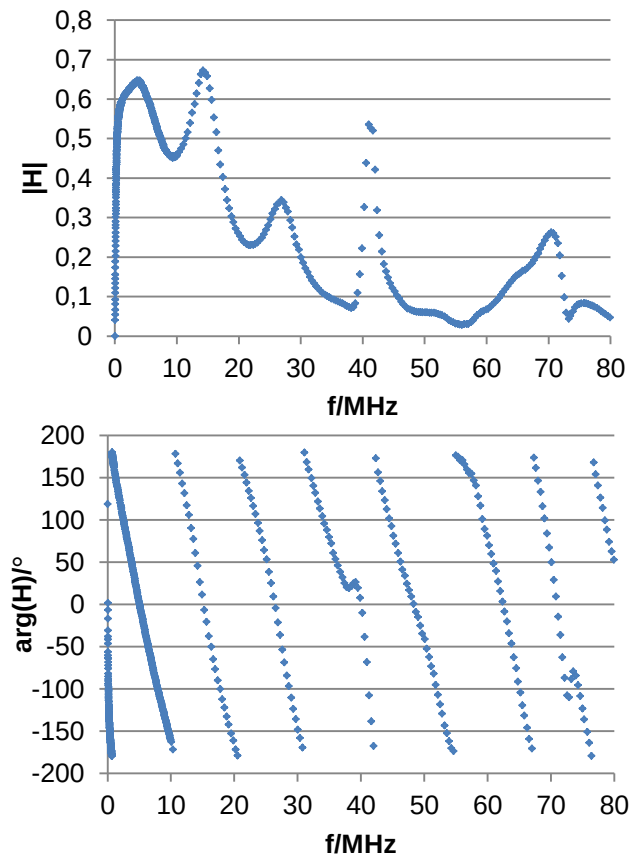
measurement result:

- frequency response results in distortion of input voltage
- pre-distortion of signals is necessary



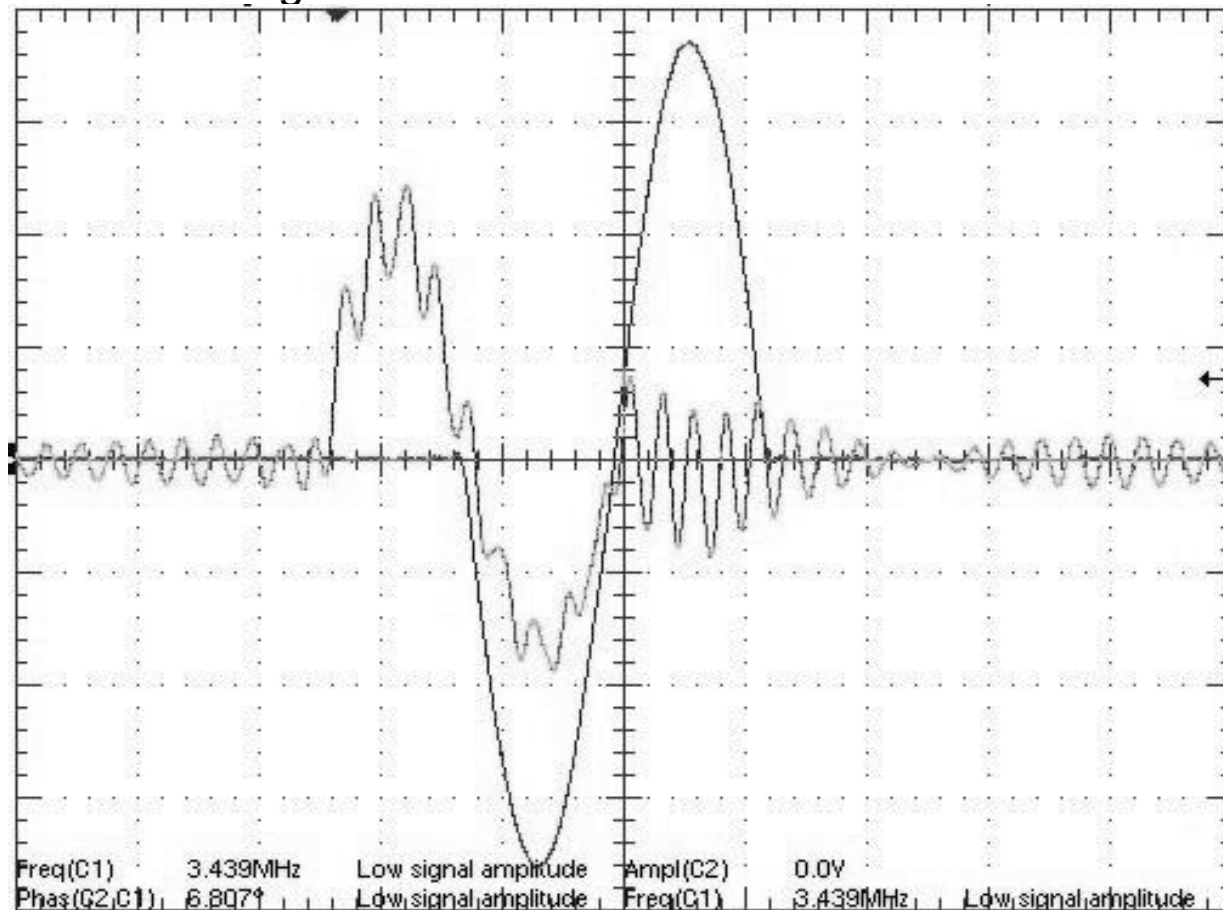
LLRF - pre-distortion of signals

1. measure transfer function $\underline{H}$



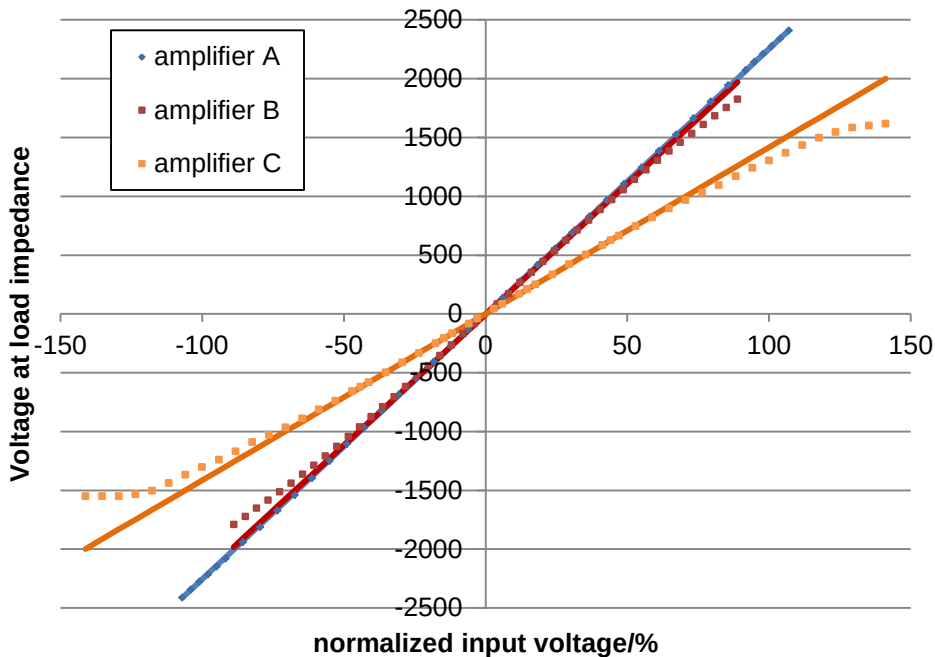
2. calculate Fourier-coefficients of pre-distorted signal

3. transformation to time-domain + application

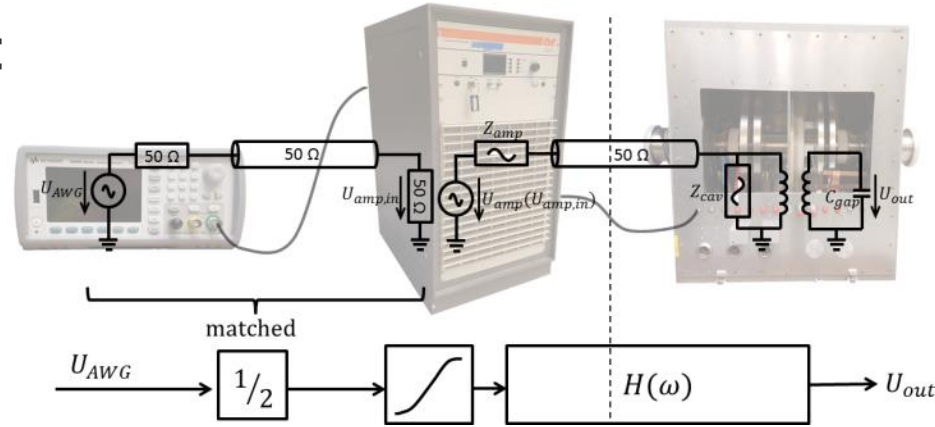


LLRF - non-linear predistortion

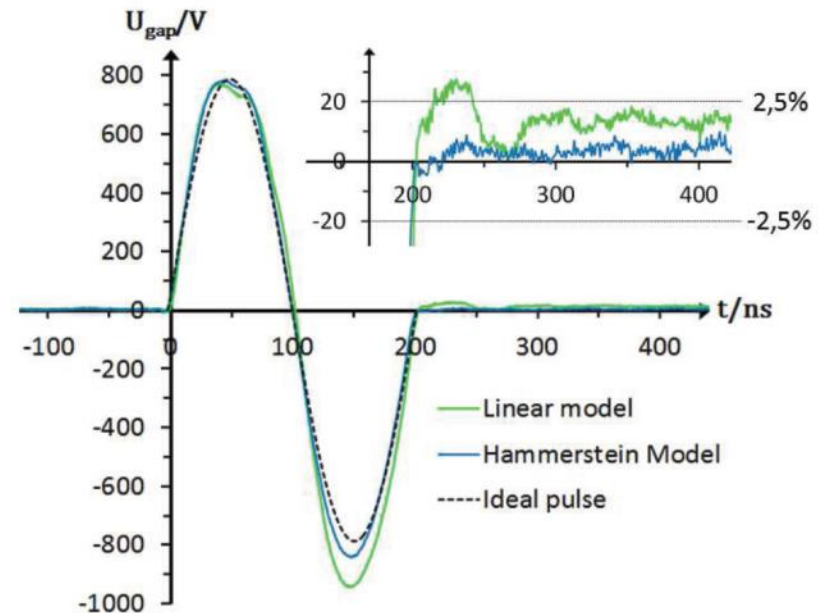
problem with linear pre-distortion:
amplifier characteristic



no datasheet value depicts this
characteristic -> amplifier
selection by testing



J. Harzheim, H. Klingbeil, Temf, TU Darmstadt



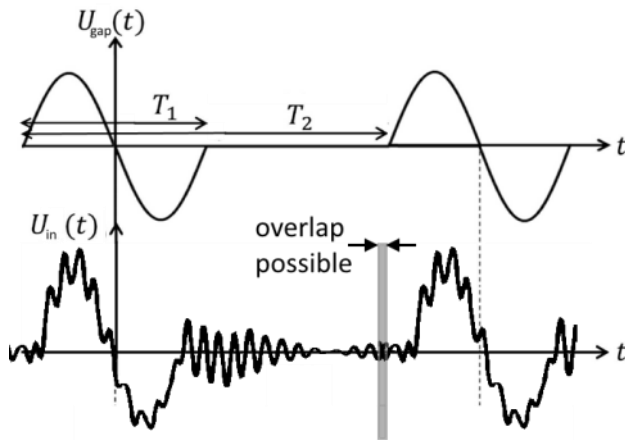
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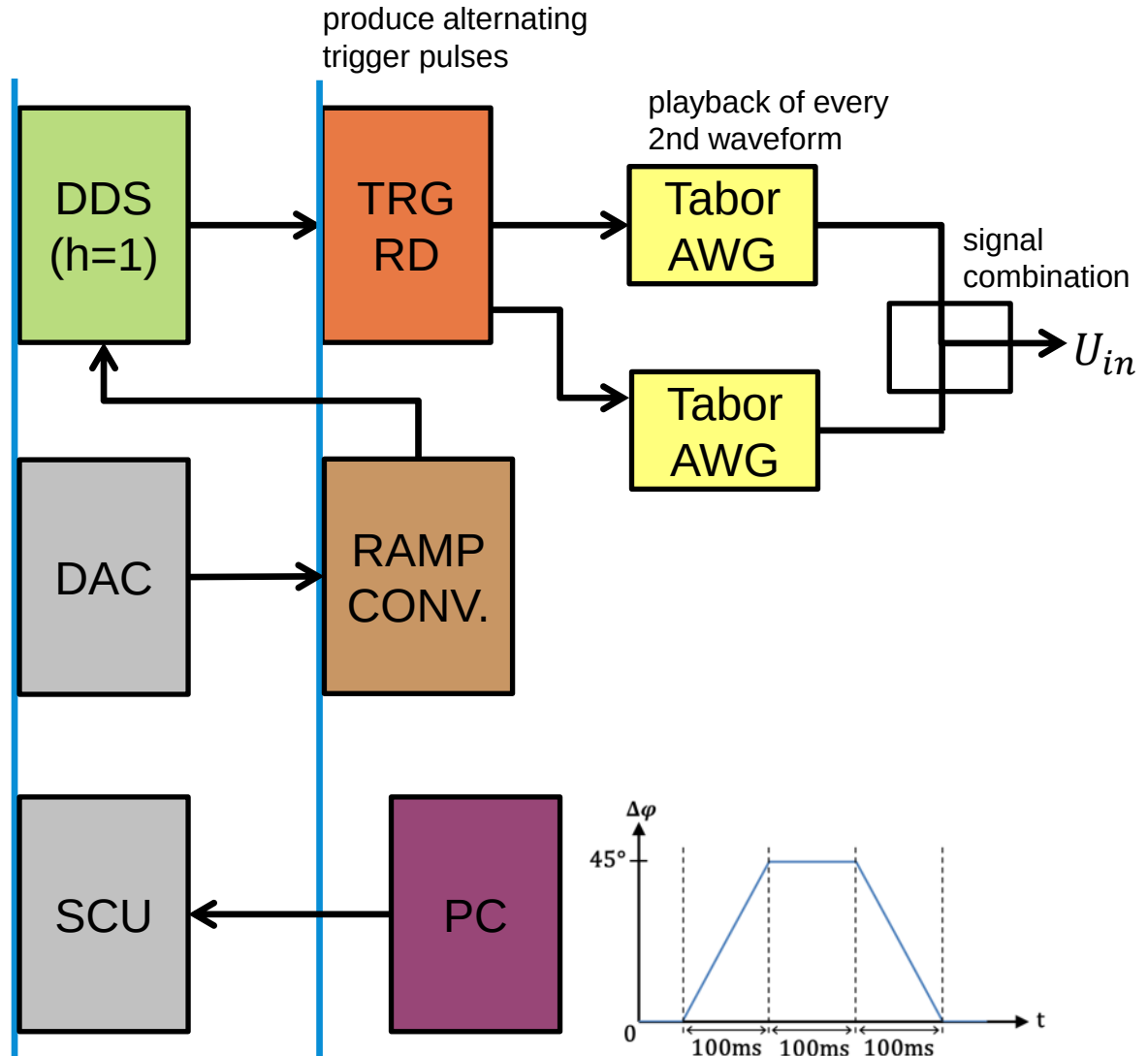
- SIS100 BB system

LLRF – re-triggering

when barriers are moved, consecutive pre-distorted waveforms may overlap

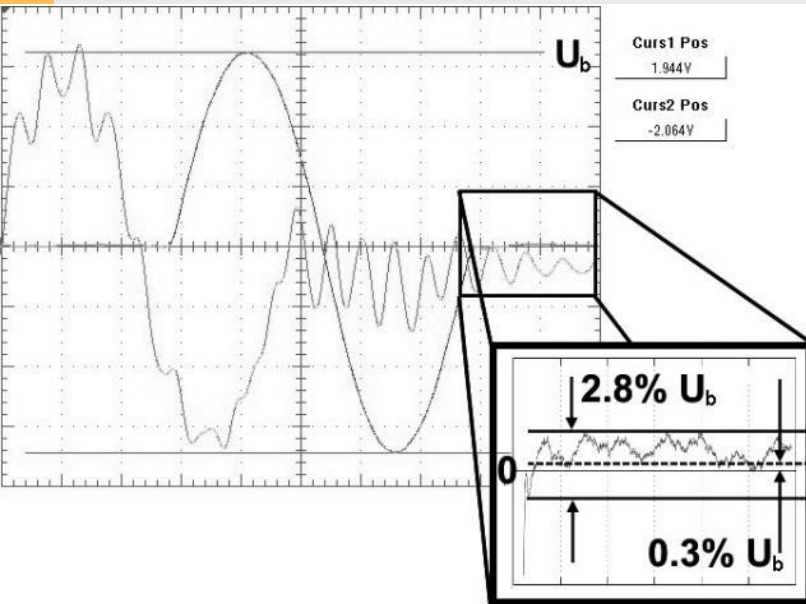


signal generation must detect new trigger while output still active
 -> 2 alternating signal generators



K. Groß, H. Klingbeil, Temf, TU Darmstadt

ESR BB system – full system results I

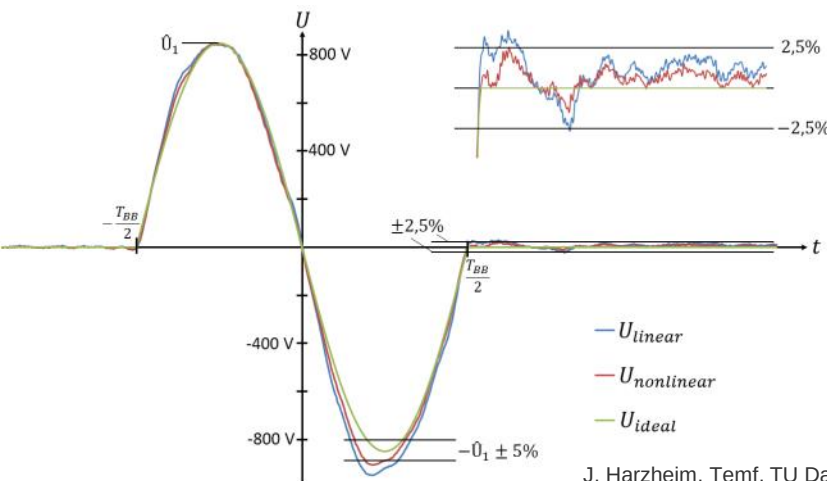


linear pre-distortion:

- $U_b = 520 \text{ V}$
- good quality

non-linear pre-distortion:

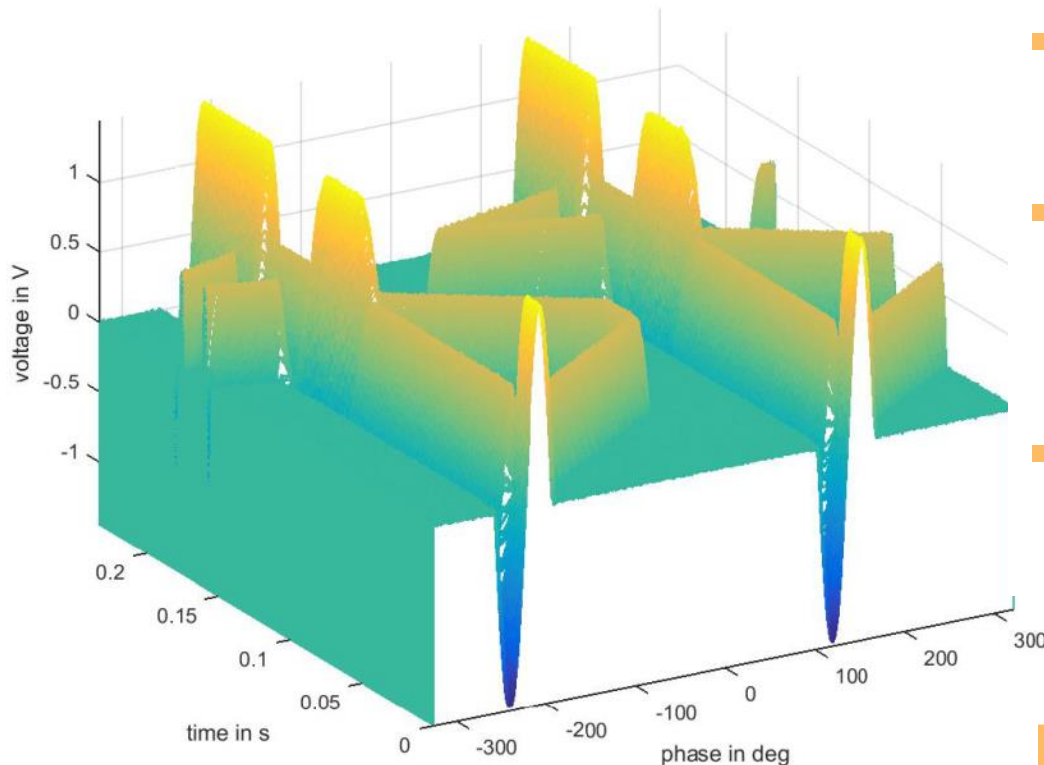
- $U_b = 800 \text{ V}$
- improvement in ringing after pulse
- symmetry insufficient (internal amplifier limitation?)



J. Harzheim, Temf, TU Darmstadt

ESR BB system – full system results II

- phase shifting of moving barriers demonstrated with full system (manual data supply from PC to SCU)



- two revolution periods are shown
- here barriers are created at equal phase angle (amplitude doubles)
- one barrier is shifted by 180° in both directions



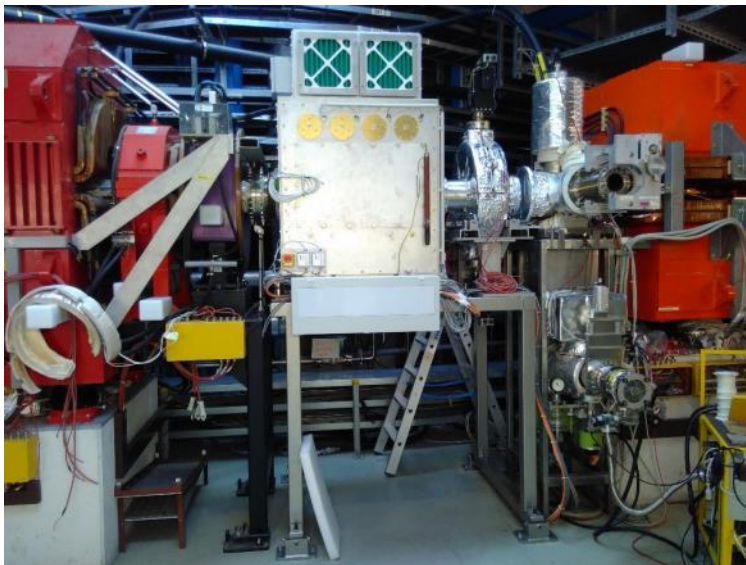
full system works
as intended!

-> installation approval

ESR BB system – status + outlook

status:

- function of full system demonstrated
- pulse amplitude $U_b=520$ V with high quality achieved (1 kW amplifier)
- installation in ESR finished



to do:

- software development for unit controller (task: e.g. calculation of pre-distorted waveforms, control of signal generators)
- adaption of control system connection (e.g. phase ramp in FESA-class for ramped-devices?)

outline

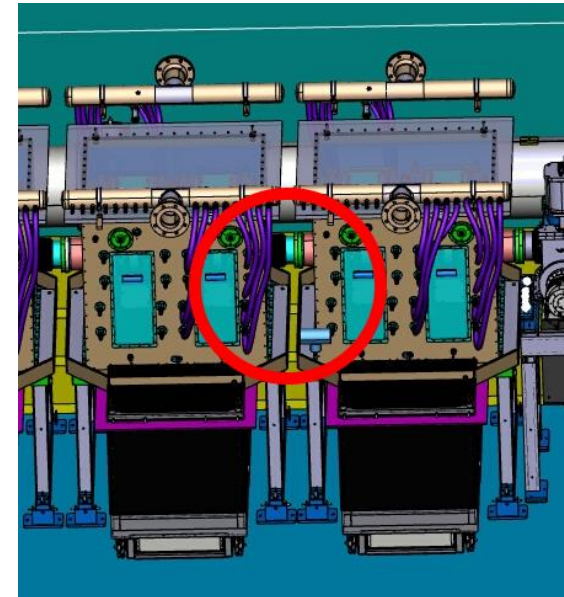
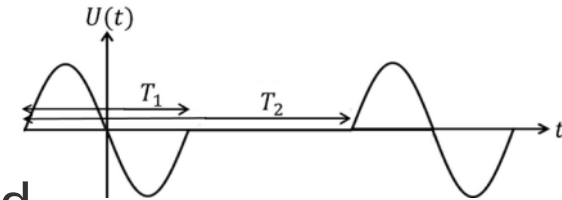
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- SIS100 BB system: pre-development phase
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 - oil cooling
- SIS100 BB power amplifier design
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 - frequency domain
 - time domain
- SIS100 BB outlook

procurement
starts 2019



SIS100 requirements

- creation of 2 barriers in two empty buckets -> single sine pulses of $T_1=666$ ns ($f_{BB}=1.5$ MHz)
- flexible control of amplitude and repetition period T_2 between $f_{rep}=110$ kHz and $f_{rep}=270$ kHz
- pulse amplitude $\hat{U} = 15$ kV
- maximum beam impedance 1000Ω (cavity+amplifier)
- cavity length < 1.3 m, but only 1.0 m for housing (due to feasibility of flange mounting)
- usability of identical cavities and amplifiers for SIS100 Longitudinal Feedback workpackage



SIS100 BB cavity design

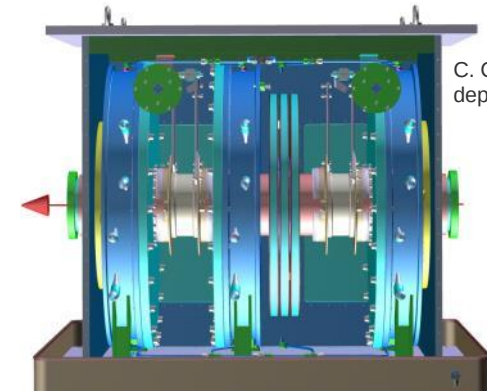
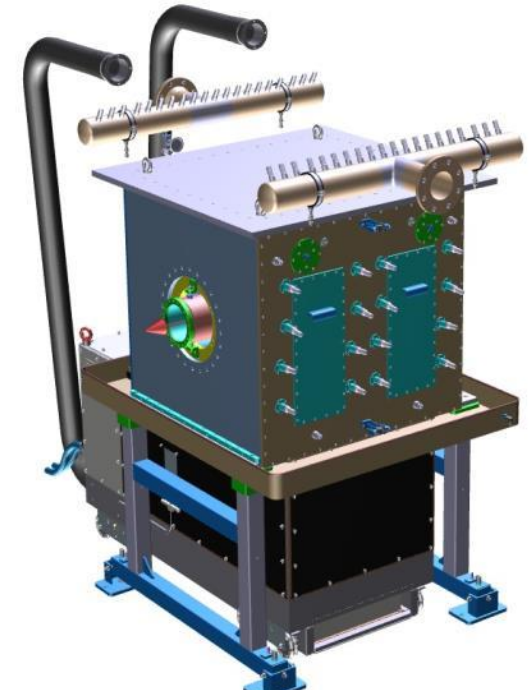
design goals:

- broadband behaviour (-> MA cores)
- voltage gradient 15 kV/m (MA cores)
- matching with tetrode amplifier at tetrode's working point
- cavity's resonance frequency at or below barrier-bucket frequency f_{BB}

=> very similar to SIS18 h=2 cavity requirements!

working hypothesis:

- use h=2 cavity with less MA cores in order to increase resonant frequency

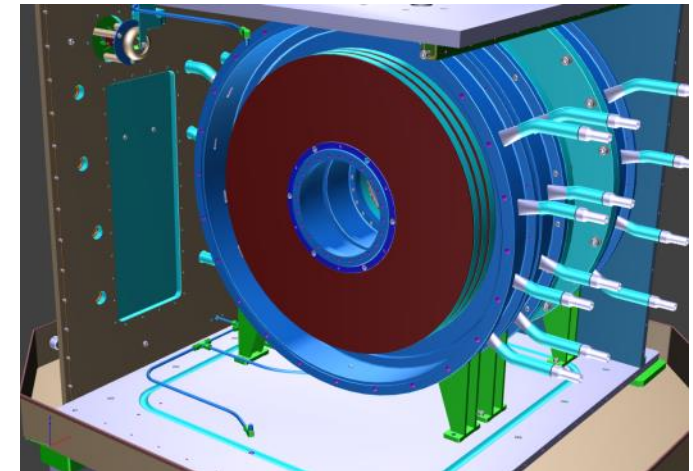
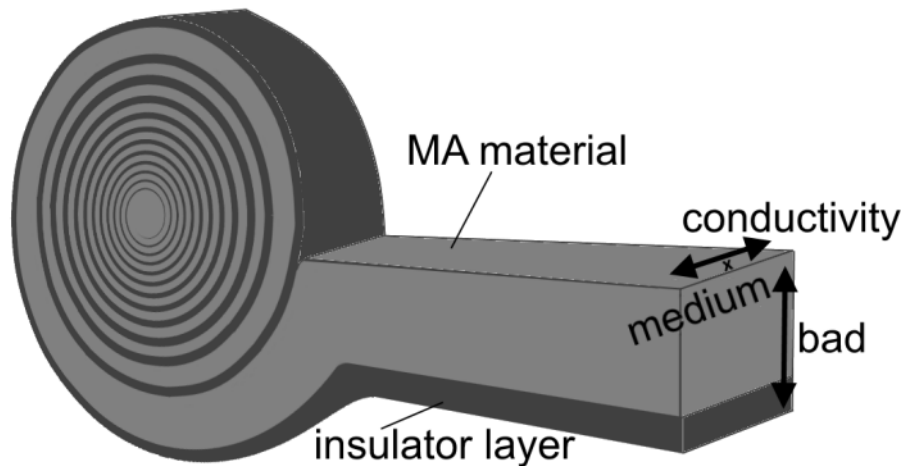


C. Christoph, RRF department, GSI

SIS100 BB – oil cooling

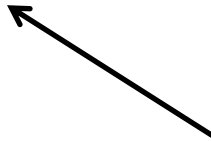
- due to magnetic loss effects, ring cores heat up during operation
- heat conductivity in FT-3M is anisotropic

P. Hülsmann, RRF
department, GSI



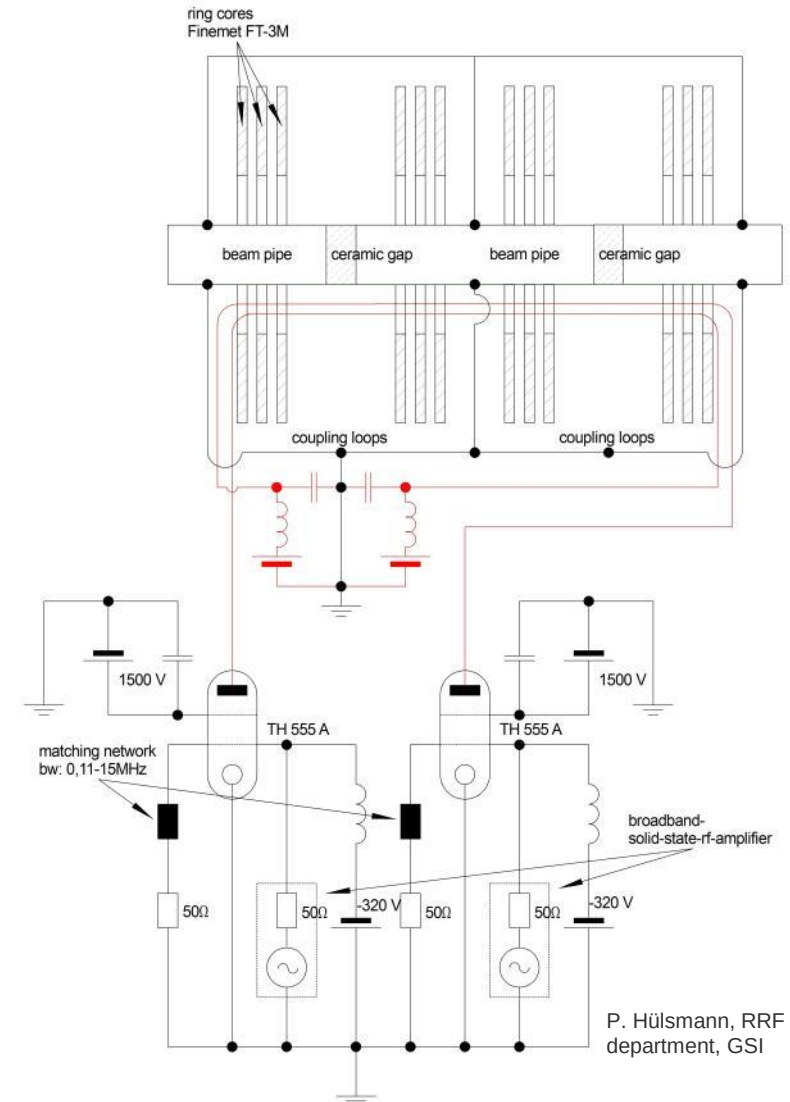
- heat can only be removed through side surface, which is not flat
- insufficient heat transfer to cooling disks or air makes direct liquid cooling (oil) necessary

outline

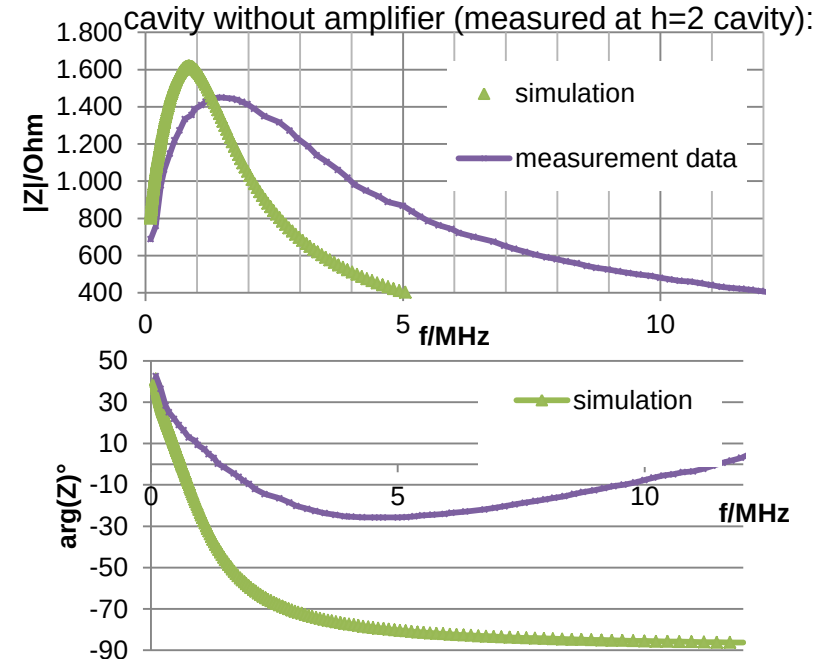
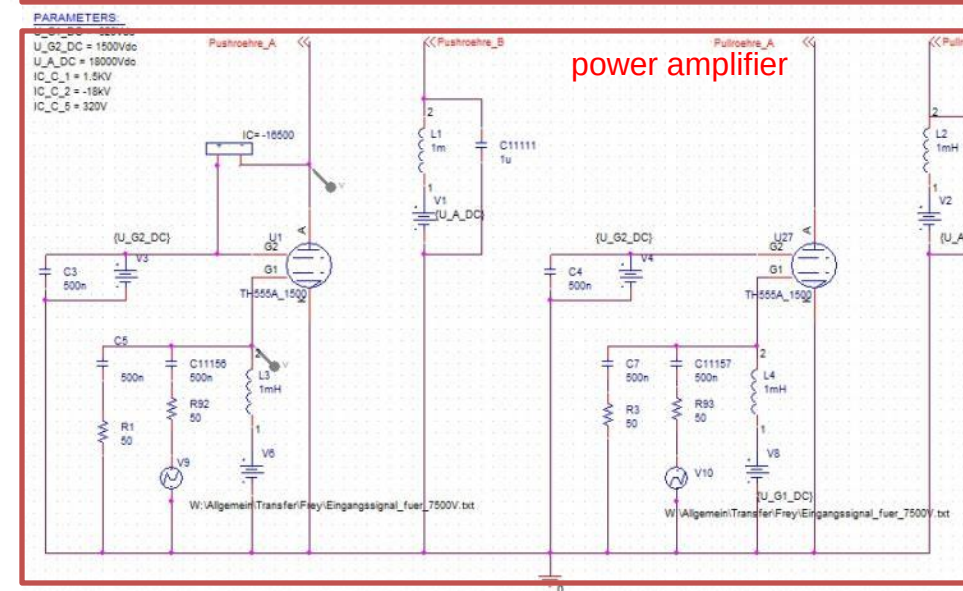
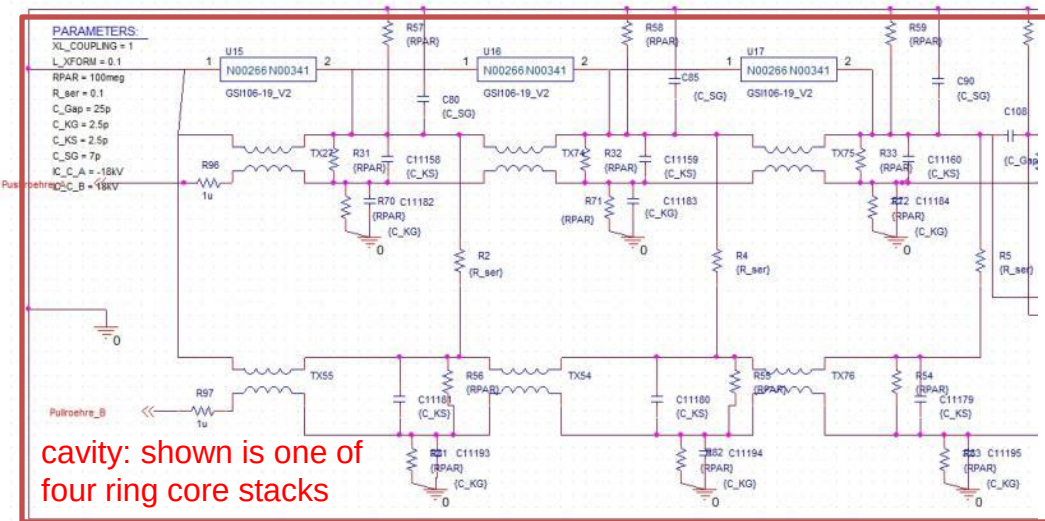
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- strategy:
- PSpice simulation of planned SIS100 BB cavity system
 - comparison with measurements from mock-up of SIS100 BB cavity (with $h=2$ components)
- 

SIS100 BB power amplifier design

- required signal quality
-> class A amplifier (to avoid distortion in push-pull configuration)
- tetrode capable of the expected anode dissipation power at working point above 15 kV -> Thales TH555
- compensation of anode currents by opposing winding directions of coupling loops

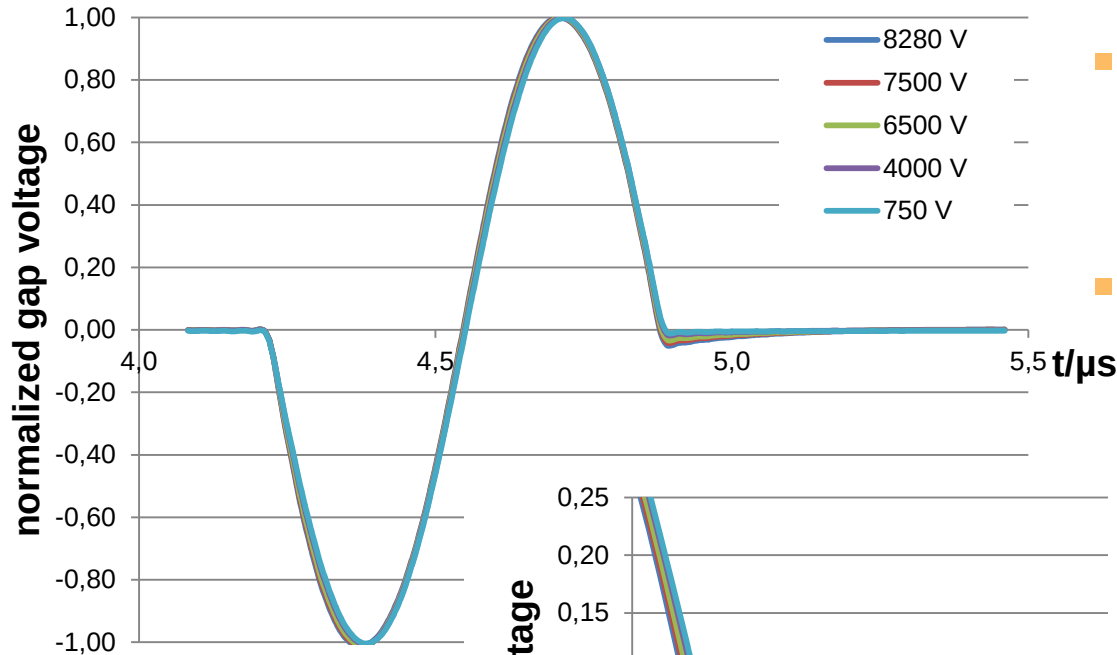


SIS100 BB simulation results – frequency domain

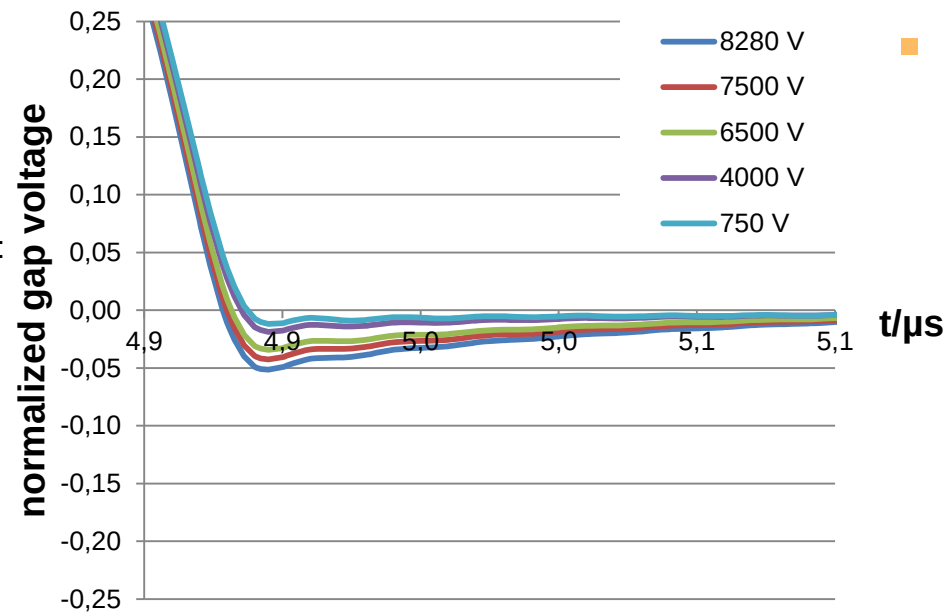


- tetrode model includes non-linearity
- deviations now understood
- sufficient matching between cavity and tetrode ($R_i \approx 1500\Omega$)
- resonant frequency $f_r \approx 1.5 \text{ MHz}$

SIS100 BB simulation results – time domain

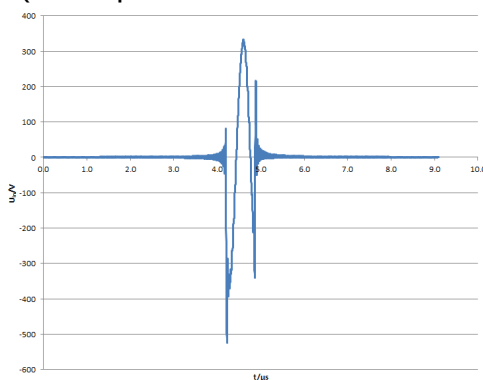


- desired pulse amplitude of 15 kV is achieved (7.5 kV across each gap)
- ringing at the pulse's end is below 5% even with linear pre-distortion



- desired bandwidth for input signal transmitting components: from 20 kHz to 30 MHz

input voltage in time domain
(linear pre-distortion, 0.02-30 MHz):



SIS100 BB status and outlook

- Technical Concept document finished
- considerable effort was made to reduce technical risks by investigating (mostly at ARD broadband test cavity):
 - frequency dependent ring core properties
 - cavity bandwidth
 - ring core cooling
 - frequency- and time-domain simulations of full cavity/amplifier system
 - impedance reduction by cavity detuning
 - beam loading (effect of DC-fraction)
 - signal generation (LLRF system)
- Technical Concept proved feasible through all tests (15 kV, <5% ringing expected with non-linear pre-distortion)
- Detailed Specification 95% finished
- start of procurement is planned for June 2019

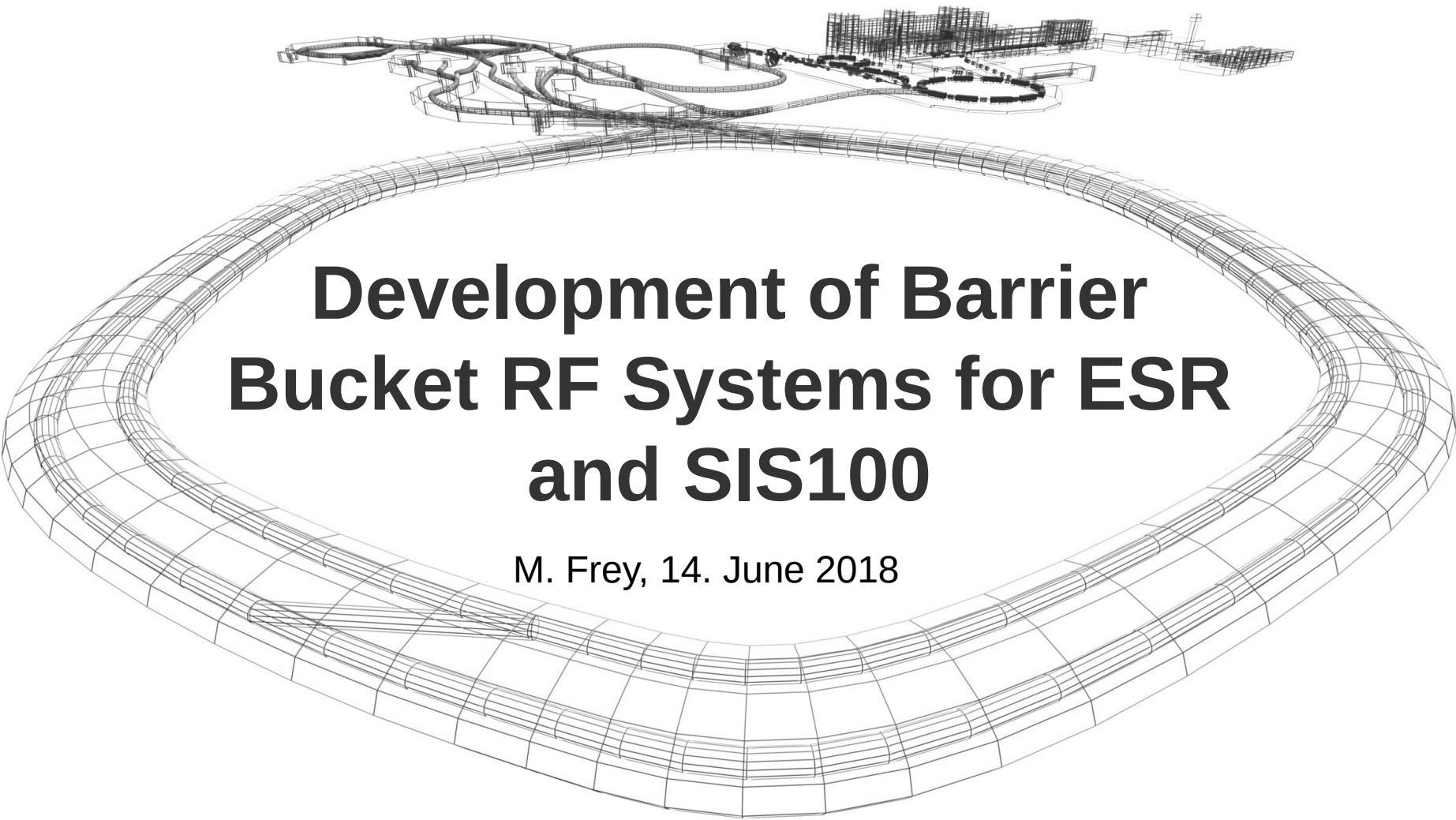
Thanks to all contributors



Thank you for your attention



GSI Helmholtzzentrum für Schwerionenforschung GmbH

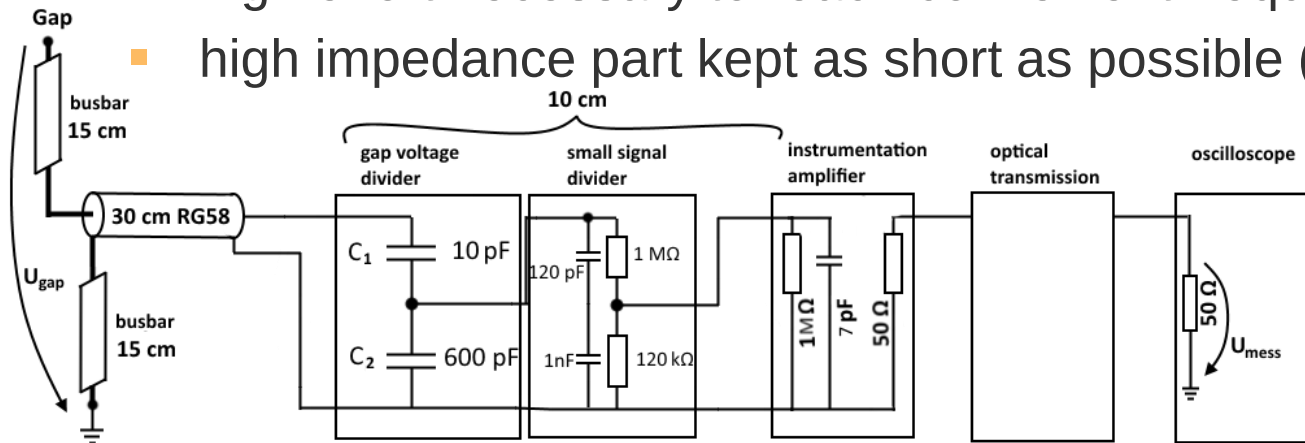
A 3D wireframe model of a particle accelerator, showing a large, oval-shaped ring structure with a grid-like pattern, and a smaller, more complex structure in the background.

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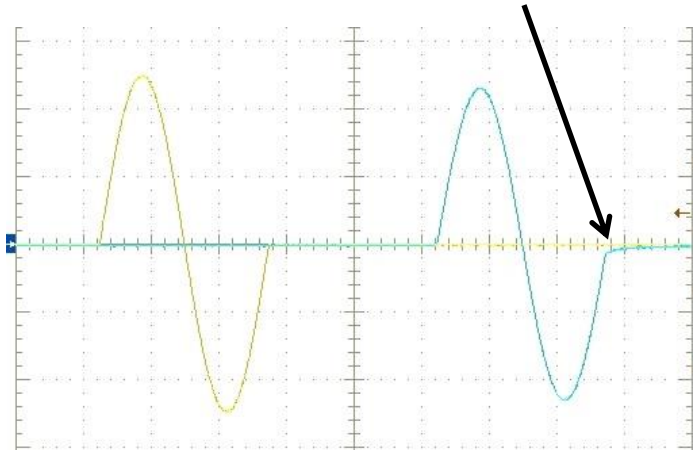
M. Frey, 14. June 2018

Appendix - gap voltage measurement

- distortion in measurement chain directly alters gap voltage signal
- high effort necessary to reach convenient frequency-response
- high impedance part kept as short as possible (reduce reflections)



130 m ½" Cellflex: 5% distortion



2000 m optical fiber: 2% distortion (but synchronisation with SIS18 not possible yet)

